Original Research

Enhanced Adsorption of Two Reactive Dyes onto Al-Based Waterworks Sludge Modified by Calcination

Minghua Wei^{1,2}, Xiaohan Duan³, Wani Zhou⁴, Kai Huang⁴, Yawei Chen⁴, Jingxi Tie^{5*}

1 School of Water Resources, North China University of Water Resources and Electric Power, Zhengzhou 450046, PR China 2 Henan Key Laboratory of Water Resources Conservation and Intensive Utilization in the Yellow River Basin, Zhengzhou 450046, PR China 3 School of Water conservancy, North China University of Water Resources and Electric Power, Zhengzhou 450046, PR China 4 Zhongzhou Water Holding Co., Ltd., Zhengzhou 450000, PR China 5 School of Environmental and Municipal Engineering, North China University of Water Resources and Electric Power, Zhengzhou 450045, PR China

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Abstract

Al-based waterworks sludge (ABWS) modified by calcination was reused as an adsorbent for the removal two reactive dyes, namely, reactive yellow 176 (RY-176) and reactive red 195 (RR-195) from aqueous solution. 800ºC was proved to be the optimal calcination temperature in the range of 200-900ºC. A series of static adsorption experiments were carried out using ABWS calcinated at 800ºC (ABWS-800) as adsorbent. The results indicated that the adsorption of both the two dyes by ABWS-800 was almost independent of initial solution pH, and the adsorption capacity of ABWS-800 for RR-195 was about 1.4 times higher than that for RY-176. The pseudo-second-order kinetic model was best among the three models to describe the adsorption of the two reactive dyes, and Freundlich isotherm model was better matched than the Langmuir isotherm model to describe the adsorption process. Na₂SO4 inhibited the adsorption of the two dyes onto ABWS-800. This work provided the theoretical basis and technical support for the optimization of reaction conditions for the decontamination of dyes wastewater by "waste" ABWS.

Keywords: adsorption, reactive dye, Al-based waterworks sludge, calcination

^{*}e-mail: 15202843@qq.com

Introduction

One of the most pressing environmental and public health challenges today is the contamination of aquatic environment by colors derived from various industrial processes, such as textile, dyeing, paper, pulp, tannery, paint, and dye manufacture, especially for those with synthetic origins [1]. Reactive dyes, which can form covalent bonds with the hydroxyl or amine groups of natural fibers, are one of the most prominent types of azo dye with various reactive groups and have a wide industrial application due to their excellent dyeing processes, brighter colors, and low price [2-4]. However, due to the high solubility of the dyes, around 10-20% of the total consumption is lost in the effluent during the dyeing process [5]. Becuse of the complex aromatic molecular structures and xenobiotic properties, they are mutagenic, carcinogenic and resistant to the physicochemical, thermal, and optical degradation in the environment [6, 7].

As a result, the dyes discharges into receiving water bodies could cause major threat to ecosystem through blocking the sunlight, reducing photosynthesis and dissolved oxygen concentration. Reactive dyes are more recalcitrant compounds than other dyes because of their defects such as strong color, high alkalinity, and high concentration of organic materials [8]. The presence of those dyes in water is highly undesirable even in very low concentrations.

Various physical, chemical, and biological technologies including coagulation/flocculation [9, 10], adsorption [11-13], advanced oxidation [14], membrane separation [15] and microbial degradation [16], etc. had been developed for reactive dye removal from water. Among those methods, adsorption had been adopted widely due to their easy operation, low cost,

As a raw material with huge potential for beneficial reuse in water and environmental engineering, waterworks sludge has been applied for the treatment of contaminants such as phosphorus [29, 30], heavy metal [31, 32], dyes [33] and so on, but the removal of reactive dyes by raw waterworks sludge was poor [33]. The adsorption performance of waterworks sludge could be improved by calcination. For instance, Jeon et al. found that the adsorption capacity of modified alum sludge for $As(V)$ was 5.4-8.7 times greater than that of the raw adsorbent [34]. Everaert et al. revealed that the alum sludge granule calcinated at 550ºC had the largest phosphorus adsorption of 7.27 mg/g compared to those calcinated at 100ºC and 300ºC [35]. However, the research on reactive dyes adsorption by thermally modified Al-based waterworks sludge (ABWS) was currently not well documented.

