

本レポートは、日本原子力研究所が不定期に公刊している研究報告書です。

入手の問合わせは、日本原子力研究所研究情報部研究情報課 (〒319-1195 茨城県那珂 郡東海村)あて、お申し越しください。なお、このほかに財団法人原子力弘済会資料セン ター (〒319-1195 茨城県那珂郡東海村日本原子力研究所内) で複写による実費頒布をお こなっております。

This report is issued irregularly.

Inquiries about availability of the reports should be addressed to Research Information Division, Department of Intellectual Resources, Japan Atomic Energy Research Institute, Tokai-mura, Naka-gun, baraki-ken T319-- 1195, **Japan.**

> © Japan Atomic Energy Research Institute, 2003 編集兼発行 日本原子力研究所

JAERI-Research 2003-004

A Systematics of Fission Product Mass Yields with 5 Gaussian Functions

Jun-ichi KATAKURA

Department of Nuclear Energy System Tokai Research Establishment Japan Atomic Energy Research Institute Tokai-mura,Naka-gun,lbaraki-ken

(Received January 29, 2003)

A systematics of fission product mass yields is proposed. The systematics is based on Moriyamna-Ohnishi systematics developed about 30 years ago. The parameter set of the systematics is newly determined by examining measured data taken after Moriyama-Ohnishi systematics was released. The systematics using the newly determined parameter set is employed to calculate mass distributions of various kinds of fission and compare them with measured data. The comparison shows rather good agreement between them from spontaneous fission to high energy particle induced fission.

Keywords: Fission Yields, Mass Distribution, Fissioning Nuclide, Fission Product, Systematics

 \bar{A}

JAERI-Research 2003-004

5つのガウス関数による核分裂収率システマティックスの検討

日本原子力研究所東海研究所エネルギーシステム研究部

片倉 純一

(2003年1月29日受理)

核分裂生成物の核分裂収率を予測するシステマティックを検討し、新たなシステマティックス を提案した。このシステマティックスは30年程前に提案された森山-大西システマティックスに基 づいている。森山-大西システマティックスの後に測定されたデータを基にパラメータの見直しを 行い、新たな関数型によるパラメータを決定した。このパラメータを用いて核分裂収率を計算し、 測定データと比較した。様々な核分裂による収率について自発核分裂から高エネルギー粒子によ る核分裂まで広い範囲で測定との良い一致を得た。

東海研究所: 〒 319-1195 茨城県那珂郡東海村白方白根 2-4

Contents

. I ~~1 2 ZW-7j~,7i %'-y... 2 2.1 AM-) h-t~tf7t N *-* AZQ) ME 2 2.2 *Lb-tN AU-t t - 7YZOA0M -AA. ⁴ **3 A 777 '(43t** 6~5X)(-!51O)1. **.** .6 6 4 新たに作成したシステマティックスによる計算.............................. 10 *5 *~Y* 17 AW **171** 0 .:4 .M **181**

目次

This is a blank page.

1 Introduction

It is an important problem for nuclear technology to reduce the nuclear waste produced in nuclear reactors. Several concepts for transmutation of nuclear waste $\frac{1}{1}$ have been proposed, using classical thermal or fast fission reactors as incinerators or using accelerator driven systems, These concepts are being extensively studied with regard to their feasibility, neutron economics, environmental safety, and so on.

For these studies, nuclear data including fission yields are required. For the requirement, Nuclear Data Section, International Atomic Energy Agency, organized a coordinated research program (CRP) titled "Fission Product Yield Data Required for Transmutation of Minor Actinide Nuclear Waste". In the task of the CRP, it is recognized that it is necessary to develop fission yield systematics to estimate the yields over a wide range of fissioning nuclides and the energy range from thermal to 150 MeV.

There are some evaluated fission yields data which are compiled as Evaluated Nuclear Data File such as JENDL²⁾, ENDF³⁾, JEF⁴⁾ and so on. As these evaluated data, however, are for traditional nuclear reactors, the evaluated yields are categorized for thermal neutron fission, fast neutron (neutron emitted by fission) fission and high energy (14 MeV) neutron fission. Although these evaluated yields data are applicable to the traditional reactor technology covering the above energy range, they are not able to apply to the higher energy region required for the CRP. The reliable evaluated fission yields data by such high energy neutrons has not been compiled yet. Even measured data have been limited to those for some fissioning nuclides. Then the systematics of the fission yields data of so-called minor actinides is needed to predict the fission yields data by such high energy neutron fission.

