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EHF - 87 - 56

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EFFICIENCY OF A SIDE COUPLED LINAC

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EFFICIENCY OF
A LINAC \equiv SHUNT IMPEDANCE

$$\hookrightarrow ZT^2 = \frac{(\text{Energy gained by a part.})^2}{\text{Power dissipated}}$$

Cost $\propto \frac{1}{\sqrt{ZT^2}} \Rightarrow$ AIM OF A LINAC
DESIGN IS TO
MAXIMIZE THE
SHUNT IMPEDANCE

$$Z \propto \sqrt{p}$$

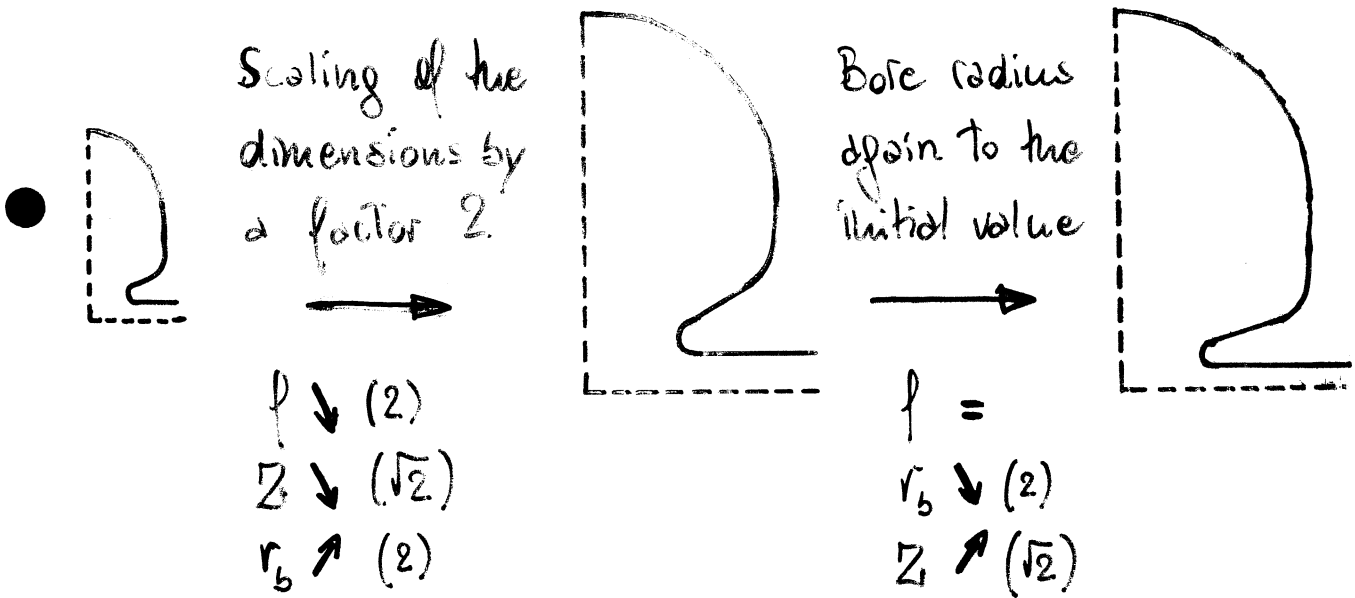
EFFICIENCY OF A LINAC AS
A FUNCTION OF FREQUENCY

$\left\{ \begin{array}{l} \text{- CAVITY DIMENSIONS} \propto \frac{1}{p} \\ \text{- SKIN DEPTH} \propto \frac{1}{\sqrt{p}} \end{array} \right. \Rightarrow$

$$\Rightarrow Z \propto \frac{1}{R_s} \propto \frac{\delta}{D} \propto \sqrt{p}$$

④ FIRST CORRECTION - BORE RADIUS

$$Z \propto \frac{1}{\sqrt{r_{\text{bore}} + 2r_{\text{nose}}}}$$



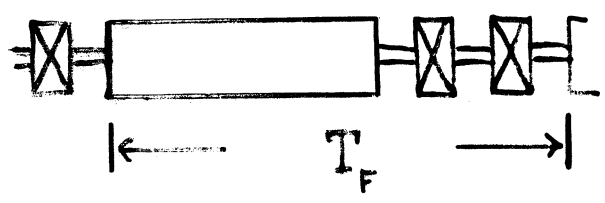
⇒ FOR A ^NCONSTANT BORE, THE EFFICIENCY OF A SIDE COUPLED STRUCTURE IS INDEPENDENT FROM THE FREQUENCY

