

AA INJECTION AND EJECTION BEAM LINES

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Introduction

This note gives a summary of the beam optics calculated for the AA beam lines. A non-standard version of TRANSPORT has been used, but users of the standard CERN version should be able to follow the appended data lists. Appendix I explains the relevant differences as well as giving some correspondences between TRANSPORT and BEATCH data conventions. Data files are stored on the permanent data file base for the CDC-MFB computer under the names AADn, ID = PS 321 TRS.

Names of beam line magnets follow the system described in PS/AA/Mem.79-41 (Blechsmidt, Sherwood, 28.3.79) and differ from those used in previous (informal) notes.

Lists of beam elements are given showing beam size and required currents against apertures and maximum nominal current available. The geometrical layout is given in PS/ML/BS/nc, (Mayoud, Szeless, 25.5.79).

When reading the geometry and beam optic lists, the following points should be noted:

1. Distances are given along the beam axis, whether sloping or horizontal.
2. Magnetic lengths are usually used, but in any case, the centre of the element and the integral of the field or gradient are always well defined.
3. The length of a bending magnet is defined as the arc length of the central trajectory (TRANSPORT convention). For a rectangular magnet block, of length  $L$ , oriented symmetrically to the incoming and outgoing beams and which gives a deflection angle  $\theta$ , we have the related lengths:

a) arc-length,  $s$ , where

$$s = L\theta / (2 \sin \frac{\theta}{2})$$

and  $L'$ , the distance from entry (or exit) to the intersection point of the entering and exiting beams where

$$L' = (L/2) \sec \frac{\theta}{2}$$

Usually  $s$ ,  $2L'$  and  $L$  are only slightly different.

4. Tilt angles are defined in the geometry memo. In TRANSPORT a tilted magnet is treated by rotating the beam reference axis about the beam longitudinal direction so as to align it with the magnet element system. The angle is introduced via a TRANSPORT type 20 element. When the incoming beam  $X$  axis is horizontal, tilt and rotation angles are identical. Since beam envelopes are given in the beam reference system, the presence of tilted magnets introduces the discontinuities seen in the graphs. A vertical bending magnet is treated as a tilted magnet with tilt angle  $90^\circ$ .

### Beam Envelopes

The injection line is treated in two parts:

- a) From the PS to the antiproton production target  
and
- b) From the target to the end of the injection/ejection straight section.

The ejection line is taken from the start of the ejection straight section to a point just beyond the crossing with TT2.

The interpretation of the accompanying beam envelope and momentum vector graphs differ in these three sections.

#### Injection line PS to target

A small beam waist is required at the target for 26 GeV/c incident protons. The lower limit to beam size (apart from power density in the target itself) is given by the emittance and momentum spread of the PS beam as well as the apertures in the final vertical bending magnet and pulsed quadrupoles. The momentum vector ( $\alpha_p, \alpha_p'$ ) should be zero at the target in both transverse planes, ( $\alpha_p'$  does not affect beam size at the target but does use aperture in the upstream magnets). Such solutions were not found, in particular the condition  $(\alpha_p')_y$  was not possible and allowance had to be made for this.

The aperture required to pass this fraction of the beam is then

$$A = 2 \left[ w^2 + \left( \frac{\Delta p}{p} \alpha_p \right)^2 \right]^{\frac{1}{2}} + 2 \frac{d p}{p} \alpha_p$$

where  $w$  is the half-width of one component. Values of  $A_H, A_y$  are given in the table comparing required aperture with that available. No special allowance has been made for steering errors or poor magnetic field quality regions. In the calculations the starting point has been taken as magnet QD102. The beam parameters at this point were obtained from a BEATCH run for normal operation of TT2 when the beam is going to the ISR.

### Injection line - Target to AA ring

The antiproton beam is matched to the AA ring using the lattice parameters given in the 7th edition of the parameter list (Jan. 1979) using an acceptance of  $100\pi$  mm.mR., a momentum spread of  $\pm 0.75\%$ . The septum magnets and the small effect of the kicker on the momentum vector are included.

It is assumed that the antiproton beam is a waist of radius 22 mm at the exit of the magnetic horn. The beam envelope is for  $\frac{dp}{p} = 0$  and the required apertures are given by:

$$A = 2(w + \frac{dp}{p} \alpha_p)$$

Even to get  $(\alpha_p, \alpha_p')_H = 0$  requires changing two quadrupoles, QF 107, in the TT2 line to run at currents a little higher than for normal ISR operation.

Solutions are given for the following beam sizes at the centre of the target:

- 1) horizontal 1.4 mm, vertical 1.5 mm
- 2) " 2.0 mm, " 2.0 mm
- 3) " 3.0 mm, " 3.0 mm

Two solutions are given for case 3). Beam envelopes are for zero momentum spread.

### PS beam assumptions

The characteristics of the PS beam have been given in PS/DL/Note.78-7 (P. Lefèvre). If the beam is combined into five bunches at 26 GeV/c, we can consider it as a double beam, each component matched to the PS lattice but separated by a distance:

$$\delta x = \alpha_p \frac{dp}{p}$$

Each component is expected to have an emittance of  $2\pi$  mm.mR and a momentum spread  $\frac{\Delta p}{p} = \pm 10^{-3}$  (contains 95% of the beam) but separated in momentum by  $\frac{dp}{p} = \pm 2.10^{-3}$ .

The envelopes calculated are for a component emittance 2.46 mm mR giving nearer to 97½% of the beam (assuming a Gaussian model).

Ejection Line - AA ring to junction with TTL2

The hande-over point is at the end of EJ 2575( D8 is the TTL2 name). This is the second quadrupole magnet after the ejection line crosses TT2. At this point the matching conditions requested are:

$$\begin{array}{ll} (\alpha_p)_H = 0 & , \quad (\alpha_p')_H = 0 \\ (\alpha_p)_V = -0.508, & (\alpha_p')_V = -0.0135 \\ L_H = 10 \text{ mn} & , \quad L_V = 75 \text{ m} \\ S_H = 0 & , \quad S_V = 0 \end{array}$$

The ejected beam is matched to the AA lattice with an initial horizontal momentum vector (-0.0745 m, 0.0039 rad) due to the ejection kicker. The emittances used are  $1.4\pi$  mm mR for the horizontal and  $1.\pi$  mm mR for the vertical. Beam envelopes are for  $\frac{dp}{p} = 0$ . Required apertures are given by:

$$A = 2 \left[ (w^2 + (\frac{dp}{p} = \alpha_p)^2) \right]^{\frac{1}{2}}$$

using a value of  $\frac{dp}{p} = 3 \times 10^{-4}$ .