There are several systematics of fission yields. Of such systematics, Wahl's systematics **-5** is widely recognized and shows good agreement with existent yields data by low energy neutrons. It is, however, uncertain that the systematics can be extended to the energy region more than 100 MeV and how is the uncertainty of the systematics in such a high energy region. Therefore it will be worthwhile to make another systematics.

In Japan Moriyama-Ohnishi (hereafter MO) proposed a systematics about 30 years ago 6 . The systematics succeeded to reproduce the mass distributions of the fission products experimentally available at that time. The systematics, however. fails to reproduce the recently measured mass distributions by high energy neutron and proton induced fission. Then new systematics is needed to get the mass yields by higher energy neutron or proton fission. We examined the parameters in the MO systematics based on newly measured data and obtained a new set of the parameters which are applicable to the higher energy fission than 100 MeV.

First the outline of the MO systematics and the problem using the MO systematics are given in Chapter 2. In Chapter 3 the parameter search for new systematics is given. The calculations using the newly determined parameters and comparisons with measured data are described in Chapter 4. Summary is given in Chapter 5.

2 Moriyama-Ohnishi Systematics

2.1 Outline of the Moriyama-Ohnishi Systematics

In the MO systematics, the mass distribution $\psi(A, E^*)$ of fission products just after prompt neutron emission is described as sum of symmetric component $\psi_s(A, E^*)$ and asymmetric component $\psi_a(A, E^*)$. In these expression *A* is a mass of fission fragment and E^* is an excitation energy of of the fissioning nuclide. The asymmetric component is then divided into heavy fragment component $\psi_h(A, E^*)$ and light fragment component $\psi_l(A, E^*)$. And each of these components is formed of two curves (curve 1 and 2). Then the mass distribution $\psi(A, E^*)$ is expressed as follows:

$$
\psi(A, E^*) = N_s \psi_s(A, E^*) + N_a \psi_a(A, E^*)
$$

= $N_s \psi_s(A, E^*) + N_a [\psi_{h1}(A, E^*) + \psi_{l1}(A, E^*) + F {\psi_{h2}(A, E^*) + \psi_{l2}(A, E^*)}] ,$ (2.1)

where N_s , N_a and F are normalization factors and determined by systematics.

The five components in the above equation are assumed to be Gaussian distribution:

$$
\psi_s(A, E^*) = \frac{1}{\sqrt{2\pi}\sigma_s} \exp \left\{ -(A - A_s)^2 / 2\sigma_s^2 \right\},\tag{2.2}
$$

$$
\psi_{h1}(A, E^*) = \frac{1}{\sqrt{2\pi}\sigma_{h1}} \exp \left\{ -(A - A_{h1})^2 / 2\sigma_{h1}^2 \right\},\tag{2.3}
$$

$$
\psi_{h2}(A, E^*) = \frac{1}{\sqrt{2\pi}\sigma_{h2}} \exp \left\{ -(A - A_{h2})^2 / 2\sigma_{h2}^2 \right\},\tag{2.4}
$$

and the other two functions $\psi_{l1}(A, E^*)$ and $\psi_{l2}(A, E^*)$ for the light fragment are given by reflecting $\psi_{h1}(A, E^*)$ and $\psi_{h2}(A, E^*)$ about the symmetric axis $A_s = (A_f - \bar{\nu})/2$. Here A_s , A_{h1} and A_{h2} are the mass numbers corresponding to the peak positions of the Gaussian distribution curves, and σ_s^2 , $\sigma_{h_1}^2$ and $\frac{2}{h_2}$ are the dispersions of these distributions. A_f denotes the mass number of the fissioning nuclide. The quantity $\bar{\nu}$ is the average number of prompt neutrons emitted per fission, and is given by

$$
\bar{\nu} = \begin{cases} 0.107A_f - 23.37 + 0.085E^*, & E^* \le 7.967 \text{ MeV}, \\ 0.107A_f - 23.968 + 0.16E^*, & E^* > 7.967 \text{ MeV}. \end{cases} \tag{2.5}
$$

