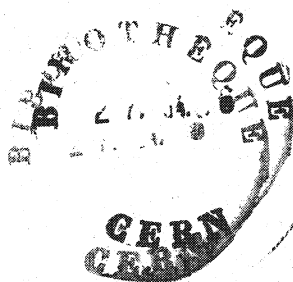


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**A data reduction program
for the linac total-
scattering amorphous
materials spectrometer
(LINDA)**

J. H. Clarke
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AERE Harwell, Oxfordshire
January 1976

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**A DATA REDUCTION PROGRAM FOR THE LINAC TOTAL-SCATTERING
AMORPHOUS MATERIALS SPECTROMETER (LINDA)**

J.H. Clarke*

ABSTRACT

A computer program has been written to reduce the data collected on the A.E.R.E., Harwell linac total-scattering spectrometer (TSS) to the differential scattering cross-section. This instrument, used for studying the structure of amorphous materials such as liquids and glasses, has been described in detail [1]. Time-of-flight spectra are recorded by several arrays of detectors at different angles using a pulsed incident neutron beam with a continuous distribution of wavelengths.

The program performs all necessary background and container subtractions and also absorption corrections using the method of Paalman and Pings [2]. The incident neutron energy distribution is obtained from the intensity recorded from a standard vanadium sample, enabling the observed differential scattering cross-section $\frac{d\sigma}{d\Omega}(\theta, \lambda)$ and the structure factor $S(Q)$ to be obtained.

Various sample and vanadium geometries can be analysed by the program and facilities exist for the summation of data sets, smoothing of data, application of Placzek corrections [3] and the output of processed data onto magnetic tape or punched cards.

A set of example data is provided and some structure factors are shown with absorption corrections.

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ILLUSTRATIONS

FIGURE

- 1 The geometrical arrangement of the spectrometer
- 2 The energy distribution of the incident beam
- 3 The input spectra for the program normalised for monitor counts
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1. Introduction

A schematic diagram of the spectrometer is shown in Fig. 1. A more detailed description of the apparatus is given by Sinclair et al [1].

Pulsed neutrons, at a repetition rate of 192 Hz, are incident on the sample from the moderator. The energy distribution of these neutrons is shown in Fig. 2. The time taken for each neutron after emission from the moderator to travel the 4.75m to the detector is called its time-of-flight. Between each burst it is possible to record the arrival of these neutrons and to sort them into 2048 channels of width 2 μ s. An initial timing delay of a few hundred μ seconds is used in the system to select neutrons with the shortest wavelength of interest.

After some hours a time-of-flight distribution will have been recorded for each detector. In general, each experiment would consist of several samples, e.g. sample, container, vanadium and background.

The samples may be changed automatically after a preset monitor count, usually taking some minutes, so that several time-of-flight distributions can be recorded for different samples and detectors. These distributions can be written onto magnetic tape for subsequent analysis using the computer program described in this report. The collection of the time-of-flight data and the transfer to magnetic tape is described in the program DATIN and TAPRIT, Johnson [2].

2. Calculations used in this program

(a) The Q-value

If it is assumed that the scattering process was elastic with no recoil of the scattering molecule the velocity of the neutron is given by:

$$V = \frac{L_0 + L_S}{ID + (n - \frac{1}{2}) \Delta t} \quad \dots (1)$$

ID is the initial timing delay or the time period after the firing of the electron pulse at which the counting began, n is the number and Δt is the width of the time channel, L_0 and L_S are the lengths of the initial and secondary flight paths. The Q-value for this event is given by:

$$Q = \frac{4\pi \sin(\theta/2)(L_0 + L_S)252.7}{ID + (n - \frac{1}{2})\Delta t} \quad \dots (2)$$

Where θ is the angle of the detector (scattering angle). If L_0 and L_s are in metres, ID and Δt are in microseconds then Q will be in reciprocal Ångströms.

If in the model adopted for the data analysis the nucleus of effective mass number M is allowed to recoil then:

$$Q = \frac{2\pi(L_0 + L_s)252.7}{[ID + (n - \frac{1}{2})\Delta t] x} \left(\frac{L_s}{L_0} + \left[1 - \frac{L_s}{L_0} \right] x \right) \sqrt{1 + x^2 - 2 x \cos\theta} \quad \dots (3)$$

and

$$x = \sqrt{1 - \frac{2M}{(M+1)^2} \left\{ 1 - \cos \left[\theta + \sin^{-1} \left(\frac{\sin\theta}{M} \right) \right] \right\}} \quad \dots (4)$$

x is the ratio of the neutron velocity after being scattered to its initial velocity.