The effect of momentum spread on aperture requirement is small for the above values.

## APPENDIX I

### Non-Standard TRANSPORT

The beam optic calculations were made using a non-standard version of TRANSPORT. The attached data lists are for this version. They differ from that required for the CERN version of TRANSPORT (CERN 73-16) in format and the presence of both non-standard element types and modified standard types. These differences are noted below. The purpose of these notes is to enable a person familiar with the standard version of TRANSPORT to be able to construct a standard data list.

1. Format. The data is given in a fixed format (IX, A10, 7F 10.5). The first word is any table (or blank). The rest of the words on each line conform to the data requirement for the element type (word 2).
2. No indicator word is used.
3. Beam momentum (4th word) is entered via the type 16. element, not with a type 1 element.
4. The initial beam description is entered by the combination of the special type 24 emittance element and the modified type 1 element. The type 24 element gives three independent emittances for the horizontal, vertical and longitudinal planes in that order. The following type 1 element gives (in TRANSPORT notation)

$$\sigma_{11}^{\frac{1}{2}}, r_{12}, \sigma_{33}^{\frac{1}{2}}, r_{34}, \sigma_{55}^{\frac{1}{2}}, r_{56}$$

5. The special type 22 element is used to obtain plots of beam envelopes.

### Relations between some BEATCH and TRANSPORT parameters

1. Quadrupole strengths. TRANSPORT expect two parameters (words 4 and 5) viz. field and a radius.

The fields are given in KG and an arbitrary radius of 1 cm is used. Consequently word 4 can be interpreted as gradient, G, in KG/am. BEATCH requires the parameter K(m<sup>-2</sup>). G and K are related by

$$K = - \frac{G}{(B\rho)}$$

where G is in T/m, B $\rho$  is in T.m

In TRANSPORT G is positive for a horizontally focussing magnet.

2. Bending magnet lengths. BEATCH uses the straight length of a straight magnet while TRANSPORT uses the arc length of the reference trajectory.
3. BEATCH uses the parameters L, S. TRANSPORT uses the sigma matrix

Horizontal beam size,  $\sigma_{11}^{\frac{1}{2}} = \left[ (\epsilon/L_H) (S_H^2 + L_H^2) \right]^{\frac{1}{2}}$   
" divergence,  $\sigma_{22}^{\frac{1}{2}} = (\epsilon/L_H)^{\frac{1}{2}}$

Distance to beam waist is  $r_{12} \cdot (\sigma_{11}/\sigma_{22})^{1/2} = S_H$

giving  $r_{12} = S_H / (L^2 + S^2)^{1/2}$

$\epsilon$  is the emittance (ellipse area /  $\pi$ )

## ERRATUM

Please note that all magnetic elements  
in the ejection line should have names  
of the form xyz 25 nn NOT xyz 24 nn  
as in the data lists and diagrams.













DISOL1	AAD1	FINAL	VERSION	25/4/79	TARGET TO AA	RING	16/05/79	12.21.22.
*P*	16.	000000	16.	000000	3.575200			
*CHITT*	24.	000000	10.	000000	10.000000	75.000000	0.000000	
*BEAM*	1.	000000	2.	200000	0.000000	2.200000	0.000000	100.000000
*SP CH*	22.	000000	0.	250000	0.000000	200.000000	0.000000	1.000000
*SLIT*	10.	000000	0.	000000	2.000000			
60	3.	000000	2.	810000				
65	3.	010000	1.	160000	-457392	1.000000		
70	3.	000000	1.	340000				
75	3.	010000	1.	160000	.440517	1.000000		
80	3.	000000	2.	250000				
85	4.	000000	1.	140300	8.213910	0.000000		
90	2.	000000	2.	250000				
95	7.	000000	1.	849600				
H24	1.	010000	1.	160000	-234131	1.000000		
H24	3.	000000	0.	840000				
H24	1.	010000	1.	160000	.151600	1.000000		
H24	3.	000000	0.	190000				
H24	1.	010000	1.	160000	.127873	1.000000		
H24	3.	000000	3.	920000				
H24	1.	010000	1.	160000	-203178	1.000000		
H24	3.	000000	3.	420000				
H24	1.	010000	1.	160000	.148980	1.000000		
H24	3.	000000	8.	052200				
H24	6.	000000	6.	500000				
H24	3.	000000	3.	900000	6.820000	0.000000		
H24	3.	000000	3.	549270				
H24	3.	000000	3.	575000				
H24	3.	000000	3.	549270				
H24	2.	000000	2.	750000	2.548112334	3.120000		
H24	2.	000000	2.	614410				
H24	2.	000000	2.	575000				
H24	2.	000000	2.	614410				
H24	3.	000000	3.	900000	6.820000	0.000000		
H24	3.	000000	3.	336000				
H24	3.	000000	3.	926500				
COND1	1.	000000	1.	000000	1.000000	4.318970	.001000	
COND2	10.	000000	2.	000000	3.000000	4.050810	.001000	
COND3	10.	000000	3.	000000	3.000000	3.815190	.001000	
COND4	10.	000000	4.	000000	4.000000	3.713300	.001000	
COND5	10.	000000	2.	000000	6.000000	.109000	.001000	
COND6	10.	000000	22.	000000	6.000000	.063000	.001000	
SENTINEL								