The quantities N_s , N_a , A_s , σ_s , A_{h1} , A_{h2} , σ_{h1} and σ_{h2} are obtained by least-squares method and are given by

$$
N_s = 200/(1+2R), \tag{2.6}
$$

$$
N_a = 200R / \{(1 + F)(1 + 2R)\},\tag{2.7}
$$

$$
\sigma_s = 0.1759A_f - 41.71 + 0.2056E^{*0.25}(S + 31.908), \tag{2.8}
$$

$$
A_{h1} = 0.5190(A_f - \bar{\nu}) + 0.02840A_f(40.2 - Z_f^2/A_f)^{1/2}, \qquad (2.9)
$$

$$
A_{h2} = 0.5673(A_f - \bar{\nu}) + 0.02151A_f(40.2 - Z_f^2/A_f)^{1/2}, \qquad (2.10)
$$

$$
\sigma_{h1} = 0.07327A_f - 14.50 + 0.01783E^{*0.25}(S + 31.908), \tag{2.11}
$$

$$
\sigma_{h2} = 0.08089A_f - 15.87 + 0.006847E^{*0.25}(S + 31.908). \tag{2.12}
$$

The quantities *R* and *F* are given by

 ϵ

$$
R = \exp\left\{2.262S + 0.0682A_f - 11.542 + \alpha + \exp(\beta)\right\},\tag{2.13}
$$

$$
F = \sigma_{h2}/\sigma_{h1} \exp(-0.08349A_f + 19.43), \qquad (2.14)
$$

where

$$
\alpha = \begin{cases}\n+7.75(A_f)^{-1/2}, & \text{for even } Z_f \text{ - even } N_f, \\
-7.75(A_f)^{-1/2}, & \text{for odd } Z_f \text{ - odd } N_f, \\
0, & \text{for odd } A_f,\n\end{cases}
$$
\n(2.15)

and

$$
\beta = \begin{cases} 2.531 - 0.10546E^*, & \text{for even } A_f, \\ 2.118 - 0.07990E^*, & \text{for odd } A_f. \end{cases}
$$
 (2.16)

These α and β represent the pairing effect of the fissioning nuclide (Z_f, A_f) . The *S* factor appearing in the above equations represents the nuclear shell effect of both fissioning nuclide and fission fragments. The latter is included because of the importance of the shells of the fission fragments which is comparable to that of the fissioning nuclide. Moriyama and Ohnishi employ the shell energy formula $S(N_f, Z_f)$ given by Meyers and Swiatecki⁷⁾ for the S factor adopting the magic number of $N = 126$, 164 and 184 for neutrons and $Z = 82$, 100 and 114 for protons. The numbers $N = 164$ and $Z = 100$ are introduced to take into account the shell effect of fission fragment. The S factor is represented as follows by Meyers and Swiatecki:

$$
S(N, Z) = 5.8s(N, Z), \tag{2.17}
$$

$$
s(N, Z) = \frac{F(N) + F(Z)}{\left(\frac{1}{2}A\right)^{\frac{2}{3}}} - 0.26A^{\frac{1}{3}}.
$$
\n(2.18)

$$
F(N) = q_i(N - M_{i-1}) - \frac{3}{5}(N^{\frac{5}{3}} - M_{i-1}^{\frac{5}{3}}), \quad \text{for } M_{i-1} < N < M_i \tag{2.19}
$$

$$
q_i = \frac{3}{5} \frac{M_i^{\frac{3}{3}} - M_{i-1}^{\frac{3}{3}}}{M_i - M_{i-1}},
$$
\n(2.20)

where M_i is the magic number mentioned above.

2.2 Problems of the Moriyama-Ohnishi Systematics

The calculated mass yields curves using the MO systematics were compared with the measured data of mass distributions for various kinds of fission available at that time. They showed rather good agreement with the measured data. The measured data available at the time, however, were restricted to a limited number. When we make comparison with recently measured distribution, some discrepancies between the calculated distribution and the measured one are seen. An example of the discrepancy is shown in Fig. 2.1, where mass distributions of 248 Cm fission by 20 MeV protons are compared between the calculated results using MO systematics and the measured data 8). The measured mass yields show obvious asymmetric components even though each data point shows scattering behavior, but the MO systematics shows only symmetrical distribution and fails to reproduce the asymmetric behavior the measured data show. This failure seems to imply that the way taking the shell effect into the ratio of the symmetric component to the asymmetric one in the MO systematics is not suitable and should be revised for the application to such kind of fission as 248 Cm.