Thus, the aim of this study was to evaluate the adsorption capacity of ABWS modified by calcination to remove two kinds of reactive dyes, namely, reactive yellow 176 (RY-176)and reactive red 195 (RR-195) from artificial dye-bearing wastewater. The molecular structures of the two dyes are shown in Fig. 1. Compared with RY-176, RR-195 has more anionic groups $(-SO_3^2)$ and larger molecular size. The physiochemical and properties of the adsorbents were characterized using X-ray florescence (XRF), X-ray diffraction (XRD), and Brunauer-Emmett-Teller surface analysis (BET). The effect of various parameters such as calcination temperature, solution initial pH, inorganic salt, and the kinetic and isotherm of adsorption process were investigated in detail.

C.I. Reactive Yellow 176

C.I. Reactive Red 195

Fig. 1. The molecular structures of RY-176 and RR-195.

Material and Methods

Calcination of the ABWS

ABWS was collected from a sludge drying filed in a drinking water treatment plant in Zhengzhou, China, where polyaluminum chloride was used as coagulant for drinking water process. ABWS collected from five points distributed at the for corners and the midpoint of the sludge drying filed was mixed evenly and dried in open air and in a drier at 105ºC for 2 h in sequence. The dried ABWS was crushed and passed through 0.15 mm screen. Then the ABWS powder was calcinated at the temperature ranging from 200ºC to 900ºC for 2 h at a temperature gradient of 100ºC. At last the ABWS calcinated at different temperature were collected to test the adsorption capacity for RY-176 and RR-195.

Characterization of ABWS

The raw ABWS and the ABWS calcinated at 800ºC (ABWS-800) which was tested to possess the best adsorption capacity for the two dyes were characterized. The X-ray florescence (XRF, Smartlab 3kw, Rigaku Ltd., Japan) was used to analyze the compositions of the two samples. XRD patterns of the two samples were obtained using an X-ray diffractometer (Smartlab 3 kw, Rigaku Ltd., Japan). The surface areas of the two samples were measured using N_2 adsorption isotherm with a model of Brunauer, Emmett, and Teller (Autosorb-I, Quantachrome, USA).

Preparation of the Artificial Wastewater

The dye-bearing wastewater was synthesized by adding RY-176 (Decai pigment chemical Co., Ltd, Shenzhen, China) and RR-195 (Yien chemical technology Co., Ltd, Shanghai, China) into the deionized water, and the pH value of the wastewater was adjusted using 0.1 mol/L HCl (Tongjie chemical reagent Co., Ltd, Shanxi, China) and NaOH (Kemio chemical reagent Co., Ltd, Tianjin, China) solutions. All of the chemicals used in this study are analytically pure.

Adsorption Experiments

Static adsorption experiments were carried out in the following way: 0.1 g ABWS and 30 mL dye-bearing solution were added into flask and allowed to react in a shaker at different temperature for various time. At the end of the reaction, the mixture was centrifugated at 8000 rpm for 5 min. The residual RY-176 and RR-195 in the supernatant were determined using a spectrophotometer (UV-5100B, Yuanxi instrument, China) at 400 nm and 540 nm, respectively. The dye uptake was calculated using the following equation [36]:

$$
q = \frac{(C_0 - C_e)V}{m} \tag{1}
$$

where q is the amount of RY-176 and RR-195 adsorbed (mg/g) by per unit of adsorbent, C_0 and C_e are the initial and equilibrium concentration of RY-176 and RR-195 (mg/L), respectively, V is the volume of solution (L), and m is the mass of ABWS-800 (g) used in the experiment.

Results and Discussion

Effect of Calcination Temperature

The effect of calcination temperature on the adsorption of RY-176 and RR-195 by ABWS is shown in Fig. 2.

It can be seen that the adsorption capacity o f RY-176 and RR-195 by ABWS could be changed obviously by calcination. The best removal of both the two dyes was achieved using ABWS-800, and the corresponding removal efficiency of RY-176 and RR-195 were 68.9% and 78.6%, respectively. With the further increase of calcination temperature to 900ºC, the adsorption of RY-176 and RR-195 decreased, probably resulted from the transformation of amorphous aluminum hydroxide/oxide into crystalline forms at higher calcination temperature, which would lead to the decrease of adsorption capacity [34]. Thus, 800ºC was determined to be the best calcination temperature, and ABWS-800 was used as the adsorbent in the following experiments.

Characterization of ABWS

The primary compositions of raw ABWS and ABWS-800 are shown in Table 1. SiO_2 , CaO, Al_2O_3

Fig. 2. Effect of calcination temperature on the adsorption of RY-176 and RR-195 by ABWS.

