

Sea Ice Detection and Monitoring Using UK TDS-1 GNSS-R Data

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Abstract

A sea ice detection algorithm developed using UK TDS-1 Global Navigation Satellite Systems (GNSS)-Reflectometry (GNSS-R) data over the Arctic and Antarctic regions is presented. It is based on detecting the coherence of the received GNSS reflected waveform or Delay-Doppler Map (DDM). Over the open ocean the scattered signal has a diffusive, incoherent nature; it is described by the rough surface scattering model based on the Geometric optics and the Gaussian statistics for the ocean surface slopes. Over sea ice, and in particular newly formed sea ice, the scattering is mostly coherent which is typical for a mostly flat surface. In order to measure the degree of coherence of the received waveform or DDM three different estimators are presented: the normalized DDM average, the Trailing Edge Slope (TES), and the matched filter approach. Here we present a probabilistic study based on a Bayesian approach using two different and independent ground-truth datasets. This approach allow us thoroughly assessing the performance of the estimators. The best results are achieved for both the TES and the matched filter approach with a probability of detection of 97%, a probability of false alarm of $\sim 2\%$, and a probability of error of 2.5%. However, the matched filter approach is preferred due to its simplicity. The measurement of the sea ice concentration is also assessed in this work, but the nature of the UK TDS-1 data (lack of calibrated data) does not allow us to make any specific conclusions about the sea ice concentration.

Index Terms

Sea Ice, coherent scattering, incoherent scattering, GNSS-R, UK TDS-1

I. INTRODUCTION

Global warming represents a growing concern for the society due to the drastic consequences it may have on our planet. One of its consequences is the melting of the Antarctic ice and the consequent rise of the sea level, which is a serious threat for all cities located near the coastline. One source of information to analyze climate models and evaluate the effects of global warming is the sea ice extent parameter, which is the area on the Arctic and Antarctic regions covered by sea ice. The rise of temperature will reduce the area covered by sea ice year after year, which is an early warning of a forthcoming bigger problem: the polar ice caps melting. Active and passive techniques have been used to monitor sea ice. Passive techniques based on microwave radiometry have been used to determine the Sea Ice Concentration (SIC) parameter, which is the percentage of ice on a pixel [1]. For instance 0% indicates open water, 50% indicates that half of the pixel is covered by ice, and 100% indicates that the whole pixel is solid ice. Active techniques based on real aperture radar and synthetic aperture radar generally measure surface roughness, which leads to sea ice type classification, as the

31 waveform shape is highly sensitive to surface roughness. However, in order to achieve a high resolution the
 32 frequency band used is normally Ku-band or K-band (12-18 GHz and 18-26 GHz respectively), which makes
 33 the radar technique sensitive to small (\sim cm) and large (\sim m) scale roughness.

34 The idea of using GNSS signals of opportunity for remote sensing purposes first was discussed in the late 80s
 35 [2]. One of its direct applications is the use GNSS reflected signals for mesoscale altimetry, as proposed in 1993
 36 with the PAssive Reflectometry and Interferometry System (PARIS) concept [3]–[5]. It is a passive technique,
 37 as it uses the GNSS signals already transmitted by satellites for navigation purposes, and only a receiver is
 38 needed. In 2000, initial results comparing the waveform peak power of the GNSS reflected signals over ice
 39 against RADARSAT back-scattering echoes were presented [6]. In 2003, a theoretical model explaining the sea
 40 ice scattering was proposed [7]. In 2006, it was shown that there is a strong presence of the coherent component
 41 in the GNSS-R bistatic scattering echoes [8], indicating a deficiency of a purely diffusive scattering model.
 42 This was confirmed in 2010 with a detailed study using United Kingdom Disaster Monitoring Constellation
 43 (UK-DMC) GNSS-R dataset [9]. However, unambiguous relations between waveform peak power or shape and
 44 sea ice parameters have not been found. Airborne studies using GNSS-R data were also performed in 2010 for
 45 the determination of sea ice parameters. Also, the effect of surface roughness was analyzed and compared to
 46 lidar measurements [10].

47 In this work we propose and demonstrate the use of GNSS reflected signals for sea ice detection with simple
 48 and straightforward algorithms that can be implemented on future space-borne platforms. Section II shows
 49 the theoretical background that justifies the analysis performed along the entire work. Section III describes
 50 the approach followed based on the experimental evidence from UK TDS-1 mission. Section IV describes the
 51 ground-truth used to validate the analysis performed. Section V evaluates the GNSS-R approach against the
 52 available ground-truth. Section VI discusses the results achieved, the error sources, and the applicability of the
 53 techniques proposed. Finally, section VII presents the conclusions of this work.

54 II. THEORETICAL BACKGROUND

55 Conventional satellite radar altimetry was used for the sea ice studies long ago [11]. It relies on scattering
 56 of EM waves from the surface while the radar antenna is looking strictly at nadir. In that situation, the power
 57 waveform or returned power as a function of the delay is composed of three distinct components [11]–[13]:

$$W(\tau) = S_r(t) * P_{FS}(t) * r(t), \quad (1)$$

58 where $S_r(t)$ is the shape of the transmitted pulse or point target response, $P_{FS}(t)$ is the flat surface response,
 59 which is the radar cross-section as a function of the delay time (over the horizontal surface) weighted by the
 60 gain pattern, and $r(t)$ characterizes the surface roughness, and it is the mean density of point scatterers as
 61 a function of the delay time. In other words, $S_r(t)$ is a Doppler cut of the so-called Woodward Ambiguity
 62 Function (WAF) [14] through its maximum. $P_{FS}(t)$ depends on the antenna pattern and the radar cross-section,
 63 which at the same time depends on the probability density function of the surface's slopes. It determines
 64 the trailing-edge shape of the waveform while it affects also the leading-edge shape. Then, $r(t)$ characterizes
 65 generally the surface roughness parameter, and it is the main contributor to the leading-edge shape while it
 66 does not affect so severely the trailing-edge.

67 In the case of conventional GNSS-R (cGNSS-R) for the public C/A signal the equivalent radar pulse width is
 68 approximately 300 meters (1 chip). This means that, unless there is a significant variation of surface topography,
 69 Eqn. (1) can be approximated by Eqn. (2):

$$W(\tau) = S_r(t) * P_{FS}(t), \quad (2)$$

70 as the radar pulse width is much larger than the immediate *rms* elevations. Note that a nadir-looking geometry
 71 is a particular case of the forward-scattering mechanism found in GNSS-R, and consequently, part of the
 72 previous work done for altimetry can be used. In that direction, this waveform model is a particular case of
 73 the waveform/DDM model proposed by Zavorotny and Voronovich in 2000 [15] for determining the shape of
 74 the rough ocean scattered signals:

$$W(\tau, f_D) = T_c^2 \int \frac{|r(\vec{\rho})|^2 D^2(\vec{\rho}) \Lambda^2(\tau - (R_r(\vec{\rho}) + R_t(\vec{\rho})) / c) q^A(\vec{\rho})}{4R_r^2(\vec{\rho}) R_t^2(\vec{\rho}) q_z^4(\vec{\rho})} |S(f_D(\vec{\rho}) - f_c)|^2 P\left(-\frac{q_\perp(\vec{\rho})}{q_z(\vec{\rho})}\right) d^2\rho \quad (3)$$