Fig. 2.1 Mass Yield Curve of $248 \text{Cm} + 20.0 \text{ MeV}$ protons

Another example is shown in Fig. 2.2, where mass distributions of 238 U fission by 160 MeV neutrons are compared between the calculation using the MO systematics and the measurement ⁹. This figure shows that the MO systematics shifts the distribution to lower mass side than the measured data. And the width of the tail seems to be too wide. Asymmetric property is still seen in the MO systematics, although it is not apparently seen in the measured distribution. These failures of the MO systematics at high energy region seems to indicate that the energy dependence of the parameters such as width of the symmetric part, the number of emitted neutrons and the ratio of the symmetric part to the asymmetric part in the MO systematics is not suitable for this kind of fission.

As seen in those figures, the MO systematics fails to reproduce the recently measured particle

Fig. 2.2 Mass Yield Curve of 238U + 160 MeV neutrons

induced fission with high incident energy. Then new parameter set is needed to get the systematics which is applicable to these kinds of high energy fission.

3 Parameter Search for New Systematics

The basis of the MO systematics is *5* Gaussian functions as mentioned in the previous chapter. Recently multimodal fission analysis suggests that there is the mode named standard III¹⁰. In this case 7 Gaussian functions are needed to reproduce the measured mass distribution. But in most of the fissions, 5 Gaussian functions seem to be enough to reproduce the mass distribution. Then 5 Gaussian functions are kept in our search of new parameter set for the systematics.

There are several measured mass distributions available. The measured mass distributions were decomposed into *5* Gaussian functions by least squares fit. From the fitted Gaussian functions, the parameters of the systematics were calculated and examined for various kinds of fission. After the examination, the 8 parameters in 5 Gaussian distributions were determined. As for $\bar{\nu}$ value, the expression by Wahl¹¹ was used:

$$
\bar{\nu} = 1.404 + 0.1067(A_F - 236) + [14.986 - 0.1067(A_F - 236)] \cdot [1.0 - \exp(-0.00858E^*)], \tag{3.1}
$$

where E^* is the excitation energy, that is, the sum of the incident energy (E) and the binding energy *(BN)* of the incident particle. The other 7 parameters were determined as follows:

$$
R = [112.0 + 41.24 \sin(3.675S)] \cdot \frac{1.0}{BN^{0.331} + 0.2067} \cdot \frac{1.0}{E^{0.993} + 0.0951},
$$
(3.2)

 \overline{a}

$$
F = 10.4 - 1.44S,
$$
 (3.3)

$$
\sigma_s = 12.6, \tag{3.4}
$$

$$
\sigma_{h1} = (-25.27 + 0.0345A_f + 0.216Z_f)(0.438 + E + 0.333BN^{0.333})^{0.0864}, \tag{3.5}
$$

$$
\sigma_{h2} = (-30.73 + 0.0394A_f + 0.285Z_f)(0.438 + E + 0.333B_N^{0.333})^{0.0864}, \tag{3.6}
$$

$$
A_{h1} = 0.5393(A_f - \bar{\nu}) + 0.01542A_f(40.2 - Z_f^2/A_f)^{1/2}, \qquad (3.7)
$$

$$
A_{h2} = 0.5612(A_f - \bar{\nu}) + 0.01910A_f(40.2 - Z_f^2/A_f)^{1/2}.
$$
 (3.8)

where S is the shell factor defined in Eq. (2.17) but the magic numbers, N=164 and Z=100 introduced by Moriyama and Ohnishi to consider the shell effect of fission fragment are removed here.

The energy dependence of the *R* parameter was examined from the Zöller's measured data 9 . The measurement were performed using $^{238}U(n,f)$ reaction by incident neutron energy from I MeV to 500 MeV. Such wide energy region is suitable to get energy dependence in the same A and Z values. The Zöller's data were fitted with 5 Gaussian functions and the obtained parameters in the 5 Gaussian functions were used to derive the *R* values. According to the Eqs. (2.1), (2.6) and (2.7), the R value is defined as:

$$
R = \frac{\text{fragment yield given by two asymmetric components}}{\text{fragment yield given by the symmetric component}}
$$

=
$$
\frac{Y_{h1} + Y_{h2} + Y_{l1} + Y_{l2}}{Y_s}
$$

=
$$
\frac{2(Y_{h1} + Y_{h2})}{Y_s}
$$
(3.9)

where Y_{h1} , Y_{h2} , Y_{l1} and Y_{l2} are the yields of the asymmetric components and Y_s the yield of the symmetric component. Using the above equation, the *R* values of each incident energy were obtained and the energy dependence was determnined. The obtained energy dependence is shown in Fig. 3. 1.