One of the three options can be requested for the form of the output data. These are Q -value, time-of-flight or wavelength. The recoil correction can be requested but the default option in the program will calculate the Q -scale from equation (2).

(b) The scattered intensity $I^S(Q)$

If time-of-flight distributions are recorded for a sample and container $I^{S+C}(Q)$ and for an empty container $I^C(Q)$, then the sample intensity $I^S(Q)$ is:

$$I^S(Q) = \frac{I^{S+C}(Q)}{M^{S+C} \text{ Ass}} - \frac{I^C(Q) \text{ Acs}}{M^C \text{ Ass Acc}} \quad \dots (5)$$

M^{S+C} and M^C are the monitor counts for the two experiments. Ass, Acc and Acs are correction terms for absorption effects, calculated for cylindrical samples by the technique of Paalman and Pings [3].

For flat plates a similar calculation is performed. If A_1 is the attenuation factor for one window of the container of thickness t_w where;

$$t_w = (t_c - t_s)/2$$

with t_c and t_s the inner and outer widths of the can, and if A_2 is the attenuation factor for the sample then it can be shown that;

In transmission ($\theta \leq \pi/2$)

$$I^S(Q) = \frac{I^{S+C}(Q)}{A_1^2 A_2} - \frac{I^C(Q)}{A_1^2} \quad \dots (6)$$

Where
$$A_1 = \frac{\cos\phi\cos(\theta-\phi)}{\rho_c t_w \sigma_c [\cos\phi - \cos(\theta-\phi)]} \left\{ \exp \left[-\frac{\rho_c \sigma_c t_w}{\cos\phi} \right] - \exp \left[-\frac{\rho_c \sigma_c t_w}{\cos(\theta-\phi)} \right] \right\} \quad \dots (7)$$

and
$$A_2 = \frac{\cos\phi\cos(\theta-\phi)}{\rho_s t_s \sigma_s [\cos\phi - \cos(\theta-\phi)]} \left\{ \exp \left[-\frac{\rho_s \sigma_s t_s}{\cos\phi} \right] - \exp \left[-\frac{\rho_s \sigma_s t_s}{\cos(\theta-\phi)} \right] \right\} \quad \dots (8)$$

In reflection ($\theta \geq \pi/2$)

$$I^s(Q) = \frac{I^{s+c}(Q)}{A_1^2 A_2} - \frac{I^c(Q)(1 + A_1^2 A_2^2)}{(1 + A_1^2) A_1^2 A_2} \quad \dots (9)$$

Where
$$A_1 = \frac{\cos\phi\cos(\theta+\phi)}{\rho_c t_w \sigma_c [\cos\phi - \cos(\theta+\phi)]} \left\{ \exp \left[-t_w \rho_c \sigma_c \left(\frac{1}{\cos\phi} - \frac{1}{\cos[\theta+\phi]} \right) \right] - 1 \right\} \quad \dots (10)$$

and
$$A_2 = \frac{\cos\phi\cos(\theta+\phi)}{\rho_s t_s \sigma_s [\cos\phi - \cos(\theta+\phi)]} \left\{ \exp \left[-t_s \rho_s \sigma_s \left(\frac{1}{\cos\phi} - \frac{1}{\cos[\theta+\phi]} \right) \right] - 1 \right\} \quad \dots (11)$$

ϕ is the angle between the incident beam and a vector drawn normal to the can surface. θ is the scattering angle and σ_s and σ_c are the sample and can removal cross-sections (absorption + scattering).

Equations (7) and (8) above describing the attenuation of a plate in transmission geometry have a singularity when the scattering process is symmetric i.e. when $2\phi = \theta$. This is overcome in the program by setting the attenuation factor equal to the value obtained at $\theta = 0^\circ$ as for symmetric scattering the neutron path lengths are identical. So that

$$A_1 = \exp \left[-\frac{\rho_c \sigma_c t_c}{\cos\phi} \right] \quad (2\phi = \theta) \quad \dots (7a)$$

and
$$A_2 = \exp \left[-\frac{\rho_s \sigma_s t_s}{\cos\phi} \right] \quad (2\phi = \theta) \quad \dots (8a)$$

The calculated value of this attenuation factor should be compared with the experimentally observed transmission ratio on the downstream fission chamber which is evaluated in the program when $\theta = 0^\circ$ as,

$$R_s(t) = \frac{I^{c+s}(t) M^c}{I^c(t) M^{c+s}} = 1 - \exp \left[- \frac{t_s \rho_s \sigma_s^{(abs+scatter)}}{\cos \phi} \right]$$

for both sample and vanadium. The calculated value of this ratio is also plotted as a continuous line.