75 where T_c stands for the coherent integration time, r for the Fresnel reflection coefficient, the WAF is approxi-
 76 mated by a triangular function Λ in the time domain and by a sinc function S in the frequency domain, q stands
 77 for the scattering vector, ρ is a vector from the specular reflection point to the scattering point, R_r is the distance
 78 between the scattering point and the receiver, R_t is the distance between the transmitter and the scattering point,
 79 q_z is the vertical component of the scattering vector, q_\perp is the absolute value of the x,y components of the
 80 scattering vector, and $P(\vec{v})$ is the probability density function (*pdf*) of the surface slopes. Note that this model
 81 is based on the Kirchoff-Approximation Geometric-Optics (KA-GO), like Eqn. (1), and only takes into account
 82 the non-coherent component, assuming that the coherent component is negligible. Equation (3) can be expressed
 83 in a simplified form as in [16]–[18]:

$$W(\tau, f_D) \triangleq |\chi(\tau, f_D)|^2 ** |\sigma^0(\tau, f_D)|^2, \quad (4)$$

84 where f_D takes into account the power spreading in the Doppler domain, χ stands for the WAF, σ^0 for the
 85 normalized bi-static radar cross section which includes already the antenna pattern projection over the surface,
 86 the distance parameters, and the surface parameters such as the *pdf* of the surface slopes, and $**$ expresses a
 87 convolution in both domains τ and f_D . Taking a cut over the Doppler domain, which results in the so-called
 88 waveform, makes Eqn. (2) and (4) equivalent. In both altimetric and GNSS-R models, only surface scattering is
 89 taken into account. However, in 2003 Wiehl et al. [7] proposed a model that takes into account the sub-surface
 90 reflection that may occur on the ice sheets, converting Eqn. (4) into a triple convolution which can be expressed
 91 as:

$$W_v(\tau, f_D) = Z(t) * W(t, f_D), \quad (5)$$

92 where Z models the subsurface scattering or the power echo from each different ice layer, and W is the DDM
 93 model shown in Eqn. (4).

94 Although the theoretical models were proposed, no experimental cGNSS-R waveforms obtained from space
 95 were available until 2005 with the launch of the UK-DMC satellite [8]. Therein, it is observed that the waveforms

96 reflected from the ocean surface and from the sea ice were significantly different. While over the ocean there
 97 was a noticeable Delay-Doppler spreading of the signal power scattered leading to the “horseshoe” shape, the
 98 DDM over the sea ice resembled the WAF itself, without a Delay-Doppler spreading. Furthermore, for several
 99 regions the phase of the reflected signal at the DDM peak could be tracked, even identifying the navigation bits,
 100 which indicates the presence of a strong coherent component [8]. This experimentally demonstrated that the
 101 assumption of a negligible coherent component is mostly valid for the sea surface, but not for sea ice scattering.
 102 In Fig. 2 of [19] this fact was conceptually illustrated for near-normal incidence angle, and the near-normal
 103 incidence scattering cross section for the coherent and incoherent components were computed. Therein, it is
 104 seen that the *pdf* of the slopes is much narrower for the sea ice than for the open sea, tending to a δ -function
 105 centered at 0 for new ice, which means that the surface is perfectly flat and only coherent scattering occurs.
 106 The transition to an almost flat surface cannot be done within Eqns. (3)-(5). The use of the slope probability
 107 function in the form of a delta-function in these equations would lead to a wrong result. The coherent form of
 108 the DDM should be based on the original Kirchhoff approximation for the scattered field under the assumption
 109 that the surface roughness is very small (the Rayleigh parameter is significantly less than 1). The DDM model
 110 for the coherent component was introduced in [20]. Instead of a convolution, as shown in Eqn. (4), it is a
 111 product between the WAF and the surface reflectivity, times the factor that takes into account the loss of the
 112 spatial coherence due to the presence of some relatively weak surface roughness (Rayleigh parameter) [21],
 113 [22].

114 A deeper analysis of the sea ice signals scattered using the UK-DMC data was presented in [9], where
 115 again the waveforms’ shape indicated the presence of a coherent component. While the coherence seems to be
 116 temporal with some fading, which means that the waveform peak value was quite constant with some fading
 117 events, the coherent component dominates when the waveforms are incoherently summed. Therein, no clear
 118 relations between waveform’s observables and sea ice parameters were demonstrated in [9]. Furthermore, very
 119 few public data were released from the UK-DMC mission, which reduces significantly the possibility of an open
 120 data analysis, and it is one of the reasons why no specific conclusions could be made from the UK-DMC dataset
 121 about the sea ice concentration, or other ice characteristics. The nature of the United Kingdom TechDemoSat-1
 122 (UK TDS-1) data (lack of calibrated data) does not allow us to make any specific conclusions about the sea
 123 ice concentration. Nevertheless, this space experiment provides a preliminary demonstration of the potential of
 124 GNSS reflectometry over sea ice.

125 III. GNSS-R APPROACH

126 A. The “K-shape” DDM Concept

127 After analyzing several datasets from UK TDS-1 it has been seen that the shape of the measured DDM is
 128 different depending on the surface the GNSS signal was reflected on. Figure 1 shows two different extracts of
 129 the data retrieved from February 19th 2015 using the receiver specifications identification number RD000019,
 130 and the tracklist identification number TD000071. Those two figures correspond to data from the northern
 131 hemisphere (Arctic), and their spatial distance is below 60 km, as there is only 10 seconds difference among
 132 their acquisition. In Fig. 1(a) it is possible to see, on the left, the DDM over a sea ice covered surface. Particularly,
 133 the distribution of the power in the DDM resembles the shape of the letter “K” (rotated 90°). Therein, it is

134 possible to identify two different features. One of them is the vertical element of the “K” (horizontal line on
135 the image), stretching along the Doppler frequency axis and depicting a partially-coherent DDM component. It
136 corresponds to the WAF multiplied by the reflectivity, times second-order coherence function. The rest of the
137 DDM, which spans over the Delay-Doppler domain with the “horseshoe” shape, corresponds to the incoherent
138 component. For that particular DDM, that region has power levels similar to the WAF Doppler sidelobes,
139 which are at least 13 dB below its maximum, indicating that the coherent component was the main scattering
140 mechanism. On the right hand side of Fig. 1(a) the Doppler Integrated Waveform (DIW) in blue, a Doppler cut
141 of the WAF in cyan, and a Doppler cut of the DDM in green are shown. The DIW is the integral of the DDM
142 over the Doppler domain. This is a way to see the power spreading due to surface roughness but only in one
143 dimension (the Delay domain). Without doing that, the spreading of the power over the delay domain is barely
144 noticeable, as can be seen on the Doppler cut shown in the same figure in green. In Fig. 1(a) it is possible
145 to see that the leading edge is not affected by surface roughness due to the large pulse width of the GNSS
146 signals and the low roughness conditions. Also, due to the integral over the delay domain, the thermal noise
147 below the leading-edge is averaged and reduced, showing the incoherent scattered power that could be barely
148 seen on the conventional waveform (green)¹. On the contrary, Fig. 1(b) shows a totally different effect. Therein,
149 only the “horseshoe” shape of the DDM is seen and the WAF Doppler sidelobes are not present anymore.
150 Also, even though the “horseshoe” shape of the DDM is an indicator of the surface roughness, the shape of
151 the waveform’s leading-edge is barely affected. Differently, the trailing-edge of the DIW is very different. In
152 Fig. 1a there are two different regions on the trailing-edge, one where the slope is very large and follows the
153 WAF shape (associated to the coherent component), and one where the slope is smoother and corresponds to
154 the incoherent power. In Fig. 1(b) there is only one smooth region that can be identified which indicates the
155 lack of coherent power, as there is no power drop after the WAF Delay decay.