Fig. 3.1 Energy dependence of R parameter

The *A, Z* and S dependence of the *R* parameter were also examined using the measured mass distributions of various kinds of fissioning nuclides. In this case the mass distribution of nearly same incident energy of the same particle is suitable. For this purpose the data by Dickens¹²⁾ were used, because he gave the parameters of *5* Gaussian functions of mass distributions by fast neutron fission for various kinds of fissioning nuclides from ²³²Th to ²⁴⁸Cm. From the examination the S dependence of the *R* value was seemed to show a sinuous behavior. Then a sine curve was assumed for the S dependence. Figure 3.2 shows the S dependence of the *R* parameter with the fitted sine curve. Combining the energy dependence and the S dependence of the R parameter, Eq. (3.2) was determined.

Fig. 3.2 Shell energy dependence of R parameter

The Dickens' data were also used to examine the *A, Z* and S dependences of the *F* parameters. After several trial, it was found to be reasonable to assume that the *F* parameter linearly depends on only the S parameter and Eq. (3.3) was obtained. Figure 3.3 shows the S dependence of the *F* parameter with .the fitted line.

Fig. 3.3 Shell energy dependence of F parameter

As for parameters *AhI* and *Ah2* the original form of the *A* and *Z* dependences were kept as the same as the MO systematics but the coefficients were newly obtained by re-fitting measured data including newer data than those Moriyama and Ohnishi used. Then Eqs. (3.7) and (3.8) were obtained.

The width of the symmetric part, σ_s , seemed to have no apparent energy dependence when the Zöller's measured data were examined. Both Wahl⁵⁾ and Dickens¹²⁾ give a constant width for the symmetric part even though their values are different from each other. The σ_s values derived from this work based on the Zöller's measured data are seemed to be consistent with constant width and the value is nearly same as that of Dickens. Then we adopted Dickens' value of 12.6.

The parameters of σ_{h1} and σ_{h2} seemed to have no clear energy dependence but slightly increase tendency with energy when these values derived from the Zoller's measured mass distribution were examined. They seemed to have no clear A, Z and S dependence too. Then it was simply assumed that they have a linear dependence on *A* and *Z* and slight energy dependence. From these examinations the equations seen in Eqs. (3.5) and (3.6) were derived.

4 Calculation Using New Parameters Set

Using the new parameter set, mass distributions of various kinds of fission were calculated and compared with measured data and those of the MO systematics. The comparisons of 248 Cm fission by 20 MeV proton and 238U fission by 160 MeV neutron, which are indicated in Section 2.2 as problem of the MO systematics, are shown in Figs. 4.1 and 4.2. As seen in these figures the present calculations overcome the problems of the MO systematics. For 248 Cm fission by 20 MeV proton, the present calculation can reproduce the valley of the mass distribution although the MO systematics fails to make the asymmetric distribution. In the case of 238 U fission by 160 MeV neutron, the present calculation can reproduce the measured distribution rather well comparing with the MO systematics.

Fig. 4.1 Comparison of ²⁴⁸Cm fission by 20 MeV protons

The comparisons of other results are summarized in Figs. 4.3 through 4.5. In these figures, the mass distributions in log scale (lefthand side) and linear scale (righthand side) are shown.