The sub-routine ABSORP evaluates these terms. As the incident neutrons have an energy distribution, the absorption cross-section is computed for each time channel and the program requires the value of the absorption cross-sections at 1.88Å as provided in BNL-325 [4].

The total cross-section may also be used in the Paalman and Pings routine to give a correction for self-shielding i.e. the reduction of the intensity of the incident beam by the scattering of the sample. The effect of this correction on any subsequent multiple scattering correction must be considered. The scattering cross-section is read by the program through the sub-routine, READ1. It requires the cross-section as a two dimensional array of energy versus cross-section of up to 40 values.

The function BARN1 interpolates this array to produce a scattering cross-section for ABSORP if required and for the calculation of S(Q), the structure factor. The default state of the program does not apply a self-shielding correction.

If the energy variation of the scattering cross-section is not used in the program, then the provision of one cross-section value at any energy will cover the whole spectrum.

(c) **The spectrum shape I^V(Q)**

A standard sample of vanadium is studied together with the background. Because vanadium is an almost isotropic, incoherent neutron scatterer, the measured time-of-flight distribution, after background subtraction and absorption correction, represents the energy distribution of the incident neutron beam as shown in Fig. 2.

The measured sample intensity I^S(Q) can then be divided by the appropriate component of the incident energy spectrum I^V(Q). The vanadium standard, which may be a cylinder, an annular sleeve (to reduce absorption) or a flat plate, is corrected for self-absorption and the normalized counting ratio R(Q) is obtained if the parameter CRYOST=T is coded in the data list &CONTRL.

$$R(Q) = \frac{\frac{I^{S+c}(Q)}{M^{S+c} A_{ss}} - \frac{I^c(Q) A_{cs}}{M^c A_{ss}}}{\frac{I^{v+b}(Q)}{M^{v+b} A_{vss}} - \frac{I^b(Q)}{M^b A_{vss}}} \quad \dots (12)$$

The absorption corrections are simpler for the vanadium standard because there is negligible absorption of neutrons by the background. M^b and M^{v+b} are the background and vanadium monitor counts and A^{vss} is the self absorption of the vanadium sample.

An additional correction may be made for the absorption of the background intensity by the sample. In equation (5) Section 2(b) the Paalman and Pings absorption correction procedure reduces the intensity of the empty container $I^c(Q)$ by the factor Acs . This represents the absorption of neutrons which are scattered by the container and absorbed by the sample. However, a proportion of these neutrons $I^b(Q)$ are not from the container but are due to external background sources such as air scattering in the counter aperture and in the incident collimator.

If these neutrons are assumed to have passed through the sample en route to the detector, too large a background contribution will be subtracted, particularly in the case of strongly absorbing samples such as bromine or carbon tetrachloride. This is best corrected experimentally by evacuating the sample area as in a cryostat or furnace.

If a vacuum enclosure has been used the ratio $R(Q)$ is calculated according to equation (12). However, if air scattering was present, an option exists in the program to calculate $R(Q)$, i.e. if `CRYOST=F` in the list `&CONTRL`.

$$R(Q) = \frac{\left[\frac{I^{s+c}(Q)}{M^{s+c}} - \frac{I^b(Q)}{M^b} \right] \frac{1}{A^{ss}} - \left[\frac{I^c(Q)}{M^c} - \frac{I^b(Q)}{M^b} \right] \frac{Acs}{A^{ss}Acc}}{\left[\frac{I^{v+b}(Q)}{M^{v+b}} - \frac{I^b(Q)}{M^b} \right] \frac{1}{A^{vss}}} \quad \dots (13)$$

(d) The observed differential scattering cross-section $\frac{d\sigma}{d\Omega}(\theta, \lambda)$ at each angle

The differential scattering cross-section $\left. \frac{d\sigma}{d\Omega} \right|^{eff}$ can be calculated at each detector angle by using the known scattering cross-section of the vanadium standard so that if the parameter `EXPO=T` is coded in the input list `&CONTRL`,

$$\left. \frac{d\sigma}{d\Omega} \right|^{eff} = \frac{R(Q) A_v [1 - \exp(-\rho_v \sigma_v t_v)] \sigma_s^T}{A_s 4\pi [1 - \exp(-\rho_s \sigma_s t_s)]} \quad \dots (14)$$

$R(Q)$ is the ratio (12,13), ρ_v and ρ_s are the number of atoms and molecules per cubic Ångström in the vanadium and sample respectively, t_v and t_s are the effective plate thicknesses of the vanadium and

sample in centimetres, A_v and A_s are the effective areas, σ_s^T is the total scattering cross-section of the sample and σ_v is the scattering cross-section of vanadium.