LIST 5 Data list AAD1. Injection line. Target to AA ring

D7SOL1		AA EJECTION-FINAL		14/06/79 08.58.16.			
P	16.000000	16.000000	3.575200				
EMIT	24.000000	-1.400000	.100000	.000010	0.000000		
BEAM	1.000000	.511027	-.820547	.281819	-.294713	100.000000	0.000000
PLOT	22.000000	.500000	0.000000	200.000000	0.000000	1.000000	
INTR2	6.000000	0.000000	2.000000				
INTAP	14.000000	1.000000					
INTAPP	1.000000	0.000000	0.000000	0.000000	-.07450		
D0	14.000000	2.000000					
D1	1.000000	0.000000	-0.000000	0.000000	.03890		
EDG1	33.000000	0.000000	0.000000				
SMH1	3.920500	3.920500					
EDG2	2.220000	-.215000					
EDG3	4.400000	.900000	-6.824000	0.000000			
EDG4	2.230000	-2.736000					
EDG5	2.230000	.575000					
SMH24	4.400000	2.736000	-2.259410	425.200000			
EDG6	2.230000	-3.549000					
D4	2.230000	.575000					
QEJ2410	2.230000	3.549000	-6.824000	0.000000			
D5	2.230000	.900000					
QEJ2415	2.230000	-6.800000					
D6	2.230000	7.160000					
ROTZ1	2.230000	.500000	.831380	1.000000			
EDG7	2.230000	1.700000					
BTI2420	2.230000	.500000	-.908389	1.000000			
EDG8	2.230000	.812900					
ROTZ1B	2.230000	-17.559700					
D7	2.230000	-6.859600					
QEJ2430	2.230000	1.964700	-14.534070	0.000000			
D8	2.230000	-6.859600					
QEJ2435	2.230000	17.043200					
COND10	2.230000	3.092900					
D9	2.230000	.500000	.951020	1.000000			
QEJ2440	2.230000	4.090000					
COND9	2.230000	.500000	-.886993	1.000000			
D10	2.230000	3.000000	3.000000	.800000	.100000		
QEJ2445	2.230000	5.300000					
D11	2.230000	.600000	.836143	1.000000			
QEJ2450	2.230000	1.000000	1.000000	.750000	.100000		
D12	2.230000	3.040000					
ROTZ2	2.230000	.500000	-.986792	1.000000			
EDG9	2.230000	5.920000					
BTI2455	2.230000	.500000	1.056610	1.000000			
EDG10	2.230000	.635500					
ROTZ2B	2.230000	-15.316947					
D13	2.230000	7.580000					
QEJ2460	2.230000	1.964690	16.056152	0.000000			
D14	2.230000	7.580000					
QEJ2465	2.230000	15.883200					
D15	2.230000	.782700					
QEJ2470	2.230000	.500000	-1.050000	1.000000			
D16	2.230000	.500000	.660174	1.000000			
COND1	2.230000	1.713000					
COND2	2.230000	.500000	.361335	1.000000			
COND3	2.230000	6.752200					
COND4	2.230000	3.850000					
COND5	2.230000	.500000	-.339440	1.000000			
COND6	2.230000	-21.000000	6.000000	0.000000	.001000		
COND7	2.230000	-22.000000	6.000000	0.000000	.001000		
COND8	2.230000	-23.000000	6.000000	-.507626	.001000		
COND9	2.230000	-24.000000	6.000000	-1.34750	.001000		
COND10	2.230000	1.000000	1.000000	.374160	.001000		
COND11	2.230000	2.000000	1.000000	0.000000	.001000		
COND12	2.230000	3.000000	3.000000	.865000	.001000		
COND13	2.230000	4.000000	3.000000	0.000000	.001000		
COND14	2.230000	1.000000	1.000000	0.000000	.001000		
DOEND	3.000000	1.000000					
SENTINEL							

LIST 6 Data list AAD7. Ejection line.



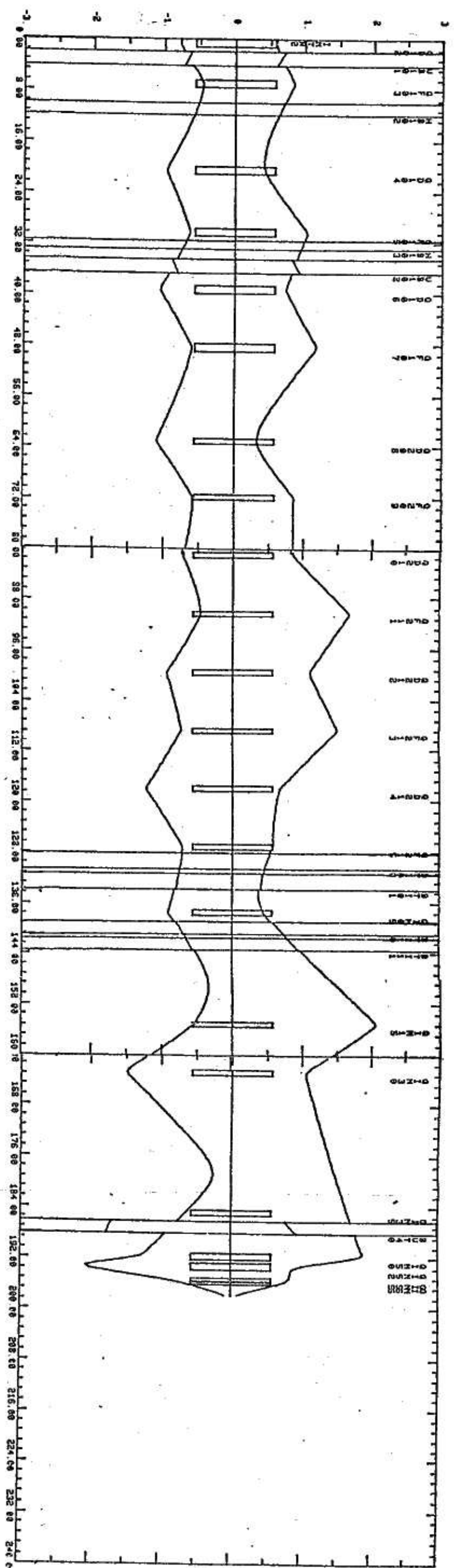


Fig. 1. Beam Envelopes from TT2 to target. Beam diameter on target 1.5 mm LIST 1. Data set AAD10