Composition	Percentage $(\%)$			
	Raw ABWS	ABWS-800		
SiO ₂	40.04	39.28		
CaO	34.14	35.89		
AI ₂ O ₃	10.8	10.76		
Fe ₂ O ₃	10.53	9.54		
K,O	1.21	1.19		
MgO	1.14	1.33		
TiO,	0.688	0.619		
Na, O	0.293	0.309		

Table 1. The main compositions of raw ABWS and ABWS-800.

and $Fe₂O₃$ were the major components of both raw ABWS and ABWS-800. SiO₂, CaO and $Fe₂O₃$ mainly derived from the minerals in the raw water, and Al_2O_3 might come from both the raw water and the coagulant used in the water plant. There was negligible difference between the primary composition of raw ABWS and ABWS-800, indicating that thermal treatment could hardly change the component content of the ABWS. However, unlike the results reported in the literature [34], the specific surface area decreased from 13.765 $g/m²$ for ABWS to 8.378 g/m² for ABWS-800, which might be attributed to the destruction of the pores during the thermal treatment.

XRD analysis was conducted to determinate the crystalline structure of ABWS and ABWS-800 (Fig. 3). The XRD spectra showed that both ABWS and ABWS-800 were characterized by amorphous substances. The 2θ peaks found at 26.4° and 20.6° were assigned to $SiO₂$ (JSPDS 05-0492) [37] and $A \,$ l P O₄ (JSPDS 11-0500) [38] for both ABWS and ABWS-800. The diffraction peaks presented at 29.4°, 36.0°, 39.4° and 43.17° were corresponded to $CaCO₃$

Fig. 3. The XRD pattern of the raw ABWS and ABWS-800. a) ABWS; b) ABWS-800.

(JSPDS 47-1743) for ABWS [39, 40], which disappeared in the spectrum of ABWS-800, indicating the decomposition of $CaCO₃$ at 800°C.

Effect of Initial Solution pH

Solution pH is an important factor for the adsorption process due to its influence on both the characteristic of adsorbent surface and ionization of dyestuff molecule [32]. The effect of initial solution pH on the adsorption of RY-176 and RR-195 on ABWS-800 was examined in the pH range of 3-10, the results are shown in Fig. 4.

As shown in Fig. 4, the adsorption capacity of RY-176 and RR-195 on ABWS-800 varied slightly as solution pH increased from 3 to 10, with a value from 12.4 mg/g to 13.5 mg/g and 17.1 mg/g to 18.3 mg/g, respectively, indicating that the adsorption of RY-176 and RR-195 on ABWS-800 was broadly independent of solution pH. The result in the present research was consistent with that reported in the literature. Kayranli et al. found that changing the pH value affected slightly on the removal of reactive blue 29 onto iron based waterworks sludge [32], and Netpradit et al. observed that when the initial pH of the dye solution was in the range 3-10, the adsorption of azo reactive dyes by metal hydroxide sludge derived from the electroplating sector was unaffected [41]. Though the adsorption of anion dyes was mainly through electrostatic attraction between sulfonate ions $(-SO_3^2)$ and the positive binding sites on metal hydroxide sludge, which depended highly on the pH of solution, the sludge might contain some buffer that could resist the pH change of the aqueous system to maintain a stable removal of dyes. The results of the present work implied that ABWS-800 could be applied to the removal of RY-176 and RR-195 in a wide range of initial solution pH.

In comparison, the adsorption capacity of ABWS-800 for RR-195 was about 1.4 times higher than that for RY-176, probably resulting from the fact that

Fig. 4. Effect of initial solution pH on adsorption of RY-176 and RR-195 on ABWS-800 (Temperature: 30ºC, Reaction time: 3 h).

Fig. 5. The adsorption kinetic behavior of RY-176 and RR-195 onto ABWS-800 (Temperature: 30ºC, pH: 5.5).

RR-195, whose molecule was larger than RY-176, was more strongly adsorbed by metal hydroxide sludge due to its higher negative charge and lower solubility. It was concluded that more charged dyes had a higher adsorption affinity, and so the higher the charge quantity of the dyes, the greater the adsorption on the metal hydroxides sludge [42].

Kinetics Study

The kinetic behavior of the adsorption process of RY-176 and RR-195 onto ABWS-800 was examined at different dyes concentration, the result is shown in Fig. 5. The adsorption process achieved equilibrium in around 8 hours, and the equilibrium duration increased with starting dye concentration. Each of the four adsorption processes included a fast and a slow adsorption stage. The fast stage lasted from the beginning of the experiment to the $10th$ min during which the ABWS-800 could offer enough active sites for the adsorption reaction and resulted in a rapid adsorption. It also indicated a high affinity between the two dyes and the surface of ABWS-800. Whereas, the adsorption slowed down in the second stage, suggesting a gradual equilibrium of adsorption, probably due to less active site left for the reaction and the lagging intraparticle diffusion of the dye molecules in the adsorbent.