156 These indicates two different scattering mechanisms that affect the scattering over sea ice or open water.
157 When the reflection is purely coherent, there is no Delay-Doppler spreading and the reflected waveform is the
158 WAF multiplied by the power Fresnel reflection coefficient. If the reflection is purely incoherent, there is a
159 large Delay-Doppler spreading. The spreading depends on the roughness and in particular on the *pdf* of the
160 slopes. It might be logical that when the reflection has a coherent part and a non-coherent part, the waveform
161 is a linear combination of both models, as shown in Fig. 1(a). The more coherent, the more it will tend to the
162 coherent model, and the more incoherent, the more it will tend to the model in [15]. The combination of both
163 models tends to the “K-shape” DDM model. Furthermore, an inversely-proportional relationship was observed
164 between these two components: the larger the coherent component, the smaller the incoherent one, and vice
165 versa.

166 It has been theoretically [15] and empirically [8], [23] demonstrated that under open ocean conditions,
167 even at weak winds, the surface will be rough, and the coherent component will be negligible [15]. On the
168 other hand, there is no correct theoretical model that matches the waveforms obtained from the sea ice. The

¹The Doppler domain integration of the DDM is only needed sometimes for GNSS-R spaceborne data, as due to the geometry and the platform’s relatively high speed, the power is spread largely on the Doppler domain. Note that the Global Positioning System (GPS) satellite effective speed is much smaller than the platform’s effective speed. For the airborne case, as the platform’s speed is much lower, the Doppler spreading is not as large as the spaceborne case, and the waveform shows all the sensitivity to surface roughness on the trailing edge slope [15], without the need of a Doppler integral. Note that the slope of the DIW was proposed as an indicator of the ocean’s *ms* [15].

169 coherent component can be introduced into the non-coherent model in two different ways. The first one, as
 170 aforementioned, could comprise of a bistatic radar equation (3) as a DDM incoherent part plus a separate DDM
 171 term which describes a coherent (or partially-coherent) component. The second one is to devise a single bistatic
 172 radar equation which would have, under the surface integral, a single combined bistatic radar cross section
 173 similar to that in [24]. The equivalent bistatic cross section will consist of a sum of two terms: one, the same as
 174 in Eq. (3) describing the incoherent diffuse scattering, and another, describing the coherent reflection from the
 175 flat component of the surface. Formally, this can be done, and previously this approach was used for simulating
 176 the coherent and incoherent received scattered power under the bistatic geometry for soil moisture monitoring
 177 purposes [25], [26]. However, it makes the combined bistatic radar cross section distance and antenna parameters
 178 dependent. It makes this approach at odds with a traditional definition of the radar cross section which should
 179 only be a surface dependent parameter.

180 *B. Definition of the GNSS-R Observables*

181 There are several approaches that have been used up to now in order to match simulated GNSS-R data with
 182 real data in order to retrieve the geophysical parameters. One of the most common is the waveform fitting [27]–
 183 [29], which consists of minimizing the cost function created using measured data and simulated one. This one
 184 has been widely used for the retrieval of wind-speed over the ocean. Other heuristic approaches have been used
 185 in order to infer the surface roughness, such as the Volume under the normalized DDM (V_{DDM}), or the area
 186 under the normalized waveform (A_{WF}) [30]. Furthermore, different heuristic approaches have been compared
 187 against the wind-speed over the ocean such as the DDM Average (DDMA), the DDM Variance (DDMV), the
 188 Allan DDM Variance (ADDMV), the Leading Edge Slope (LES), and the Trailing Edge Slope (TES) [31]. In
 189 [30] it was already stated the correlation between the (V_{DDM}), which can be seen as the DDMA for large a
 190 Delay-Doppler region, and the TES was 0.74.

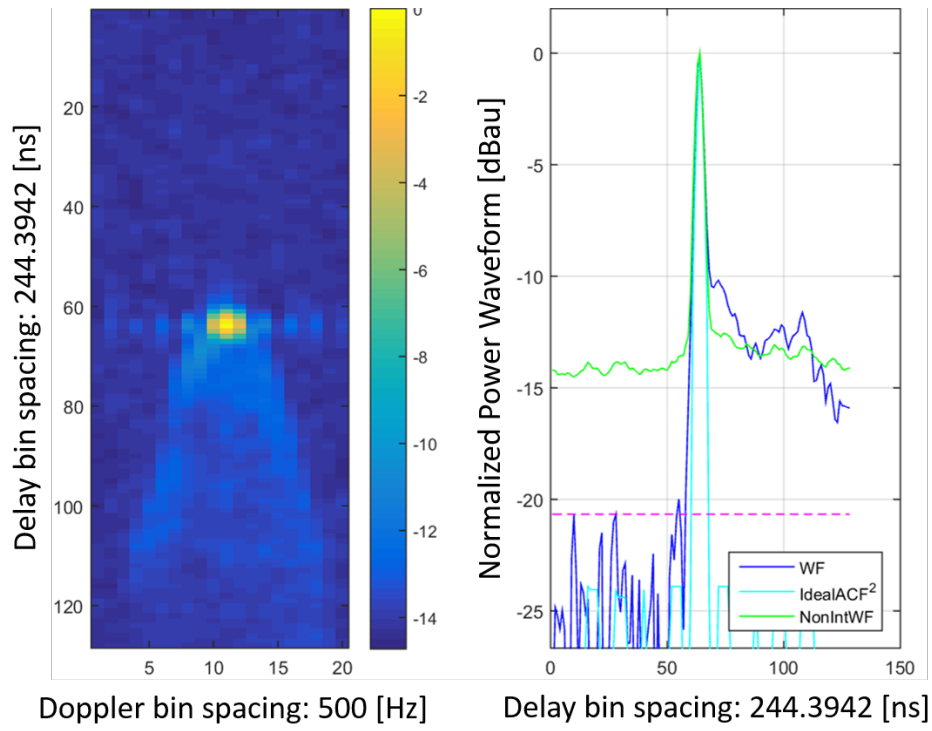
191 UK TDS-1 data are DDMs time-referenced and geo-located with a coherent integration time of 1 ms and
 192 an incoherent integration time of 1 s. In other words, there is no access to the 1 ms complex DDMs generated
 193 in the operation to obtain the 1 s incoherently integrated DDM. The delay bin is approximately 244 ns, and
 194 the Doppler bin is 500 Hz. Consequently, any operation that can be done among 1 ms coherently integrated
 195 complex DDMs, such as the DDMV or the ADDMV must be discarded. Furthermore, data from UK TDS-1 is
 196 not calibrated, as there is no information about the direct signal power impinging on the ground or about the
 197 signal power at satellite level. This excludes the use of parameters such as the Signal-to-Noise Ratio (SNR),
 198 as there the transmitted power depends on the satellite used and is not constant along time. Consequently, all
 199 DDMs retrieved from UK TDS-1 have been normalized to its maximum. So, the CYclone Global Navigation
 200 Satellite System (CYGNSS) approach to the wind-speed retrieval based on the signal power received cannot
 201 be applied to UK TDS-1 data.