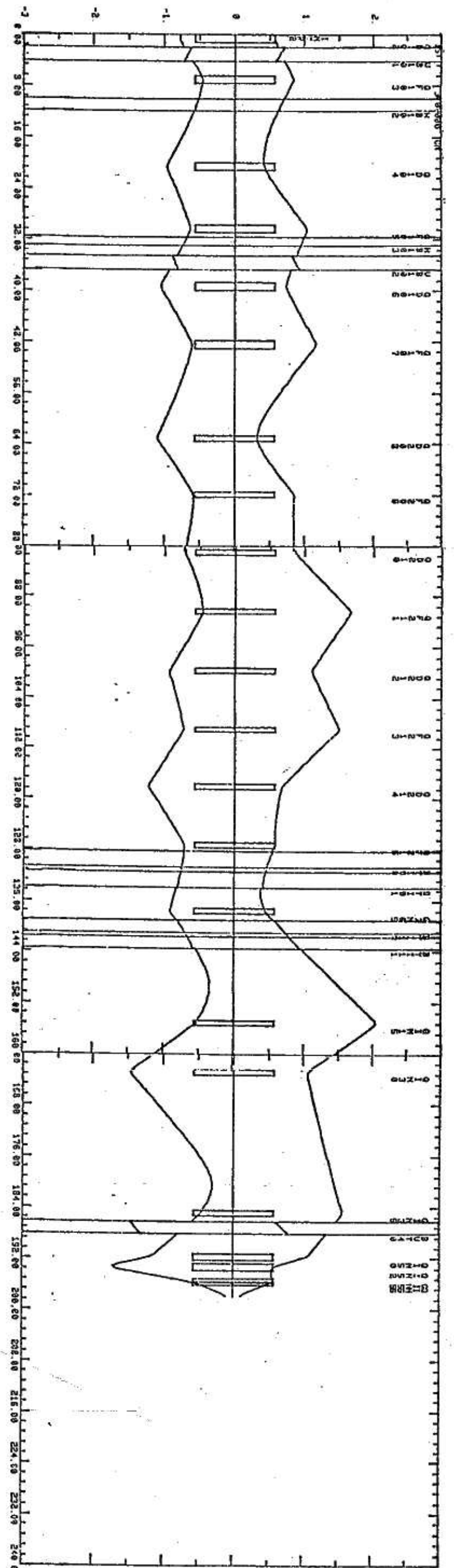


Fig. 2. Beam Envelopes from TT2 to target. Beam diameter on target 2.0 mm LIST 2. Data set AAD11

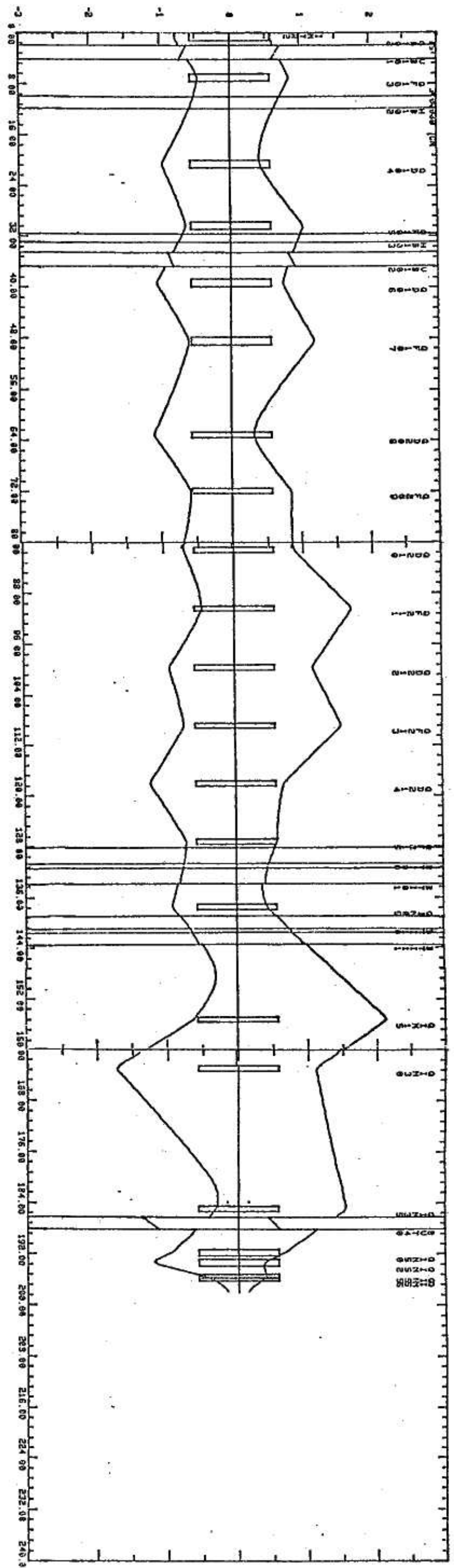


Fig. 3. Beam Envelopes from TT2 to target. Beam diameter on target 3.0 mm LIST 3. Data set ADD12 Solution 1