Three famous models, namely, pseudo-first order, pseudo-second order and Elovich model were used to fit the experiment data to further understand the adsorption process. The linear forms of the three models are presented as Eq. (2)-Eq. (4) [26]:

$$
\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303}t
$$
 (2)

$$
\frac{t}{q_t} = \frac{t}{q_e} + \frac{1}{k_2 q_e^2}
$$
 (3)

$$
q_{t} = \frac{1}{\beta} \ln(\alpha \beta) + \frac{1}{\beta} \ln t
$$
 (4)

where q_e (mg/g) and q_t (mg/g) are the concentration at equilibrium and time t, respectively. k_1 (1/min) and k_2 (1/min) are the pseudo-first order and pseudosecond order rate constants. α (mg/g·min) is the initial adsorption rate, and β (g/mg) is the desorption constant.

The kinetics parameters obtained from the three equations are shown in Table 2. The values of the correlation coefficient R^2 of the pseudo-secondorder model were higher than those of the other two equations. Meanwhile, as shown in Table 2, the $q_{e,exp}$ obtained from the experiment of the pseudo-secondorder model agreed very well with those obtained from the model. Hence, the pseudo-second-order model was the best one to describe the adsorption process, indicating that chemical adsorption was the rate controlling step and the occupancy rate of the active sites was proportional to the square of the number of unoccupied sites, the adsorption occurred via covalent bonding and ion exchange between the dyes molecule and the surface active sites of the adsorbent [43, 44]. It could be seen in Table 2 that the q_e value of RY-176 and RR-195 increased with the initial dye concentration, resulting from the larger adsorption driving force at higher adsorbate concentration.

Isotherm Study

The influence of equilibrium concentration of RY-176 and RR-195 in the adsorption process was examined at initial dye concentration of 10-160 mg/L, and the result is given in Fig. 6.

Dye C_0 (mg/L) pseudo-first-order pseudo-second-order Elovich qe,cal k1 *R*² qe,cal k2 *R*² α β *R*² RY-176 100 | 7.394 | 0.005 | 0.947 | 19.455 | 0.003 | 0.998 | 41.324 | 0.478 | 0.962 25 2.751 0.006 0.941 7.013 0.008 0.999 16.475 1.363 0.983 RR-195 100 | 3.968 | 0.005 | 0.901 | 26.247 | 0.006 | 0.999 | 7.44E+06 | 0.836 | 0.982 25 1.976 0.005 0.937 7.305 0.010 0.990 441.801 1.793 0.952

Table 2. Parameters of the three kinetic models for RY-176 and RR-195 adsorption by ABWS-800.

Fig. 6. The influence of equilibrium concentration in the adsorption process of RY-176 and RR-195 by ABWS-800 (pH: 5.5, Reaction time: 8 h).

As seen in Fig. 6, the adsorption capacity of the two dyes increased as equilibrium concentration improved, accompanying with a decrease in the adsorption rate, indicating the gradual saturation of surface active sites on ABWS-800. Between the temperatures applied in the adsorption experiment, low temperature (20ºC) was more beneficial for the removal of the two dyes, especially for RR-195, suggesting that the adsorption of the two active dyes onto ABWS-800 was exothermic. It could be explained on the basis that the solubility of the dyes increased at higher temperature and adsorbateadsorbent interactions decreased, thus resulting in decreased adsorption. The results also indicate that more desorption than adsorption of the two dyes took place at higher temperature [45]. Consideration of the high temperature properties of dye wastewater, it would be not in favorable to the application of ABWS-800 to the decontamination of dyes wastewater.

The equilibrium isotherm is crucial to understand the interaction between adsorbate and adsorbent. The Langmuir and Freundlich isotherms, expressed as Eq. (5) and Eq. (6), respectively, were used to characterize the adsorption of RY-176 and RR-195 onto ABWS-800.

$$
\frac{c_e}{q_e} = \frac{1}{q_m b} + \frac{c_e}{q_m} \tag{5}
$$

$$
\log q_e = \log k_f + \frac{1}{n} \log c_e
$$
 (6)

where c_e (mg/L), q_e (mg/g) and q_m (mg/g) is the concentration, adsorption capacity and the maximum adsorption capacity at equilibrium, respectively. b (L/mg) is the Langmuir constant, k_f ((mg/g)/(mg/L)ⁿ) and n are the Freundlich constant.