202 The lack of a theoretical model for sea ice surface forward scattering at L-Band prevails us from applying
 203 the cost function approach. However, initially we will focus on detecting the coherency level of the scattered
 204 signal for determining the sea ice presence, so a comparison with the full coherent scattering model can be
 205 performed. The following three heuristic approaches will be used, which basically measure the peakedness of
 206 the WAF or its similarity to the coherent model:

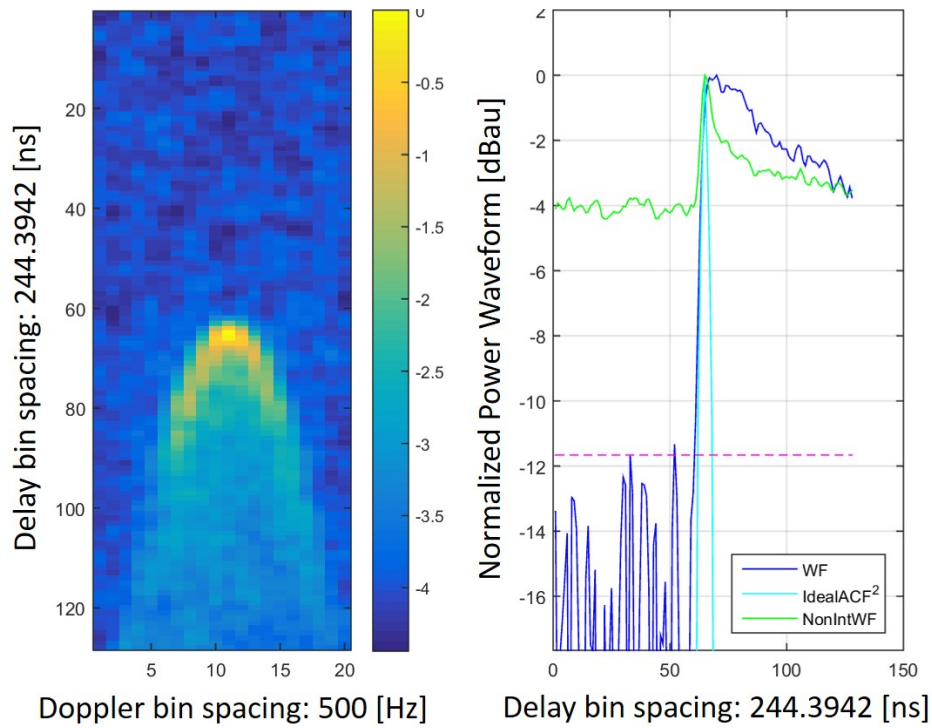
- 207 1) DDMA: it is the average value of the normalized DDM around its peak. For this analysis we have selected
208 3 different regions on the DDM.
- 209 • 3x3: 3 Doppler bin cells x 3 Delay bin cells
 - 210 • 3x5: 3 Doppler bin cells x 5 Delay bin cells
 - 211 • 3x7: 3 Doppler bin cells x 7 Delay bin cells
- 212 2) TES: it is the slope computed between the maximum of the normalized DIW and its value at different
213 delay bins. For this analysis we have selected 3 different versions.
- 214 • 3-bin: approximately 750 ns after the peak power.
 - 215 • 6-bin: approximately 1.5 μ s after the peak power.
 - 216 • 9-bin: approximately 2.25 μ s after the peak power.
- 217 3) Matched Filter (MF): also understood as correlation approach, it computes how similar are the unitary
218 energy DIW waveform is to the unitary energy WAF Doppler cut for the same satellite. It is an indirect
219 measurement of how coherent is the reflection process.

220 The results obtained with the LES estimator, were not satisfactory and are not present in this work. One of
221 the reasons is that at L-Band, as aforementioned, the waveform's leading edge is not as sensitive to surface
222 roughness as it is at higher frequency bands, such as Ku-band, or K-band, which are the frequency bands of
223 conventional altimeters, which also have much larger bandwidths. Furthermore, the higher the frequency used,
224 the more sensitive it is to small scale roughness [32].

225 Similar observables for sea ice detection and classification have been used in conventional altimetry such as
226 the SIGPK, which is the peak backscatter power in the returned echo, and the SIGTD, which is the average
227 power computed between eight early and eight late delay bins of the DIW [33]. Note, that the SIGTD is similar
228 to the DDMA approach and it is a measurement of the signal/waveform peakedness, or how much coherent is
229 the echo returned. Also note that the SIGPK cannot be used with UK TDS-1 data due to the lack of calibrated
230 data.



(a)



(b)

Fig. 1: Two DDMs and the corresponding waveforms for (a) sea ice and (b) open water regions.

IV. GROUND-TRUTH DESCRIPTION

231

232 In order to detect the presence of sea ice and compare it to the GNSS-R waveform shape, two different
 233 ground-truth SIC datasets have been used. The first one is the Arctic Radiation and Turbulence Interaction
 234 Study (ARTIST) Sea Ice (ASI) [1] algorithm using AMSR2 data. The second one is the Ocean and Sea Ice
 235 SAF (OSISAF) [34] which is computed using data from the different channels of the SSMIS sensor.

236 A. ASI Algorithm using AMSR2 Data

237 The ASI algorithm was originally developed to use the high resolution provided by the 85 GHz channel
 238 of the SSM/I sensor. Herein, it is applied to the AMSR2 data, which was launched on May 18th 2012. The
 239 AMSR2 is a multi-frequency microwave radiometer with channels at 6.93, 7.3, 10.65, 18.7, 23.8, 36.5, and 89
 240 GHz. The SIC is calculated from the polarization difference of the 89 GHz channel. The ASI algorithm is
 241 based on the polarization difference of the H and V channels ($P = T_{BV} - T_{BH}$). At 89 GHz the polarization
 242 difference for all types of ice is very small, either first-year, multi-year, or pure ice, whereas for open water
 243 it is much larger. By measuring this polarization difference, the presence of ice is determined. The SIC is
 244 determined by a linear model, which decomposes the polarization difference in the contribution from open
 245 water, and the contribution of sea ice. Both of them are multiplied by a term that depends on the SIC. The
 246 lower the polarization difference, the larger the SIC and vice versa. Using this model a third degree polynomial
 247 is finally fitted to obtain the SIC as a function of the polarization difference. However, the 89 GHz frequency
 248 band is highly prone to atmospheric effects. Even though they have a poorer resolution, the lower frequency
 249 channels of the AMSR2 data are used to assess the quality of the retrievals obtained from the 89 GHz channel,
 250 taking into account atmospheric effects and discard data without a sufficient quality. The SIC maps² used as
 251 a ground-truth for the analysis developed along this work are obtained from [35]. For more information about
 252 the ASI algorithm the interested can refer to [1].

253 B. OSI SAF Data

254 The OSISAF algorithm is based on the combination of the data provided by the different channels of the
 255 SSMIS radiometer, in particular the 19 GHz, the 37 GHz, and the 91 GHz. The combination is generally
 256 performed using a Bayesian approach. Generally, the 91 GHz channel provides the high resolution (12.5 km x
 257 12.5 km), and the other channels are used to compensate atmospheric factors as was done with the AMSR2 data.
 258 The retrieval algorithm is also based on the polarization difference between the V and H channels. However,
 259 in this algorithm the other channels are used in the model, and not only for quality assessment, resulting in a
 260 smoother transition between the open water and SIC larger than 80%. The SIC maps³ used as a ground-truth for
 261 the analysis developed along this work are obtained from [36]. The OSISAF dataset provides other information
 262 apart from the SIC maps, such as the sea ice edge, and the ice type. In order to develop those products
 263 also data from ASCAT scatterometer is used.