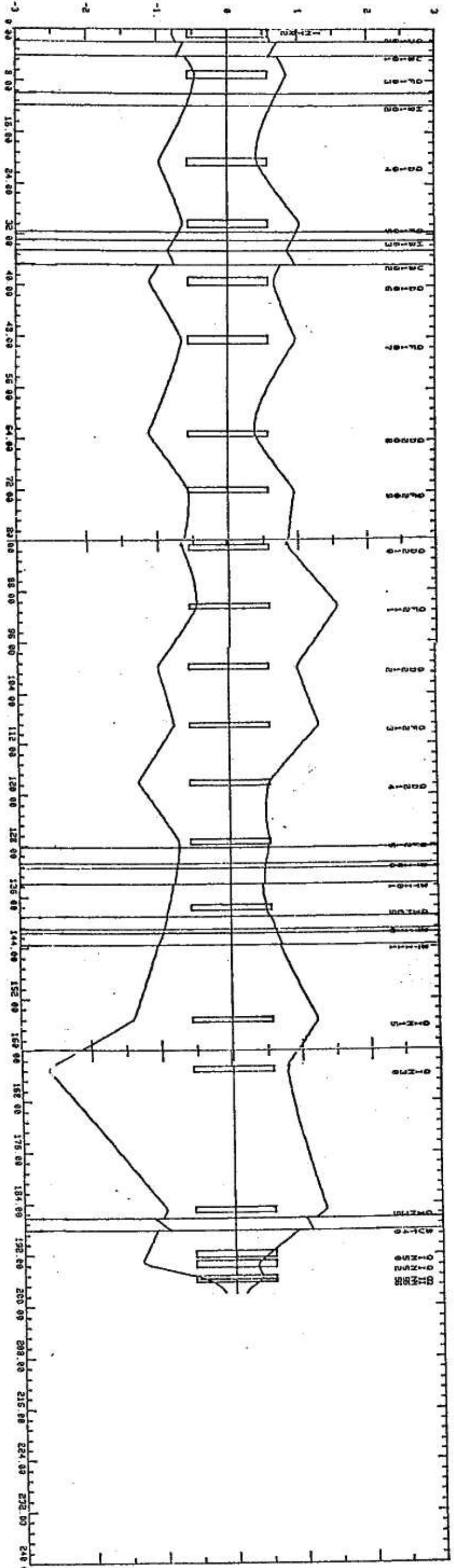


Fig. 4. Beam envelopes from TT2 to target. Beam diameter on target 3.0 mm LIST 4. Data set AAD3 Solution 2