BUT :

$$r_{\text{bore}} \propto r_{\text{beam}} \propto \sqrt{\frac{E_+}{f}} \Rightarrow \boxed{Z \propto f^{1/4}}$$

THE BORE HAS TO BE INCREASED TO TAKE INTO ACCOUNT THE INCREASED BEAM DIMENSIONS

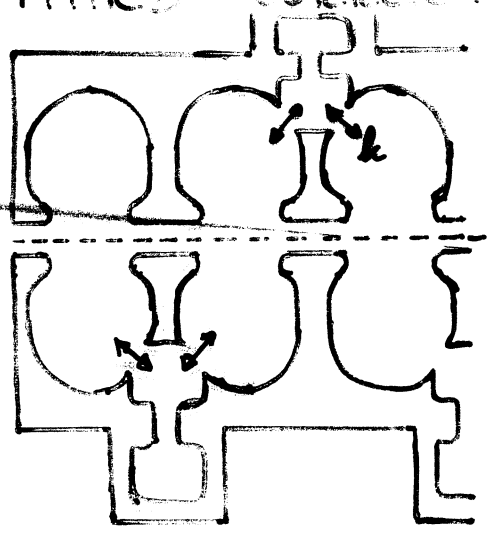
② SECOND CORRECTION - FOCUSING PERIOD



$$r_{\text{beam}} \propto T_F$$

REDUCING THE FOCUSING PERIOD IT IS POSSIBLE TO REDUCE THE BEAM SIZE (\Rightarrow THE BORE RADIUS)

③ THIRD CORRECTIONS - COUPLING



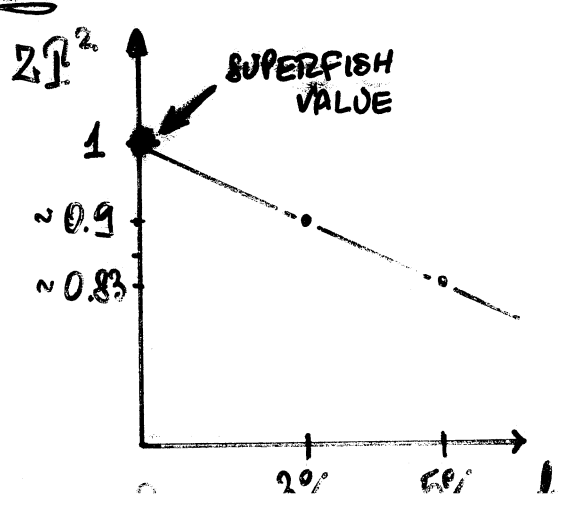
- GROUP VELOCITY
- STABILITY
- POWER FLOW DROP

$$\propto \frac{k}{N}$$

N = number of cells in a tank

\Rightarrow A REDUCED FREQUENCY ($\Rightarrow N \downarrow$) CAN ALLOW THE SAME TANK BEHAVIOUR WITH A REDUCED COUPLING

BUT:



$$Z \propto \frac{1}{\text{slot dimensions}} \propto \frac{1}{k}$$

A REDUCED COUPLING ALLOWS A HIGHER EFFICIENCY

EFFICIENCY OF A 600 MHz SIDE COUPLED LINAC COMPARED TO THE 1200 MHz SCL

- A. SHUNT IMPEDANCE OF THE 1200 MHz SCL $\rightarrow 2: 57.7 \text{ M}\Omega/\text{m}$
- B. SCALING THE CAVITIES DIMENSIONS BY A FACTOR 2 (TO GO TO 600 MHz) $\rightarrow 2^2: 40.8 \text{ M}\Omega/\text{m}$

● NEW BORE RADIUS :

$$\left. \begin{array}{l} r_{\text{beam}} \propto \sqrt{\epsilon_t / \rho} \uparrow \\ \text{tank's length} \downarrow \end{array} \right\} \rightarrow r_{\text{bore}} \uparrow$$

 (1 cm \rightarrow 1.2 cm)

D. REDUCTION OF THE COUPLING FACTOR BETWEEN CELLS

5% \rightarrow 3%

\Rightarrow THE SAME SHUNT IMPEDANCE AS AT 1200 MHz

EVERYTHING OK ?