²Those maps are given in the polar stereographic coordinates for both hemispheres (Northern and Southern) using a grid resolution of 6.25 km. This implies that the GNSS-R data is converted into those coordinates in order to make the appropriate comparisons.

³Same than previous maps using a grid resolution of 10 km.

V. SEA ICE MONITORING USING UK TDS-1 DATA

As experimentally seen, the coherency level on the GNSS-R waveform is an indicator of the sea ice presence. In order to assess the performance of the proposed estimators, which basically measure the coherency level of the GNSS-R waveform, some intermediate steps have been performed to the GNSS-R data. First of all, all available UK TDS-1 data with a latitude larger than 50° for the Northern hemisphere, and lower than -50° for the Southern hemisphere were downloaded. For that dataset, only those DDMs with a thermal SNR larger than 0 dB were used, as lower SNR indicates that the DDMs do not have a good quality. In previous analysis of UK TDS-1 data this parameter was even more restrictive (3 dB minimum SNR required) [37]. However, as UK TDS-1 orbit and GPS constellation were not designed to monitor polar areas, it is decided to lower this constrain as otherwise the dataset becomes very limited.

Regarding the ground-truth, the data has been split in Arctic and Antarctic regions, and the two different ground-truth datasets used, which leads to four different analysis. Also, a pixel has been considered as an ice pixel if the SIC value is larger than 5%. The pixel correspondence between the GNSS-R data and the ground-truth has been performed by a minimum distance algorithm between the geo-located GNSS-R data and the ground-truth grid. A landmask was applied to avoid land contaminated pixels on the data analysis.

A. Performance Evaluation of the Estimators proposed

Taking into account the previous assumptions, the sea ice detection performance for the different proposed estimators has been evaluated through a Bayesian approach. The *pdf* of the ice pixels and the open water pixel were computed and the threshold to determine the presence of ice was chosen using a maximum likelihood criterion, assuming no a priori information about the pixels content [38]. This means that the probability of having an ice pixel or an open water pixel, in the whole dataset, is assumed to be equal. Figure 2 shows the *pdf* of the estimators proposed for the Northern hemisphere using the AMSR2 dataset as ground-truth. Figures 2(a)-(c) show the performance of the DDMA algorithm for the three different approaches selected, using 3 Doppler bins and 3, 5, and 7 Delay bins. As it can be seen, the three of them look like very equal, and as the delay bins used increase, the threshold decreases. What occurs with this algorithm is that the smaller the area computed, the more similar to the WAF the reflected signal is. If the reflection is incoherent, then the reflected signal does not drop so quickly and the normalized DDMA increases. Figures 2(d)-(f) show the performance of the TES algorithm. In this case, the sharper the slope, the more more similar to the Doppler cut of the WAF the DIW is. Consequently, ice values appear on the right whereas with the DDMA they appeared on the left. Qualitatively, this estimator seems to perform better than the DDMA in each of its three different versions. Finally, the matched filter approach is shown in Fig. 2(g). Herein, it is possible to see that the *pdf* looks narrower and sharper than with previous estimators. Qualitatively, it seems to be the best estimator to distinguish between sea ice or open water.

The same operation has been performed for the OSISAF dataset, and for both ground-truth over the Antarctic region. The *pdfs* obtained are similar to the ones shown in Fig. 2, showing a similar behavior, which shows that the algorithms performed in the same way independently from the data nature. In order to summarize the results obtained and evaluate quantitatively the performance of all the estimators proposed, Tab. I is shown. Therein, four parameters are computed for each ground-truth available (OSISAF and ASI AMSR2), and each region

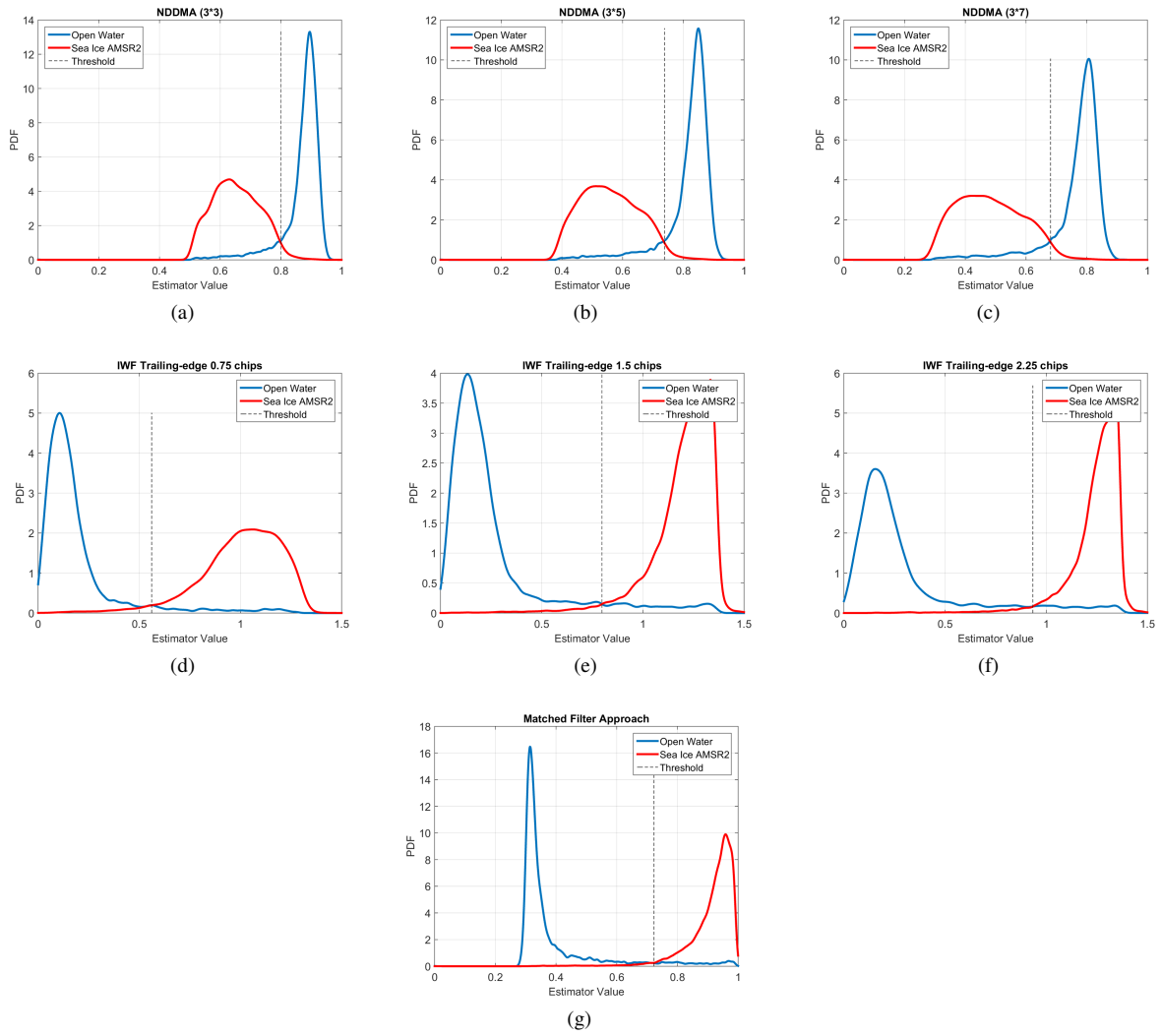


Fig. 2: Estimators performance for the Northern hemisphere using the AMSR2 dataset. (a) Normalized DDMA 3x3, (b) Normalized DDMA 3x5, (c) Normalized DDMA 3x7, (d) TES 750 ns, (e) TES $1.5\mu\text{s}$, (f) TES $2.25\mu\text{s}$, (g) Matched Filter.