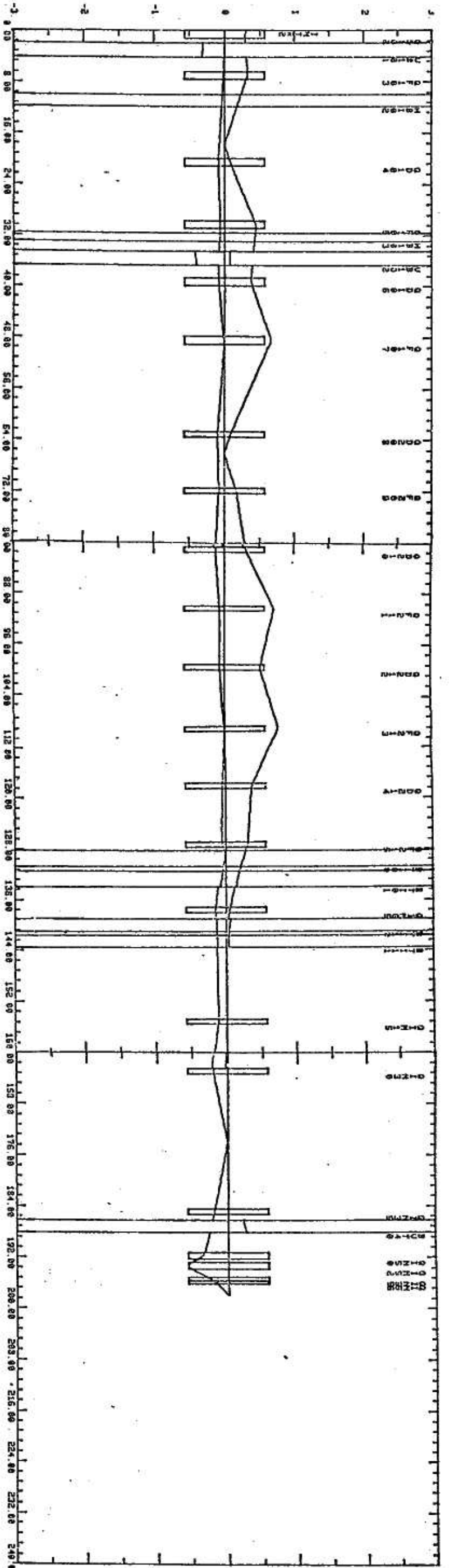


Fig. 7. Momentum Vectors  $dp/p = 0.2\%$  See Fig. 1

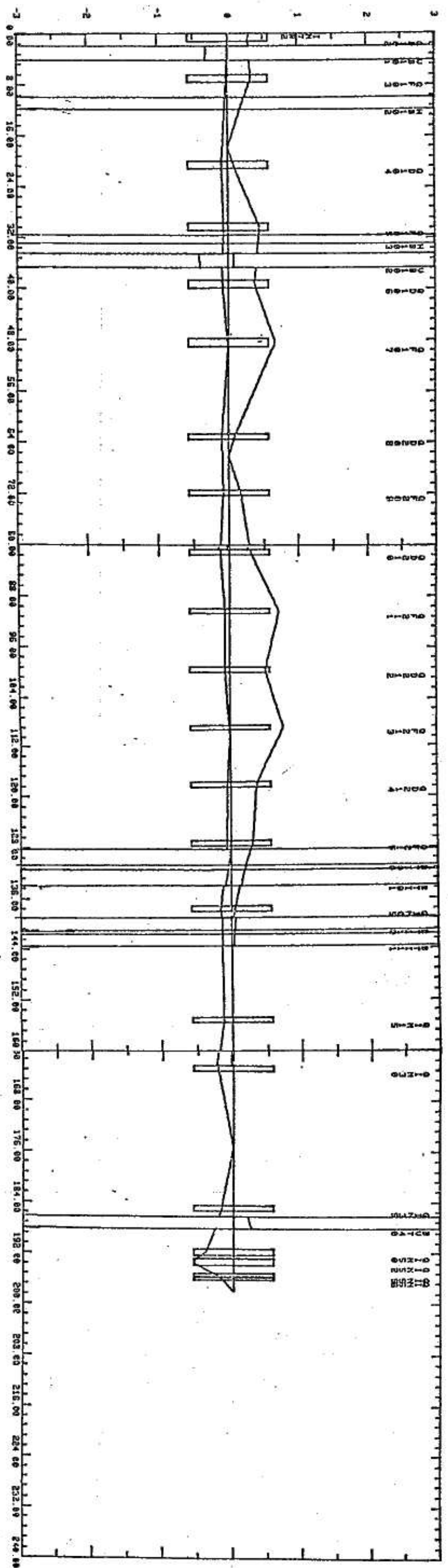


Fig. 8. Momentum Vectors  $dp/p = 0.2\%$  See Fig. 2

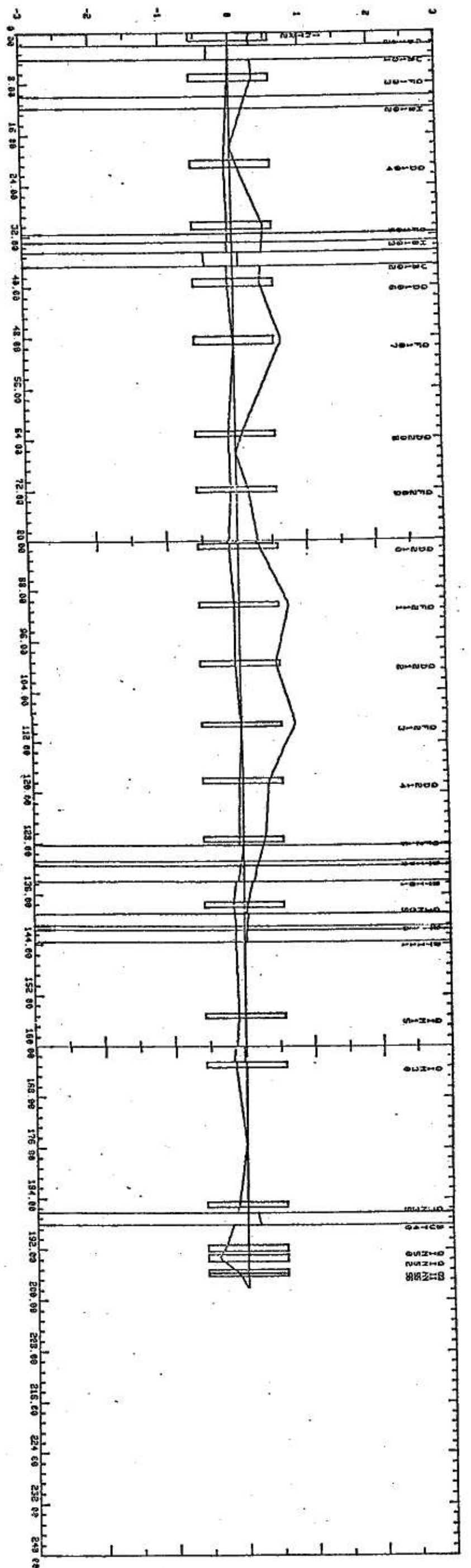


Fig. 9. Momentum Vectors  $dp/p = 0.2\%$  See Fig. 3

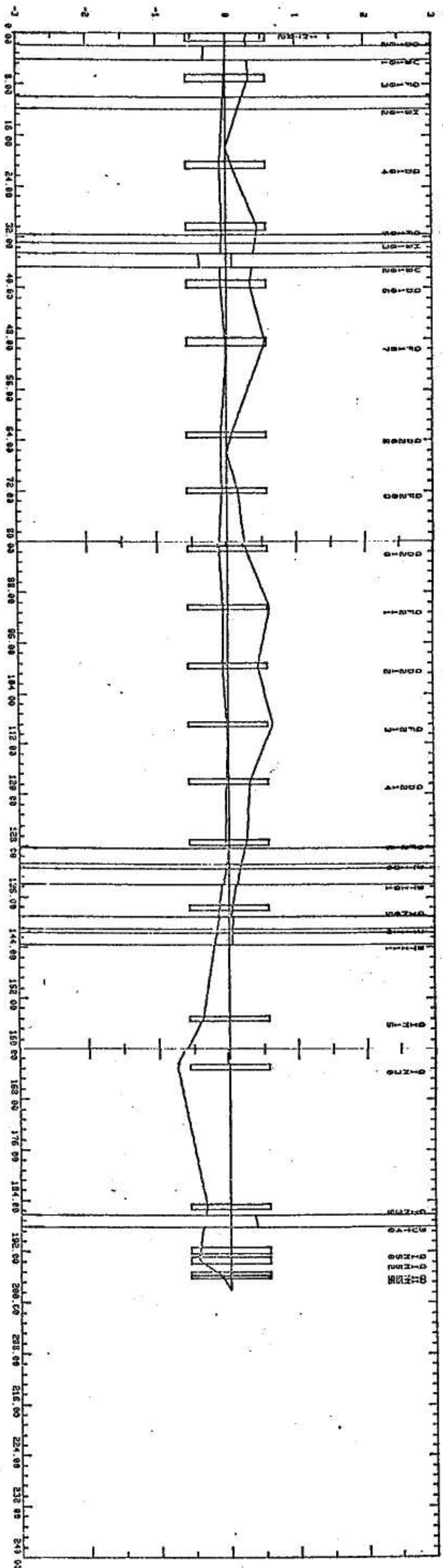


Fig. 10. Momentum Vectors  $dp/p = 0.2\%$  See Fig. 4

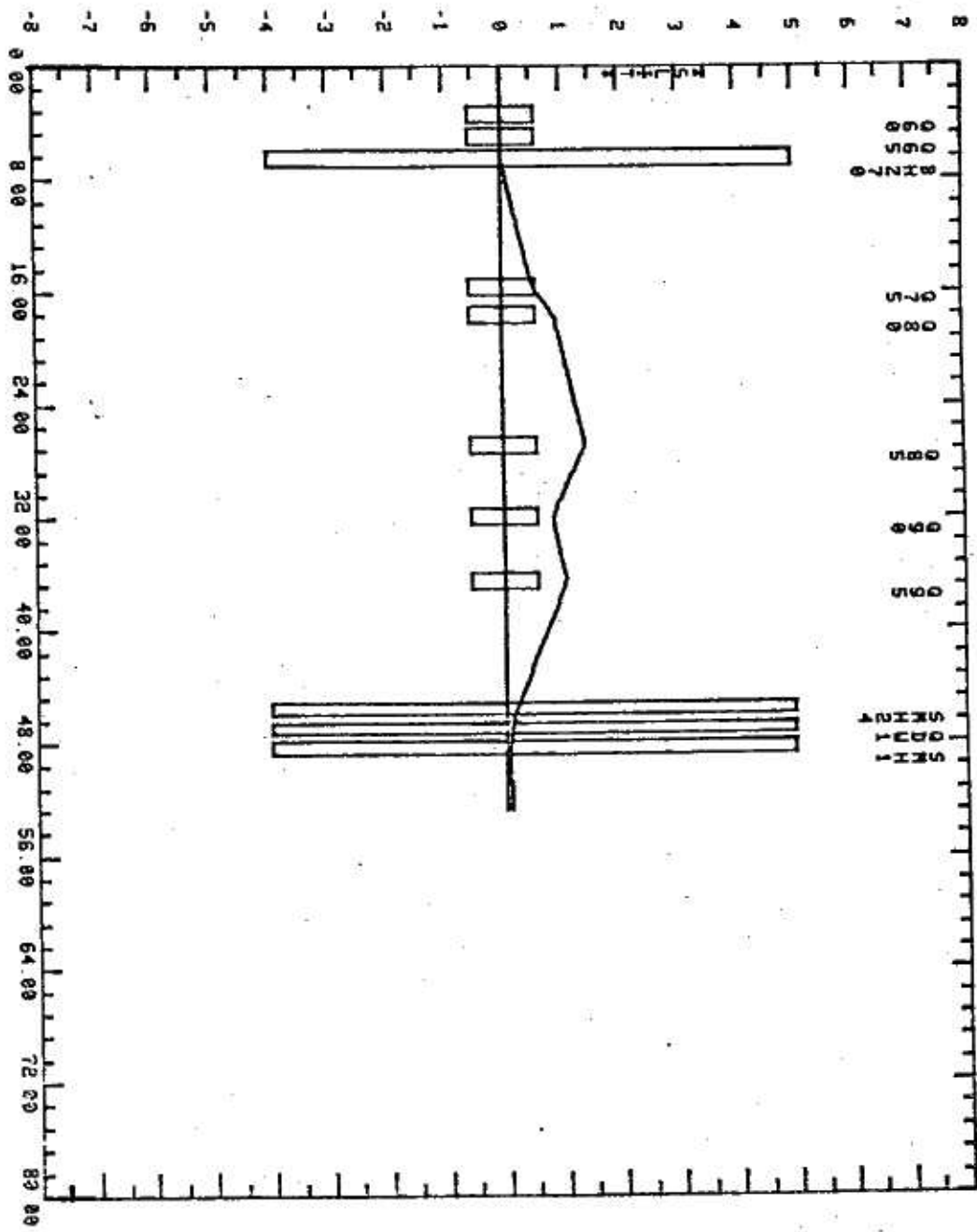


Fig. 11. Momentum Vectors  $dp/p = 0.75\%$  See Fig. 5

*Target → ring*

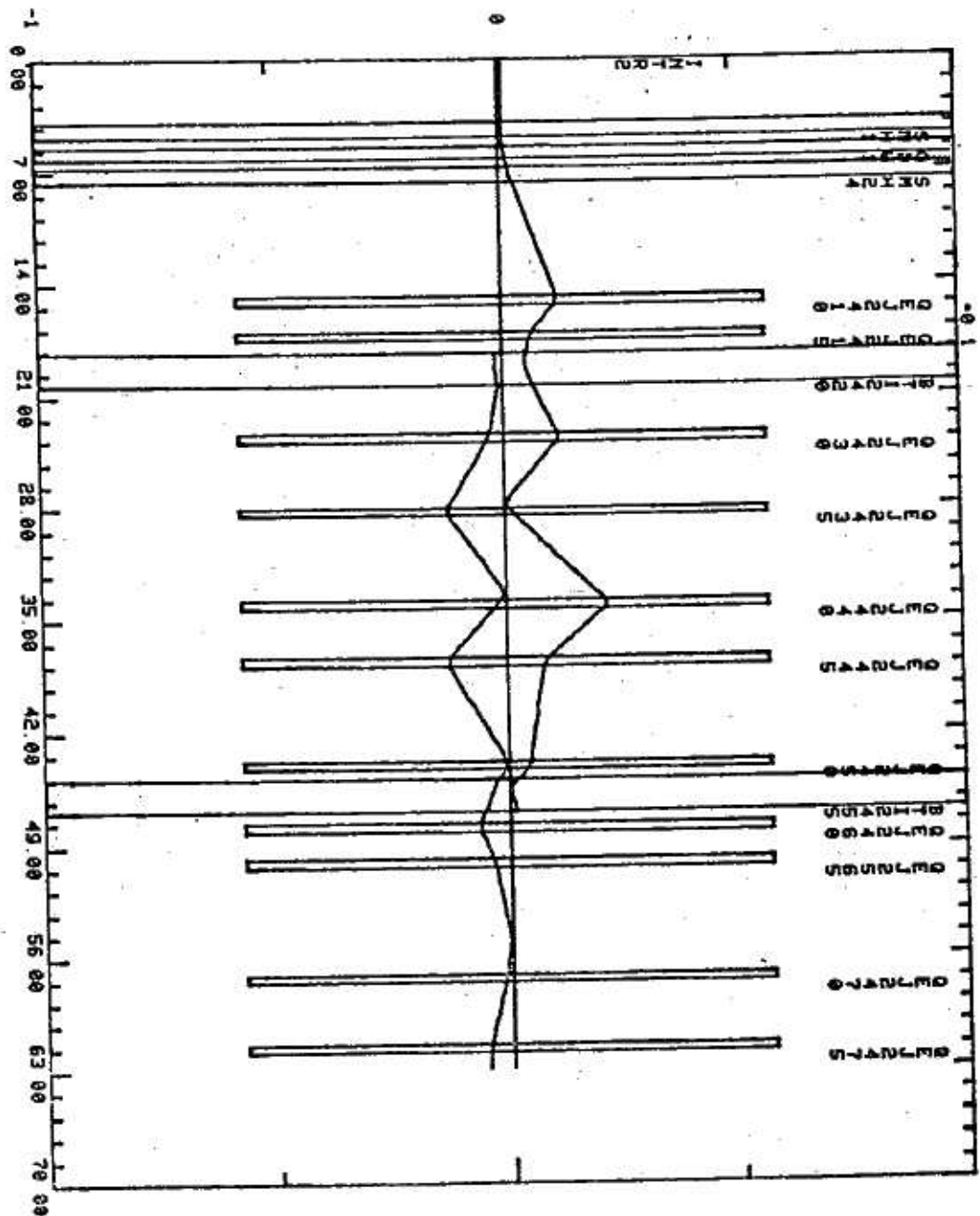


Fig. 12. Momentum Vectors  $dp/p = 0.1\%$  See Fig. 6

*ej. Line*

Name	Type Origin	Pole tip Diameter (mm)	Vacuum tube ID	Plane	Required Aperture	Required Strengths $B$ in KG/cm, $Kcm^{-2}$	Required Current	Available Current
QIN0060	Q100 PS	200	152	H V	72 52	-0.4574 0.3835	230.2	430
QIN0065	Q100 PS	200	152	H V	97 40	0.4405 -0.3694	221.7	430
QIN0075	Q100 PS	200	152	H V	70 137	-0.2341 0.1963	117.8	250
QIN0080	Q100 PS	200	152	H V	104 118	0.1516 -0.1271	76.3	150
QIN0085	Q100 PS	200	152	H V	142 98	0.1279 -0.1072	64.4	150
QIN0090	Q100 PS	200	152	H V	102 142	-0.2032 -0.1704	102.3	150
QIN0095	Q100 PS	200	152	H V	132 82	0.1490 -0.1249	75.0	150

Quadrupole Magnet - Operating Requirements - Injection Line Target to AA Ring



Name	Type Origin	Pole tip diameter (mm)	Vacuum tube I.D.	Plane	Required Aperture		Required Strength G in Kgf/cm, K in m <sup>2</sup>	* Required Current	Available Current