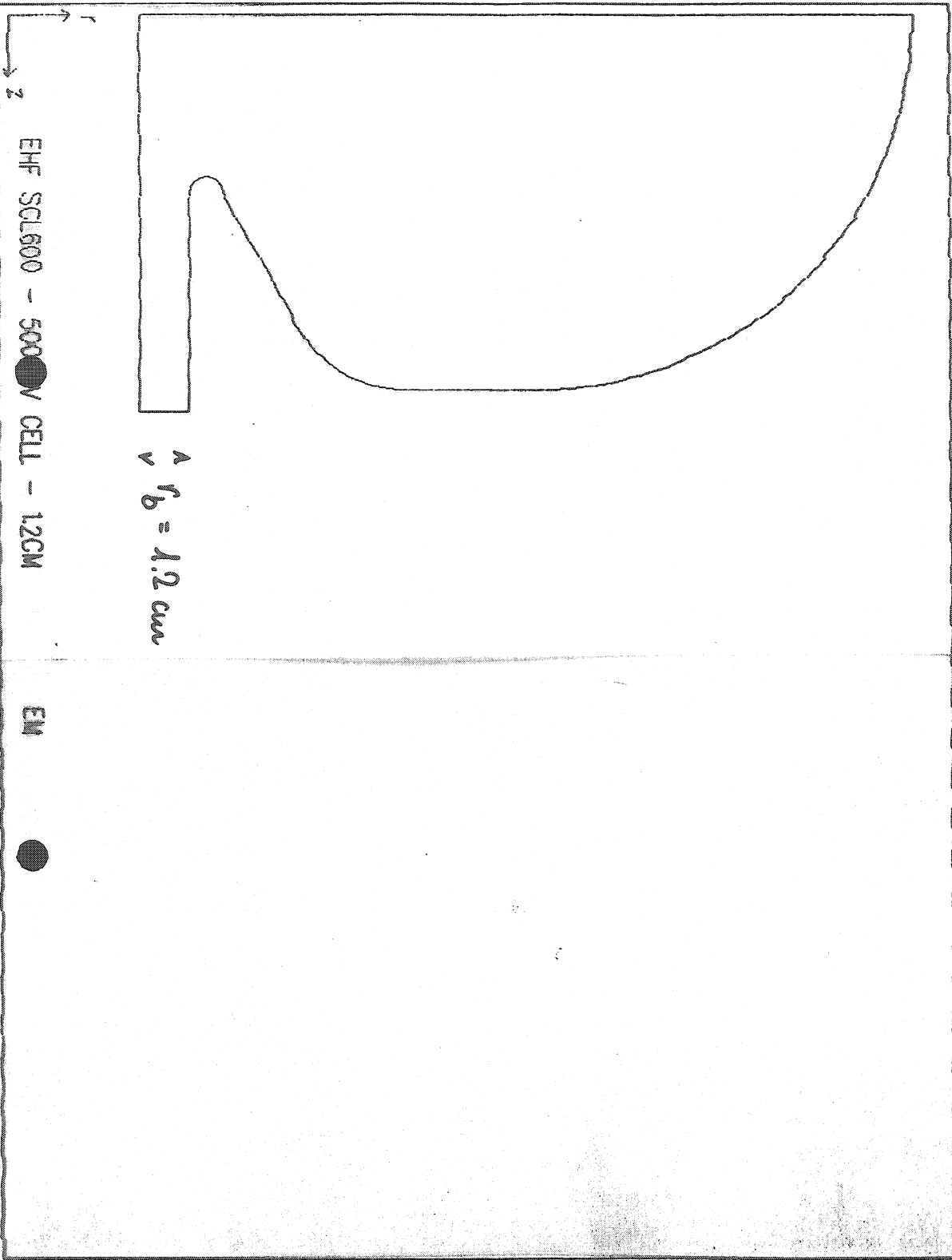
PEAK FIELD :

$$\left. \begin{array}{l} \frac{r_{\text{bore}}}{L} \downarrow \rightarrow \frac{g}{L} \downarrow \Rightarrow \frac{E_p}{E_0} \uparrow \Rightarrow E_p \uparrow \\ \text{Kilpatrick field } E_k \downarrow \text{ (22 MV/m at 600 MHz)} \end{array} \right\} \rightarrow$$