302 (Arctic and Antarctic): the probability of detection (P_d), the probability of false alarm (P_{fa}), the probability of
 303 error (P_e), and the threshold selected [38].

304 In general, it is possible to see that, independently from the algorithm used, for any region and any ground-
 305 truth dataset, the P_d is larger than 95%, reaching larger values for the ASI AMSR2 ground-truth. However,
 306 for that dataset, the P_{fa} is also larger. In the end, there is always a compromise between the P_d and P_{fa} , and
 307 consequently, the larger the probability of detection, the larger the probability of false alarm. Note that the
 308 estimators with the worst performance, which is evaluated by the probability of error, are the ones based on the
 309 DDMA. However, those ones are consistent and independent from the ground-truth and the region observed,
 310 as they all have a similar threshold. This occurs because the threshold is determined by the shape of the *pdfs*,
 311 and for those estimators they are closer and the slopes around the threshold are larger. On the other hand,
 312 the threshold for the other estimators is not as consistent. Looking to the *pdfs* presented on Fig. 2, they are

313 more separated than for the DDMA, and the slopes around the threshold are smaller. This means that, the
 314 threshold selection is not so important, and the Pd and Pfa values will not change a lot by moving the threshold
 315 computed. Also note that the performance of the trailing edge estimators and the matched filter approach is
 316 similar. However, the matched filter approach seems to be less sensitive to the threshold selection just by
 317 qualitatively explore the *pdfs*. Furthermore, the matched filter approach is the simplest one to be implemented
 318 as it only requires one Fast Fourier Transform (FFT) and one Inverse FFT (IFFT). For this reason, it is the
 319 approach preferred, as it can be easily implemented in a real-time processing software on-board the satellite,
 320 without the need of further algorithm intelligence. Finally, it is also remarkable that the results obtained using
 321 the OSISAF dataset as ground-truth are better than the ones using the ASI algorithm over AMSR2 data. The
 322 reason for that is that the first ground-truth uses a combination of different frequency bands, detecting features
 323 that are not detectable at close to 90 GHz, which is the unique frequency band used by the ASI algorithm.

TABLE I: Performance evaluation of the estimators proposed for Arctic and Antarctic regions as a function of the two different ground-truths used, the OSISAF dataset, and the ASI AMSR2 dataset.

	Estimators	Arctic				Antarctic			
		Pd	Pfa	Pe	Th.	Pd	Pfa	Pe	Th.
OSISAF	NDDMA (3*3)	0.9650	0.0308	0.0325	0.808	0.9499	0.0596	0.0544	0.816
	NDDMA (3*5)	0.9615	0.0346	0.0361	0.745	0.9481	0.0620	0.0566	0.756
	NDDMA (3*7)	0.9564	0.0407	0.0417	0.686	0.943	0.0630	0.0597	0.694
	TE (0.75 CA Chips)	0.9668	0.0189	0.026	0.416	0.9528	0.0460	0.0465	0.342
	TE (1.5 CA Chips)	0.9718	0.0212	0.0247	0.619	0.9642	0.0520	0.0439	0.466
	TE (2.25 CA Chips)	0.9723	0.0209	0.0242	0.753	0.9629	0.0496	0.0433	0.597
	MF	0.9740	0.0234	0.0247	0.583	0.9628	0.0536	0.0453	0.510
ASI AMSR2	NDDMA (3*3)	0.9735	0.1014	0.0634	0.800	0.9703	0.1425	0.0856	0.806
	NDDMA (3*5)	0.9732	0.1038	0.0648	0.738	0.9699	0.1415	0.0854	0.741
	NDDMA (3*7)	0.9697	0.1111	0.0702	0.681	0.9700	0.1467	0.0880	0.685
	TE (0.75 CA Chips)	0.9666	0.0600	0.049	0.561	0.9676	0.1281	0.0760	0.413
	TE (1.5 CA Chips)	0.9728	0.0697	0.0484	0.798	0.9765	0.1273	0.0754	0.661
	TE (2.25 CA Chips)	0.9709	0.0710	0.0500	0.934	0.978	0.1292	0.0756	0.768
	MF	0.9721	0.0671	0.0474	0.723	0.9731	0.1233	0.0750	0.627

324 B. SIC Maps from Ground-truth and GNSS-R data

325 Figure 3 shows the sea ice detection maps created from the GNSS-R data using the matched filter approach
 326 together with the SIC maps from the two ground-truths available for both the Arctic and Antarctic regions.
 327 Note that February 15th is the middle of the winter in the northern hemisphere, and the middle of the summer
 328 in the southern hemisphere, which is why the whole north pole has plenty of sea ice whereas the south pole has
 329 very few. In all maps, the presence of ice is determined by the purple color whereas the presence of open water
 330 is determined by the light blue color, which corresponds to the colorbar on the right of the figures. The gaps
 331 are due to data with thermal SNR lower than 0 dB or land contaminated pixels. In the same way, the SIC from
 332 OSISAF and ASI AMSR2 are scaled from 0% to 100%, with the 0% to the dark blue and the 100% to the dark
 333 red, which corresponds to the colorbar on the left of the figures. The coordinate system used to represent those
 334 maps is the polar stereographic coordinate system. Therein, it is seen how the transitions between open water
 335 and sea ice are monitored, and the change observed is very drastic, as expected from the *pdfs*. The sea ice

336 edge is perfectly detected using the GNSS-R data. Based on specular reflection theory, for the sea ice regions
 337 assuming coherent reflection, and using the TDS-1 satellite parameters, the spatial resolution is $\sim 6 \text{ km} \times 0.4$
 338 km, which is half of the SSMIS pixel in the along-track track direction.

339 Furthermore, note that GNSS-R data look like different transects. This is one of the properties of the multi-
 340 static GNSS-R techniques. Instead of being an image like a Synthetic Aperture Radar (SAR) or a microwave
 341 radiometer, it is a collection of transects with all the satellites in view. In order to generate a map with
 342 GNSS-R data interpolation is required. Herein, the interpolation approach has not been performed as the mission
 343 specifications do not allow to obtain sufficient points to generate a reliable map. However, a GNSS-R mission
 344 with the appropriate specifications to monitor the polar regions such as the one simulated in [20] would provide
 345 enough quality data to generate polar images.