In Figs. 4.3 and 4.4, the comparisons of neutron induced fission are shown. The neutron energy covers from thermal to 160 MeV. For thermal neutron induced fission, the mass distributions of 233 U, 235 U and 245 Cm fission are shown. These comparisons of thermal neutron fission show that the present calculations reproduce the measured data 13. 14, 15, 16, 17) rather well than the MO systematics do. For medium energy neutron fission, 235 U fission by 8.1 MeV neutron, 239 Pu fission by 7.9 MeV neutron and 237 Np fission by 5 MeV neutron are shown in these figures. The agreement with the measurements ^{18, 19, 20)} seems to be good although slight deviation is seen at the valley part of the ²³⁵U fission by 8.1 MeV neutron and at the high mass wing of the 237 Np fission by 5 MeV neutron. As examples of higher energy fission, mass distributions of ²⁴²Pu fission by 15.1 MeV neutron and ²³⁸U fission by 160 MeV neutron are shown together with the measured data $21,9$. In these comparisons the improvement of the present

Fig. 4.2 Comparison of 238U fission by 160 MeV neutrons

calculations is easily seen. For 242 Pu fission, the valley part is well reproduced by the present calculation but Moriyama-Ohnishi systematics fails to reproduce the valley part. For 238 U fission, the mass distribution of the MO systematics shifts to light mass region too much and the valley to peak ratio is not suitable comparing with the measured data. The present calculation, however, improves the discrepancy and reproduce the measured data rather well, although the slight discrepancy is still seen at the peak mass region.

In Fig. 4.5, the mass distributions of proton induced fission are shown. This figure shows the mass distributions of ²⁴¹ Am, ²⁴³ Am, ²⁴⁸Cm and ²³⁸U fission by protons whose energy values are 16 MeV, 15.6 MeV, 20 MeV and 340 MeV respectively. From all of these comparisons it is easily seen that the present calculations improve the agreement with the measured data $^{22, 8, 23}$ comparing with the MO systematics. As stated in the previous chapter, the present calculation can reproduce the asymmetric mass distribution of 248 Cm fission rather well. In the case of 238 U fission by 340 MeV protons, the present calculation shows symmetric distribution and is in good agreement with the measured data. The present systematics, then, seems to be applicable to the fission by such high energy protons as 340 MeV.

The proposed systematics can make calculation of mass distribution for even spontaneous fission. The calculated mass distributions of spontaneous fission are shown in Figs. 4.6 and 4.7 comparing with the evaluated data of ENDF/B-VI file 24). These figures also show that the present calculations are better than Moriyama-Ohnishi systematics.

Fig. 4.3 Comparison of neutron induced fission (I)

Fig. 4.4 Comparison of neutron induced fission (II)

Fig. 4.5 Comparison of proton induced fission

Fig. 4.6 Comparison of spontaneous fission (I)

Fig. 4.7 Comparison of spontaneous fission (II)

 \bar{z}

5 **Summary**

Parameters of 5 Gaussian-type fission yields systematics were proposed. The calculations using the systematics were performed for various kinds of fission. The results of the calculations were compared with the measured data. The comparisons showed rather good agreement for the mass yields of fission by proton and neutron of energy from thermal to higher than 100 MeV. The systematics seems to be applicable to even spontaneous fission.

In the framework of the IAEA CRP, several systematicses and theoretical models were proposed and inter comparisons among them were performed. The present systematics gives a useful tool to such comparisons. The results of the comparisons will be published in a CRP report. In the report, present status of fission yields prediction will be given.

Acknowledgements

The author expresses thanks to the head of Nuclear Data Center, Dr. Hasegawa, for his support to this work. Thanks are also due to the members of Working Group of Fission Yield, Nuclear Data Committee for helpful discussion.