Fig. 7. The fitting results of the two isotherms. a) Langmiur isotherm model, RY-176; b) Freundlich isotherm model, RY-176; c) Langmiur isotherm model, RR-195; d) Freundlich isotherm model, RR-195.

Dye	Temperature $(^{\circ}C)$	Langmuir		Freundlich		
		H_{m}	R^2	K_{c}	n	R^2
RY-176	20	32.154	0.971	81.581	2.501	0.995
	40	30.395	0.971	96.075	2.595	0.998
RR-195	20	41.494	0.971	29.214	1.889	0.987
	40	41.152	0.940	7.037	1.451	0.991

Table 3. Parameters of Langmuir and Freundlich isotherms for the adsorption of RY-176 and RR-195 by ABWS-800.

The fitting results and the parameters of adsorption isotherms are presented and summarized in Fig. 7 and Table 3, respectively.

As shown in Table 3, the higher R^2 values of Freundlich isotherm at both of the two temperatures than those of Langmuir isotherm for the adsorption of RY-176 and RR-195 by ABWS-800 indicated that the Freundlich equation was more suitable to describe the adsorption process, which presented that the heterogeneous surface of ABWS-800 and multilayer adsorption with non-uniform distribution of heat energy on ABWS-800 surface occurred [46]. The value of 1/n which varied between 0.39 and 0.69, indicating the favorable adsorption of dye molecule onto ABWS-800 and chemical adsorption took place during the removal of the two dyes [32]. The higher k_f value for RR-195 demonstrated that RR-195 had a higher adsorption affinity to the surface of ABWS-800 compared with RY-176, thus resulting in a greater adsorption capacity for RR-195, which was identified with the results reported in the previous section.

Effect of Salt Concentration

The effect of Na_2SO_4 on adsorption of RY-176 and RR-195 by ABWS-800 was investigated since Na_2SO_4 is widely used to improve the reactive dye uptake during the dyeing process. The result is shown in Fig. 8.

separability and applicability. Fig. 8. Effect of salt concentration on adsorption of RY-176 and RR-195 by ABWS-800 (Reaction time: 3 h, pH: 5.5, Temperature: 30ºC).

As shown in Fig. 8, the removal of the two reactive dyes by ABWS-800 was inhibited clearly in the presence of Na_2SO_4 . The adsorption capacity of RY-176 and RR-195 decreased from 20.5mg/g and 27.3 mg/g to 9.6 mg/g and 20.3 mg/g, respectively, as Na_2SO_4 dosage increased from 0 to 5 g/L, and further deceased to 8.3 mg/g and 19.3 mg/g, respectively, as Na_2SO_4 dosage increased to 15 g/L. The results indicated that the presence of Na_2SO_4 imposed more significant impact on the adsorption of RY-176 and RR-195 than the increase of Na_2SO_4 concentration. The result in the present study agreed well with that reported in the literature. According to Netpradit [36], a high decrease in reactive dyes adsorption by metal hydroxide sludge occurred in the presence of Na_2SO_4 , which had higher valence, would compete strongly with SO_3^2 for binding sites on adsorbent. Moreover, the adsorption of SO_4^2 ⁻ might also block some of the adsorption active sites for the dyes molecules, consequently leading to the decrease in the adsorption of the two dyes on ABWS-800.

Conclusions

In this study, the enhanced removal of two reactive dyes, RY-176 and RR-195, by ABWS modified by calcination was examined. Calcination was proved to be an effective way to improve the adsorption capacity of Al-based waterworks sludge, and 800ºC was found to be the best calciantion temperature in the range of 200-900ºC. The results of the adsorption experiment indicated that solution pH impacted slightly on the adsorption of the two dyes by ABWS-800. Compared with the first-second-order model and Elovich model, the pseudo-second-order kinetic model was better to describe the adsorption process, and Freundlich isotherm model fitted the experimental data better than the Langmuir isotherm model. The adsorption of both the two dyes on ABWS-800 was suppressed clearly by Na_2SO_4 . The study indicates that ABWS can be a potential adsorbent for dye-bearing wastewater treatment. However, it is necessary to assess the reusability of ABWS. Meanwhile, granules or pellet can be made from the powder ABWS to improve its

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Conflict of Interest

The authors declare no conflict of interest.

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