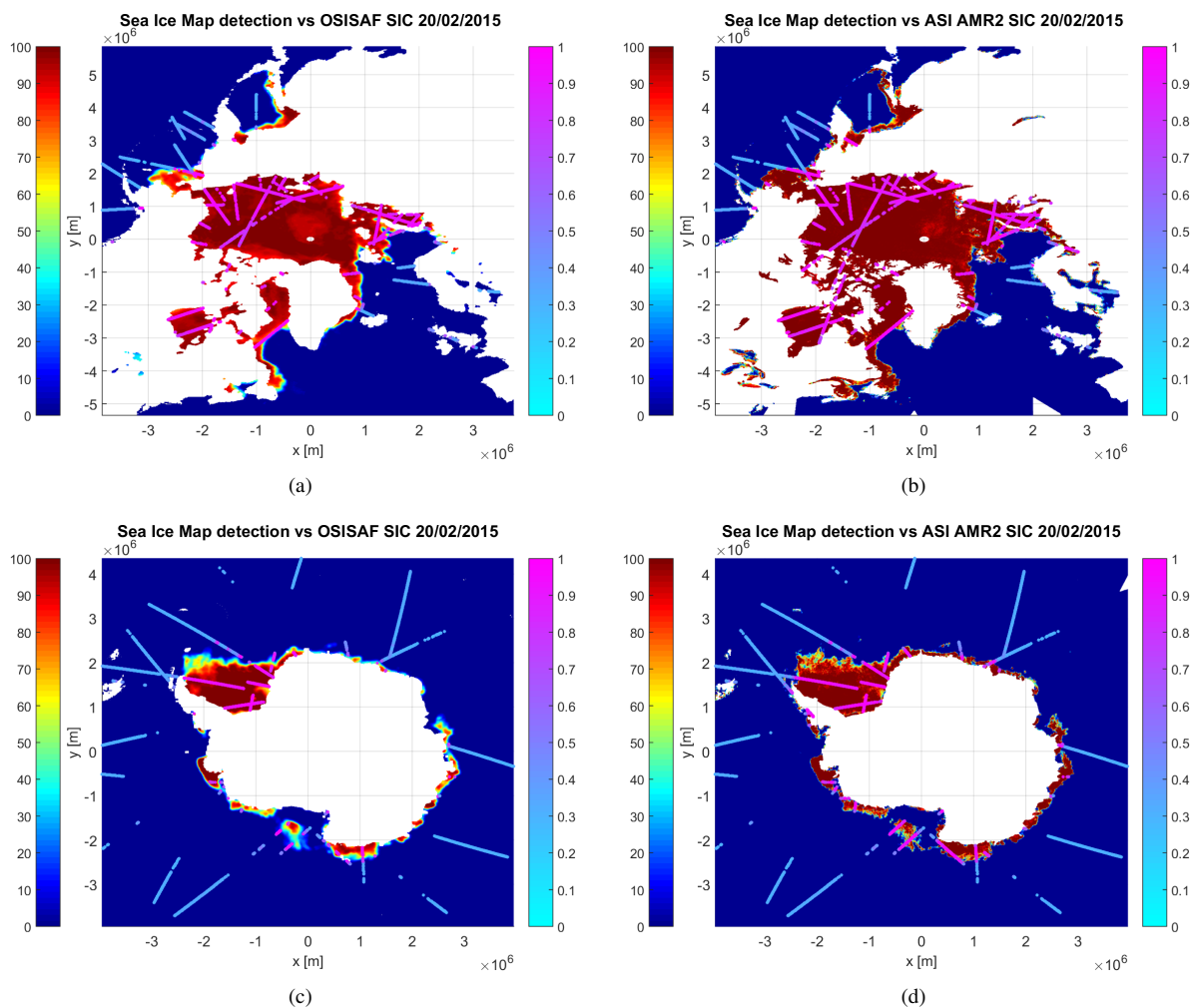


Fig. 3: Sea Ice Concentration Maps of February 20th 2015 from OSISAF and ASI AMSR2 of the northern and Southern hemisphere overlaid with the matched filter GNSS-R approach, (a) Arctic OSISAF, (b) Arctic ASI AMSR2, (c) Antarctic OSISAF, (d) Antarctic ASI AMSR2.

346 Figure 4 shows a similar image to Fig. 3, but in this case for November 15th 2014. Herein, the Arctic regions
 347 are less frozen than in February, as the freezing period has just started, whereas the Antarctic regions have
 348 plenty of sea ice as the melting process is just starting. Therein, again the transitions are monitored by the

349 GNSS-R data. Note that in the Antarctic there is a place close to the coast that has melted before the outer
 350 ice layer, and it is detected by the GNSS-R data. Also, note that for those images, there is much less GNSS-R
 351 data available. This is because the UK TDS-1 2014 dataset comes from the beginning of the mission whereas
 352 the 2015 comes from a more consolidated period of the mission. There is a gap in the GNSS-R data between
 353 November 23rd 2014 and January 26th 2015 as there was a Christmas break, and corrupted orbital parameters
 354 [39].

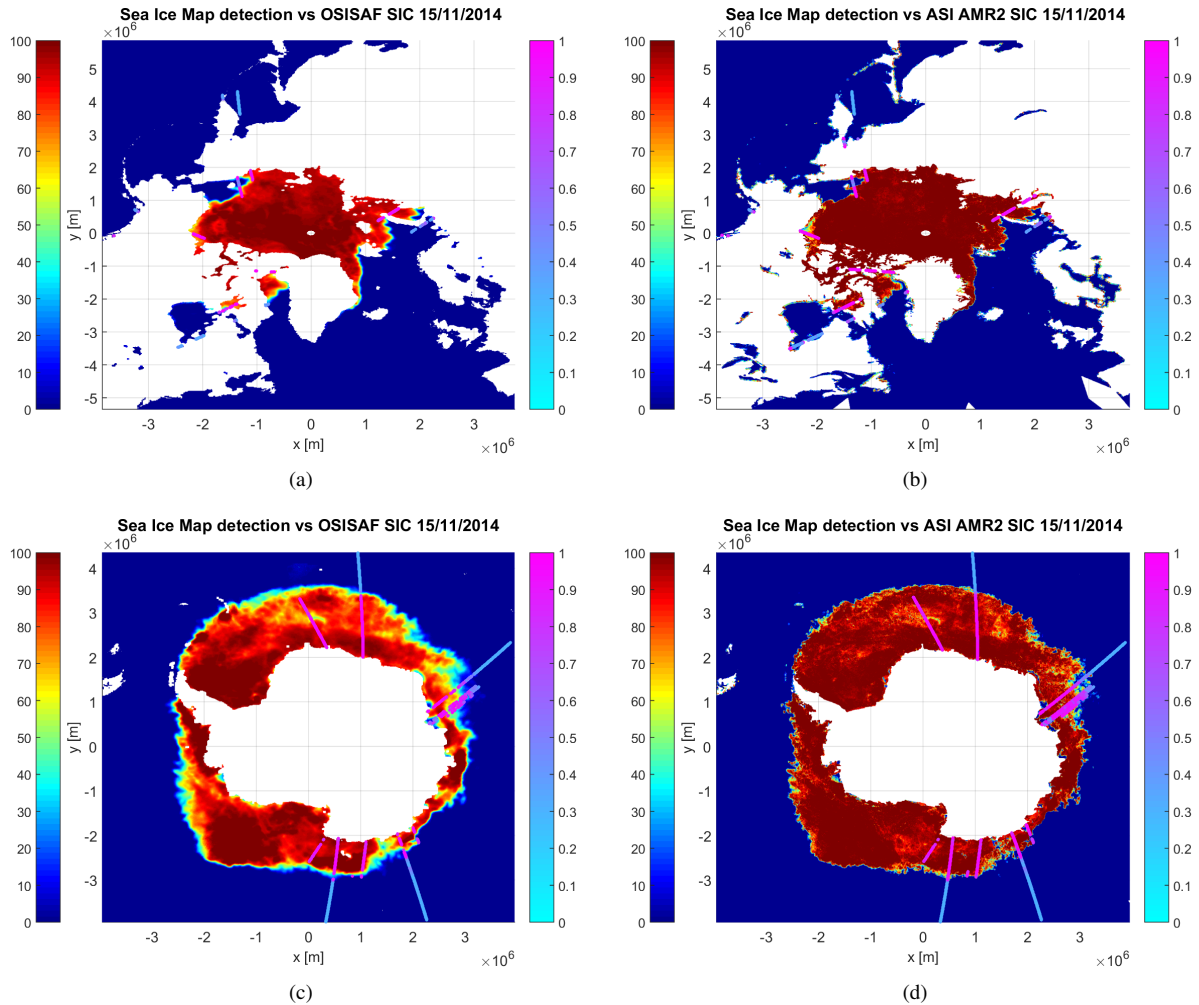


Fig. 4: Sea Ice Concentration Maps of November 15th 2014 from OSISAF and ASI AMSR2 of the northern and southern hemisphere overlaid with the matched filter GNSS-R approach, (a) Arctic OSISAF, (b) Arctic ASI AMSR2, (c) Antarctic OSISAF, (d) Antarctic ASI AMSR2.