References

-) 'Overview of Physics Aspects of Different Transmutation Concepts', report NEA/NSC/DOC(94)11 (1994).
- 2) Nakagawa T., et al.: *J. Nuci. Sci. Technol.,* 32, 1259 (1995).
- 3) Cross section Evaluation Working Group, *ENDF/B- VI Summary Documentation,* BNL-NCS- 1 7541 (ENDF-20 1) (1991), edited by P. F. Rose, National Nuclear Data Center, Brookhaven National Laboratory, Upton, NY. USA.
- 4) Nordborg C. and Salvatores M.: *Status of the JEF Evaluated Data Library,* Nuclear Data for Science and Technology, edited by J. K. Dickens (American Nuclear Society, LaGrange, IL, 1994).
- 5) Wahl A. C.: *Compilation and evaluation of fission yields nuclear data,* p.45-75, International Atomic Energy Agency, IAEA-TECDOC-1 168 (2000).
- 6) Moriyama H. and Ohnishi T.: *Systematics of Fission Fragment Mass- Yield Curves,* Tech. Rep. Inst. Atom. Energy, Kyoto Univ., No. 166 (1974).
- 7) Meyers W. D. and Swiatecki W. J.: *Nucl. Phys.* 81, 1 (1966).
- 8) Qin Z., et al.: *Radiochim. Acta* 84, 115 (1999).
- 9) Zöller C. M., et al.: Proc. VII School on Neutron Physics, Ratmino, E. Kornilov (Ed.) JINR, Dubna, 1995 Vol. I p130 (1995).
- 10) Mulgin S. I., et al.: *Phys. Lett.* **B462,** 29 (1999).
- 11) Wahl A. C.: *Notes on Development of Models for Systematic Trends in Fission-Product Yields from High and Low Energy Fission Reactions* - *Sept. 20, 1999,* presented at 1999 CRP Mtg, IAEA. $(1999).$
- 12) Dickens J. K.: *Nucl. Sci. Eng.* 96, 8 (1987).
- 13) Pleasonton F.: *Phys. Rev.* 174, 1500 (1968).
- 14) Wehring B. W., Lee S. and Swift G.: *Light-Fragment Independent Yields for Thermal Neutron Fission of U-233,* Univ. of Illinois, Urbana, Ill, UILU-ENG-80-5312 (1980).
- 15) Schmitt H. W., Neiler J. H. and Walter F. J.: *Phys. Rev.* **141**, 1146 (1966).
- 16) Geltenbort P., Gonnenwein F. and Oed A.: *Radia. Effects,* 93, 57 (1986).
- 17) Dickens J. K. and McConnel J. W.: *Phys. Rev.* **C23**, 331 (1981).
- 18) Glendenin L. E., et al.: *Phys Rev.* **C24**, 2600 (1981).
- 19) Gindler J. E., et al.: *Phys. Rev.* **C27**, 2058 (1983).
- 20) Goverdovski A. A., et al.: ISTC *304-95* Final Report (1997).
- 21) Winkelmann I. and Aumann D. C.: *Phys. Rev.* C30, 934 (1984).
- 22) Ohtsuki T., et al.: *Phys. Rev.,* **C44,** 1405 (1991).
- 23) Stevenson P. C. et al.: *Phyvs. Rev.* 111, 886 (1958).
- 24) England T. R. and Rider B. F.: *Evaluation and Compilation of Fission Product Yields 1993,* Los Alamos National Laboratory, LA-UR-94-3 106, ENDF-349 (1994).

This is a blank page.

国際単位系 (SI) と換算表

表1 SI基本単位および補助単位

表3 固有の名称をもつ SI 組立単位

 $1 eV = 1.60218 \times 10^{-19} J$ 1 u = 1.66054 × 10⁻²⁷ kg

表 4 SIと共に暫定的に 維持される単位

 $1 \text{ Å} = 0.1 \text{ nm} = 10^{-10} \text{ m}$ 1 b=100 fm²=10⁻²⁸ m² 1 bar=0.1 MPa=10⁵Pa 1 Gal=1 cm/s² = 10^{-2} m/s² $1 \text{ Ci} = 3.7 \times 10^{10} \text{Bg}$ $1 R = 2.58 \times 10^{-4} C/kg$ 1 rad = 1 cGy = 10^{-2} Gy 1 rem = $1 \text{ cSv} = 10^{-7} \text{ Sv}$

表

表 5 SI 接頭語

 \overline{a} (注)

 $\overline{}$

1. 表1-5は「国際単位系」第5版,国際 度量衡局 1985年刊行による。ただし, 1 eV および1uの値は CODATAの1986年推奨 値によった。

2. 表4には海里、ノット、アール、ヘクタ ールも含まれているが日常の単位なのでこ こでは省略した。

3. barは、JISでは流体の圧力を表わす場 合に限り表2のカテゴリーに分類されてい る。

4. EC閣僚理事会指令では bar, barn およ び「血圧の単位」mmHg を表2のカテゴリ ーに入れている。

 $\sqrt{2}$ $N(=10⁵ dyn)$ kgf lbf 0.101972 0.224809 $1\,$ 2.20462 9.80665 $\mathbf{1}$ 0.453592 4.44822 $\mathbf{1}$ 精 度 1 Pa-s(N-s/m²)=10 P(ポアズ)(g/(cm-s))

換

算

