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ACOL TUNE SHIFTS AND DISPERSION CHANGE ASSOCIATED

WITH QUADRUPOLE CURRENT VARIATIONS

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1. Introduction

In the ACOL machine, three trim power supplies will allow separate control of wide quadrupole strength to adjust the betatron tunes Q_H , Q_V and the dispersion D . This paper derives the matrix which relates the tune shifts $\Delta Q_{H,V}$ and the dispersion change ΔD to quadrupole current variations $\Delta I_{1,2,3}$.

2. Fundamental relations

Changes in betatron tunes and horizontal orbit dispersion are associated with changes in quadrupole strength by the relations ¹

$$\Delta Q_{H,V} = \frac{1}{4\pi} \int_s^{s+C} \beta_{H,V}(\sigma) \Delta K_{H,V}(\sigma) d\sigma \quad (1)$$

$$\Delta D(s) = \frac{-\sqrt{\beta_H(s)}}{2s \ln \pi Q_H} \int_s^{s+C} \sqrt{\beta_H(\sigma)} D(\sigma) \Delta K_H(\sigma) \cos(-\pi Q_H + \mu_H(\sigma) - \mu_H(s)) d\sigma \quad (2)$$

where C is the machine circumference.

Equation (1) can be replaced by a sum over the quadrupoles

$$\Delta Q_{H,V} = \frac{1}{4\pi} \sum_{j=1}^n \bar{\beta}_{H,Vj} l_j \Delta K_{H,Vj} \quad (3)$$

$\bar{\beta}_{H,Vj}$ and l_j being respectively the average value at $\beta_{H,V}$ and the length of quadrupole j .

Equation (2) can also be transformed into a sum over the quadrupoles, defined by the values β_{He} , α_{He} , μ_{He} at their entrance².

$$\Delta D(s) = -\frac{\sqrt{\beta_H(s)}}{2 \sin \pi Q_H} \sum_{j=1}^n \Delta K_{Hj} \left\{ C_{1j} \sqrt{\beta_{Hej}} \cos \varphi_j(s) - \frac{C_{2j}}{2\sqrt{\beta_{Hej}}} [(\alpha_{Hej} \cos \varphi_j(s) + \sin \varphi_j(s))] \right\}$$

where

$$\varphi_j(s) = -\pi Q_H + \mu_{Hej} - \mu_H(s)$$

and

$$C_{1j} = \int_0^{l_j} a_j^{11}(\sigma) D_j(\sigma) d\sigma \quad C_{2j} = \int_0^{l_j} a_j^{12}(\sigma) D_j(\sigma) d\sigma$$

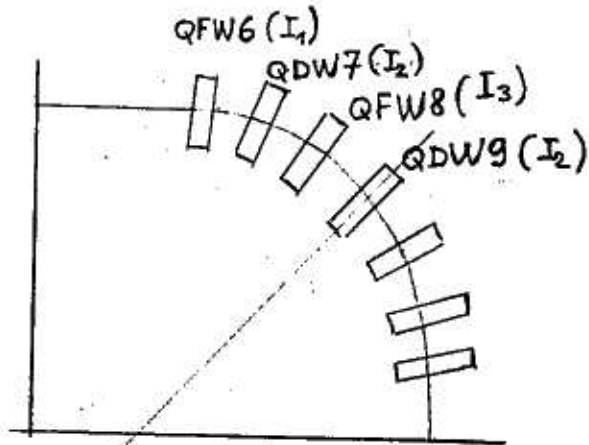
the a_j^{11} and a_j^{12} being the transfer matrix coefficients of the quadrupoles.

In the thin lens approximation, and assuming that the dispersion function may be replaced by its average value \bar{D}_j in each quadrupole, equation (4) becomes

$$\Delta D(s) = -\frac{\sqrt{\beta_H(s)}}{2 \sin \pi Q_H} \sum_{j=1}^n \Delta K_{Hj} \bar{D}_j l_j \left\{ \sqrt{\beta_{Hej}} \cos \varphi_j(s) - \frac{l_j}{2\sqrt{\beta_{Hej}}} (\alpha_{Hej} \cos \varphi_j(s) + \sin \varphi_j(s)) \right\} \quad (5)$$

3. Correction matrix

The AC wide quadrupole (QW) are divided in three families which have a separate trim power supply (currents I_1, I_2, I_3). First and third families include each 8 horizontally focusing quadrupoles, the second includes 12 horizontally defocusing quadrupoles (see Figure).



AC first quadrant

The strength variation is produced by a change in quadrupole current

$$\Delta K_{H,V} = \frac{\Delta I}{I} K_{H,V} \quad (6)$$

Using equations (3) and (5), the changes of betatron tunes and orbit dispersion with the quadrupole currents can be written in a matrix form

$$\begin{pmatrix} \Delta Q_H \\ \Delta Q_V \\ \Delta D \end{pmatrix} = M \begin{pmatrix} \Delta I_1 \\ \Delta I_2 \\ \Delta I_3 \end{pmatrix}$$

The matrix coefficient m_{jk} are

$$m_{1k} = \frac{\partial Q_H}{\partial I_K}$$

$$m_{2k} = \frac{\partial Q_V}{\partial I_K}$$

$$m_{3k} = \frac{\partial D}{\partial I_K}$$

The analytical expressions being

$$m_{1k} = \frac{1}{I_k} \sum_i \bar{\beta}_{Hi} l_i K_{Hi}$$

$$m_{2k} = \frac{1}{I_k} \sum_i \bar{\beta}_{Vi} l_i K_{Vi}$$

$$m_{3k} = \frac{-\sqrt{\beta_H}}{2 I_k \sin \pi Q_H} \sum_i K_H \bar{D}_i l_i \left\{ \sqrt{\beta_{Hei}} \cos \varphi_i - \frac{l_i}{2\sqrt{\beta_{Hei}}} [\alpha_{Hei} \cos \varphi_i + \sin \varphi_i] \right\}$$

where $k=1,2,3$ and the sums are performed over all quadrupoles of a given family I_k .

The inverse matrix M^{-1} , called current corrections matrix, gives the trim current variations needed to achieve a requested correction for one parameter without disturbing the other two.

4. Numerical results

The interest is mainly concerned with dispersion correction in nominal zero-dispersion regions where the stochastic cooling systems are located. Consequently, the matrices are evaluated at longitudinal location zero. Numerical calculations using characteristic functions provided by optics program ORBIT³ gives

$$M = 10^{-3} \begin{pmatrix} 1.36 & -0.62 & 1.43 \\ -0.40 & 1.90 & -0.53 \\ -0.48 & -1.59 & 6.84 \end{pmatrix}$$

and

$$M^{-1} = 10^2 \begin{pmatrix} 7.19 & 1.15 & -1.41 \\ 1.79 & 5.93 & 0.09 \\ 0.93 & 1.46 & 1.38 \end{pmatrix} \begin{pmatrix} Q_H \\ Q_V \\ D \end{pmatrix}$$

D in m ,
in QDNO1

$$\Delta Q_H = \Delta \cos \pi Q_H \cdot \frac{1}{-\pi \sin \pi Q_H}$$

AnnexQuadrupole characteristics⁴

	QFW6	QDW7	QFW8	QW9
l (m)	0.758	-0.754	0.751	0.760
K_H (m ⁻²)	0.4406	-0.4969	0.5453	-0.3894
I (A)	1830.6	1884.8	1782.0	1884.8

Références

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4. L. Rinolfi, Distribution des quadripôles ACOL (unpublished note) (1986).