QET2410	Q50 SPS	80	75	H V	13	G	0.8314 -0.6971	80.4	150
QET2415	Q50 SPS	80	75	H V	6	G K	-0.9084 0.7617	87.9	150
QET2430	Q50 SPS	80	75	H V	8	G K	0.9570 -0.7974	92.0	150
QET2435	Q50 SPS	80	75	H V	4	G K	-0.9870 0.7438	85.8	150
QET2440	Q50 SPS	80	75	H V	16	G K	0.8361 -0.7011	80.9	150
QET2445	Q50 SPS	80	75	H V	6	G K	-0.9868 0.8274	95.4	150
QET2450	Q50 SPS	80	75	H V	8	G K	1.0567 -0.8860	102.2	150
QET2460	Q50 SPS	80	75	H V	4	G K	-1.0500 0.8804	101.5	150
QET2465	Q50 SPS	80	75	H V	9	G K	0.6602 -0.5536	63.8	150
QET2470	Q50 SPS	80	75	H V	13	G K	0.3613 -0.3030	34.9	150
QET2475	Q50 SPS	80	75	H V	8	G K	-0.3394 0.2846	32.8	150

**[N.B.]** All references to sector 24 re QET2430 should be to sector 25 re  
should read QET2570

\* to be confirmed  
from prototype

Quadrupole Magnet Operating Requirements - Ejection Line AA Ring to TTL2

Name	Type Origin	Pole tip diameter (mm)	Vacuum tube I.D.	Plane	Required			Apertures			Required RADIO	Required RAD11	Required RAD12	Required RAD3	Required strengths G in kG/cm <sup>2</sup>	Required RAD10	Required RAD11	Required RAD12	Required RAD3	Required RAD10	Required RAD11	Required RAD12	Required RAD3	Available current	
					RAD10	RAD11	RAD12	RAD10	RAD11	RAD12															RAD10
QF105	QFL ISR																							300	
QF107	QPL ISR																							300	
QIN0005	QD ISR	91	86	H	11	23	11	11	11	12	21	21	21	25	4										500
QIN0015	QD ISR	91	86	H	41	15	15	15	15	38	16	16	38	25	4										500