VI. DISCUSSION

355
 356 A sea ice detection algorithm has been presented and justified through the sea ice scattering models available
 357 in the literature. Several estimators have been proposed to determine the sea ice edge and its performance
 358 evaluated through a Bayesian approach. Then, sea ice maps from the different ground-truths available have
 359 been shown with the GNSS-R matched filter approach overlaying them. Furthermore, it has been tried to go
 360 deeper and determine if the coherent GNSS-R waveform was sensitive to other parameters apart from the sea

361 ice presence, and therefore it could be used, for instance, for sea ice classification (first year, multi-year, or pure
362 ice [40]). Following the ice scattering coherent model, it would be expected to find the largest power received
363 when there is very low SIC, as the water is freezing and calmed (a property of new ice formation [19]), and
364 water has a very large dielectric constant. When the SIC increases, the equivalent dielectric constant is a mixture
365 of the ice one and water one, and as the dielectric constant of ice is much smaller than the water one, the
366 equivalent dielectric constant decreases, and so the reflected power or the reflected SNR. This brought to the
367 limit means that when the SIC is 100%, the coherent model would work but with a lower echo received. The
368 same reasoning applies to first year ice, whose dielectric constant is larger than multi-year ice, which at the same
369 time its dielectric constant is larger than the pure ice one. Conversely, no correlation was found between the
370 SNR received and the SIC. This might be interpreted as the GNSS-R is not sensitive to the SIC. However, since
371 UK TDS-1 data was not calibrated, and having a mixture of data from different satellites prevents to extract
372 any robust conclusion from the dataset used. This relation should be explored in the future with calibrated data.
373 Also, different roughness scales may apply to this analysis, making more difficult to obtain a clear relation.
374 CYGNSS mission will provide calibrated data, but its orbit, which was selected to monitor tropical cyclones,
375 will prevent from picking reflections from sea ice. In order to test this hypothesis data from the forthcoming
376 European Space Agency (ESA) GNSS rEfectometry, Radio Occultation and Scatterometry (GEROS) mission
377 will be needed. Furthermore, National Aeronautics and Space Administration (NASA) is leading a continuation
378 of the CYGNSS mission and new scientific challenges such as the SIC monitoring could be one of its goals,
379 as the melting of the poles and its consequent rise of the sea level is one of the major problems that concerns
380 the scientific/meteorological community.

381 Apart from that, herein, we have presented a methodology to detect the presence of sea ice based on the
382 coherency of the scattered signal. When it is coherent, the ground resolution of the GNSS-R data corresponds
383 to the First Fresnel Zone [41], [42], which is approximately 400 m x 400 m meters for a satellite at 650 km
384 altitude. Taking into account the satellite's speed (6 km/s) and 1 second of non-coherent integration, this leads
385 to a final ground-resolution of approximately 6 km x 0.4 km. This resolution is similar to the one achieved
386 by microwave radiometers working at 90 GHz, in the along track direction, and even better in the across-
387 track direction. Furthermore, the spatial resolution of coherent scattered GNSS signals is much better than
388 microwave radiometers working at the same frequency band (L-Band), such as Soil Moisture Ocean Salinity
389 (SMOS), Aquarius, and Soil Moisture Active and Passive (SMAP). This is a major point about this technique,
390 as technology is much cheaper at L-Band than at 90 GHz. Furthermore, L-Band is much less sensitive to
391 atmospheric effects than the 90 GHz frequency band [43], which means that less corrections are required.

392 One aspect that has not yet been discussed is the Pfa obtained by all the estimators, and the reasons why
393 a false alarm may be produced. The sea ice presence is determined by the coherency of the received signal,
394 which means that the reflected surface must be flat. In several of the datasets used we have realized that close
395 to the sea ice edges the GNSS-R data was detecting ice presence whereas the ground-truth had not yet detected
396 ice. The ground-truth used are SIC maps averaging several images of several radiometer orbits passes, and each
397 pixel data is not time referenced. However, the GNSS-R data it is time referenced. Several continuous data
398 observations showed that when ice was detected close to the ice edges by the GNSS-R technique, but not with
399 the radiometric data, the day after it was detected as an ice pixel by the radiometric data. This indicates that

400 either the OSISAF data and the AMSR2 data were obtained before the GNSS-R data, or that in the freezing
401 process (new ice generation) the water gets calmed before freezing, and the proposed GNSS-R technique detects
402 ice also when water is calmed.

403

VII. CONCLUSIONS

404 This work has presented a methodology to monitor and detect sea ice presence over the Arctic and Antarctic
405 regions using UK TDS-1 GNSS-R data. The detection is based on the analysis of the coherency of the measured
406 DIW or DDM, as when the reflection occurs over an icy region the scattering is mostly coherent whereas when
407 it occurs over open ocean it follows the incoherent model. Three different estimators with different properties
408 are used along the manuscript for the sea ice detection: the normalized DDMA, the TES, and the matched
409 filter approach. Among them, the matched filter approach is preferred as it classifies with only one number
410 between 0 and 1 if it is an ice pixel or an open ocean pixel. Furthermore, it is the one that requires less
411 computational cost and it can be implemented easily on the on-board processing. In order to assess the validity
412 of the algorithms proposed, two different ground-truth datasets have been used: the OSISAF dataset, and the
413 ASI algorithm over AMSR2 data. The best results are obtained for both, the TES in its three versions and the
414 matched filter estimator, over the Arctic region and using the OSISAF dataset as ground-truth, obtaining a Pd
415 of 97% and a Pe of approximately 2.5%.

416 The relation between the reflected power and the SIC could not be evaluated with the appropriate degree of
417 accuracy as UK TDS-1 GNSS-R data lacks of the measurement of the direct signal, which avoids obtaining
418 calibrated measurements. This means that only relative measurements as the ones performed can be used.
419 However, the encouraging results from this work open the door for future GNSS-R missions, as this GNSS-R
420 technique has the same ground-resolution than microwave radiometers at 90 GHz, being GNSS-R a much more
421 cost-effective technique and less sensitive to atmospheric disturbances. Unfortunately, the CYGNSS mission
422 that will be launched in 2016 will not be able to test these algorithms due to its orbit inclination (35°), but other
423 forthcoming GNSS-R missions such as GEROS, or the scientific committee of the CYGNSS follow-on may
424 take into consideration this new application of GNSS-R.

425

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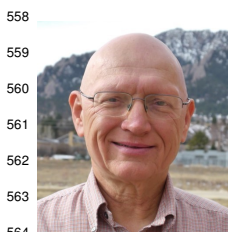
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