$$E_0 \text{ is kept the same} \downarrow$$

\Rightarrow A RELEASED DESIGN OF THE NOSES IS NEEDED

THIS PROVIDES ABOUT THE $2T^2$ TO 596 $\text{M}\Omega$

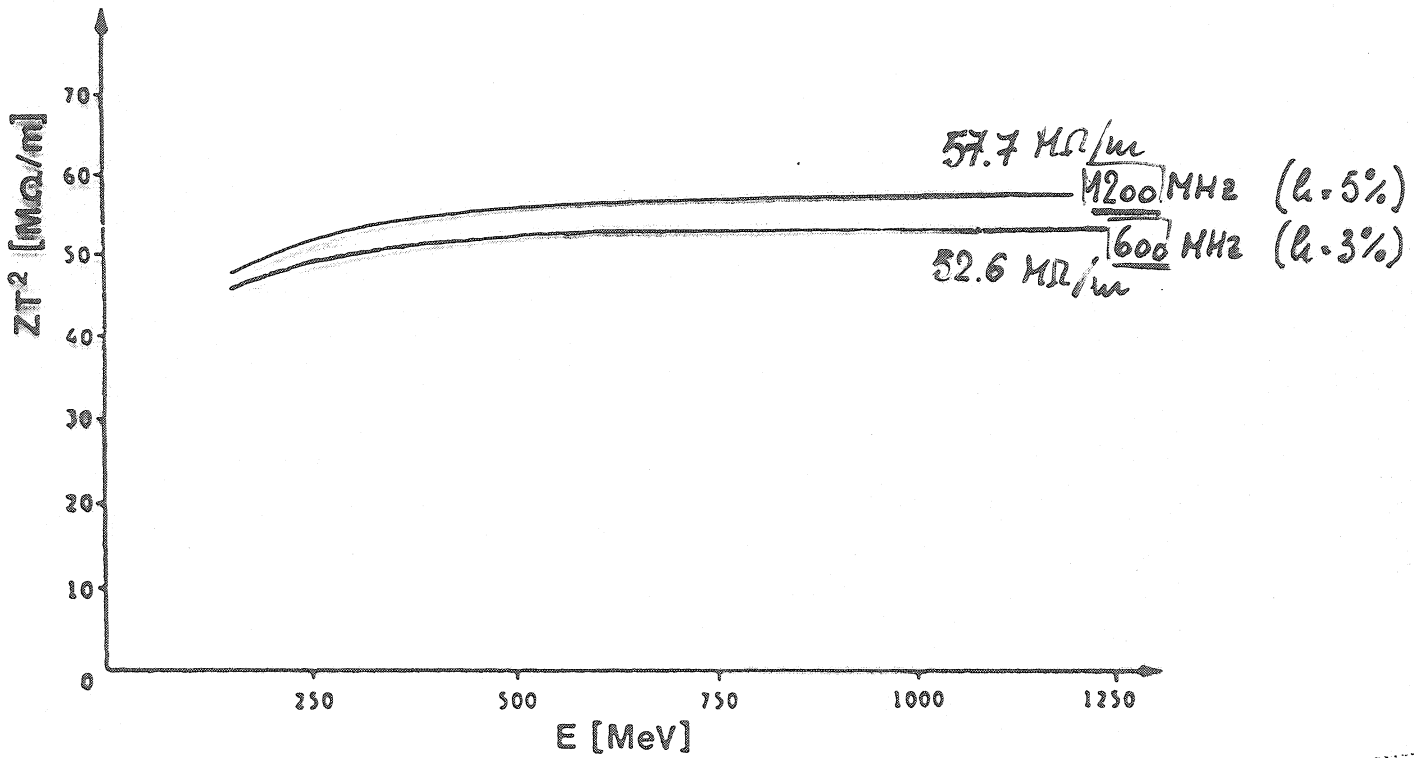


EHF SCL600 - 500V CELL - 12CM

$v_b = 1.2 \text{ cm}$

EM





④

Table 13.6: SCL - Table of Parameters

Input Energy	150	MeV	
Output Energy	1200	MeV	
Frequency	1200	MHz	600
Number of Modules	16		17
Number of Tanks	64		68
Number of Acc. Cells per Tank	38		18
Accelerating Field $E_0 T$	5.6-4.7	MV/m	
Peak Power	117	MW	125
Average Power	1.2	MW	1.25
Duty Cycle	1%		
Total Length	290.2	m	302.8
Synchronous Phase	-25°		
Beam Radius	0.4-0.25	cm	0.5-0.3
Norm. Transv. Emittance (RMS)	$\sim 0.6\pi$	mm.mrad	
Norm. Long. Emittance (RMS)	$\sim 4\pi$	deg.MeV	
Output Phase Spread	8°		5°
Output Energy Spread	2.7	MeV	1.8
Bore Hole Radius	1	cm	1.2
Ratio of gap/cell length	0.3-0.5		0.35-0.40
Accelerating Cell Radius	8.8-9.4	cm	~ 18.3
Real Eff. Shunt Impedance	47-58	MΩ/m	46.0 - 52.6
Transit Time Factor	0.89-0.85		0.93 - 0.88
Quality Factor	19-25	$\times 10^3$	~ 30
Peak Surface Electric Field	38-32	MV/m	40-33 (= 1.8-1.5 E_k)
Quadrupole Gradients	35-55	T/m	30-46
TANKS LENGTH	2.5-4.5	m	2.3-4.0

COST

40

MM

4.5