QIN0030	QD ISR	91	86	H	22	34	23	23	24	16	37	37	67	10	4										500
QIN0035	QD ISR	91	86	H	34	17	31	31	31	27	10	10	67	27	4										500
QIN0050	L60-1000 EP	60	56	H	38	43	23	23	15	11	36	36	10	4	10k										3500
QIN0052	L60-1000 EP	60	56	H	25	36	15	15	10	8	32	32	10	4	10k										3500
QIN0055	L40-420 EP	40	35	H	17	23	12	12	8	8	16	16	8	4	10k										3500
QIN0056	L40-420	40	35	H	15	19	11	11	8	8	11	11	8	4	10k										3500
Target Beam Size					1.5		2		3		3		3		1.5		2		3		3		3		

Quadrupole Magnet Operating Requirements - Injection Line from TT2 to Antiproton Production Target



Name	Type Origin	Pole gap (mm)	Plane	Available Aperture	Required Apertures							Bending Angle (deg)	Tilt Angle (deg)	Required Current	Available Current
					AAD0	AAD11	AAD2	AAD3	AD1	AD7					
BTI0000	HBT ISR	80	H V	48 48	18 16	18 16	18 16	18 16				40.22	14.09	1466	400
BTI0001	HBT ISR	80	H V	48 48	14 18	14 18	14 18	15 18				40.22	14.07	1466	400
BTI0010	B190 SPS	52	H V	100 48	16 19	16 19	16 19	14 23				36.22	14.04	376	400
BTI0011	B190 SPS	52	H V	100 48	20 16	20 16	21 16	16 25				36.22	13.99	376	400
BVT0040	B19 SPS	52	H V	48 100	36 25	30 22	28 17	23 31				37.07	90.00	400	430
DH20070	VBS ISR	108	H V					93 88				78.54	0.00	375	500
BTI2420	B190 SPS	52	H V						5			239.44	17.56	340	430
BTI2455	B190 SPS	52	H V						6			264.52	15.36	376	430

Bending Magnet Operating Conditions - Injection and Ejection Lines