For a cylinder radius r , the effective plate thickness is

$$2rt = \pi r^2$$

$$t = \frac{\pi r}{2} \quad \dots (15)$$

and $A = 2r$ is the area/unit height presented to the beam.

This function is tabulated and plotted for each counter. If EXPO=F is coded in the input list &CONTRL, a simpler formalism is used.

$$\left. \frac{d\sigma}{d\Omega} \right|_{\text{eff}} = \frac{R(Q) r_v^2 \rho_v \sigma_v}{r_s^2 \rho_s} \quad \text{if VROD=T \& SROD=T} \quad \dots (16)$$

$$\left. \frac{d\sigma}{d\Omega} \right|_{\text{eff}} = \frac{R(Q) (r_v'^2 - r_v^2) \rho_v \sigma_v}{r_s^2 \rho_s} \quad \text{if VCOIL=T \& SROD=T} \quad \dots (17)$$

and

$$\left. \frac{d\sigma}{d\Omega} \right|_{\text{eff}} = \frac{R(Q) t_v \rho_v \sigma_v \cos \theta_s}{t_s \rho_s \cos \theta_v} \quad \text{if VPLATE=T \& SPLATE=T} \quad \dots (18)$$

where r_s , r_v , r_v' and r_v'' are the radii of the sample and vanadium and θ_s , θ_v are the angles of the normals of the plates to the beam.

(e) The structure factor $S(Q)$ at each angle

The structure factor $S(Q)$ can be calculated at each angle by the expression

$$S(Q) = 1 + \frac{4\pi}{\sigma_s^{\text{coh}}} \left. \frac{d\sigma}{d\Omega} \right|_{\text{eff}} - \frac{\sigma_s^T}{\sigma_s^{\text{coh}}} \left\{ 1 + P1 + P2 + \frac{P3}{Q^2} \right\} \quad \dots (19)$$

σ_s^{coh} is the sample coherent scattering cross-section, P1, P2 and P3 are Placzek correction terms [5-7].

These are

$$P1 + P2 = \frac{2}{M} \left[1 - f(1-2n) \right] \sin^2 \frac{\theta}{2} + \frac{2}{M^2} \left[1 - f(1-2n)(1+2nf) \sin^2 \frac{\theta}{2} \right] \sin^2 \frac{\theta}{2} \quad \dots (20)$$

and

$$P3 = \frac{1.9366\bar{E} \sin^2 \theta}{3MQ^2} \frac{\theta}{2} \left[\cos \theta - 2f(1+2n)(1 - 2f[1+n] \sin^2 \frac{\theta}{2}) \right]$$

Where \bar{E} is the mean kinetic energy of the molecule in meV and M is the effective molecular mass in amu. f is the fractional flight path;

$$f = \frac{L_s}{L_o + L_s} \quad \dots (21)$$

and n is the spectrum index ($\approx .83$) [7].

S(Q) is listed and plotted for each counter. In addition if specified in the input options, S(Q) or $\left. \frac{d\sigma}{d\Omega} \right|^{eff}$ will be punched to cards as Q,S(Q) or $\left[Q, \left. \frac{d\sigma}{d\Omega} \right|^{eff} \right]$.

Due to the complexity of Placzek corrections [6,7,10] for a linac experiment, it is suggested that a user wishing to apply his own form of corrections should use this program to evaluate the observed differential scattering cross-section $\left. \frac{d\sigma}{d\Omega} \right|^{eff}$. These data may be then obtained on cards for subsequent Placzek correction.

(f) The deadtime correction

The mathematical formalism used to correct for the effect of a deadtime in the counting system has been described by Egelstaff [8]. If there are n_d dead channels after each recorded count and there are a total of N machine cycles, then the true count in channel n is given by

$$C_n^1 = \frac{C_n N}{\left[N - \sum_{m=n-n_d}^{m=n-1} C_m \right]} \quad \dots (22)$$

In the PDP-11 computer used to record data on the Linac total-scattering spectrometer, each detector has a separate input buffer store so that the deadtime corrections are not cross-linked between different counters.

(g) Equal Q-steps option

In the study of liquids and glasses most forms of data analysis, Fourier transforms in particular, require the data to be in equal Q-value increments.

As the data are collected as time-of-flight spectra the data increments as a function of Q-value are inversely proportional to the time-of-flight and are non-linear.

The option of equal Q-value steps is specified by

EQUALQ=T in &LINAC Section 3(b) (Default is T)

The routine QBIN first reads the stored $S(Q)$ or $\left. \frac{d\sigma}{d\Omega} \right|_{\text{eff}}$ from a scratch disc. A set of data points are then produced at $.002\text{\AA}^{-1}$ intervals by linear interpolation using a cubic spline. This distribution is then smoothed by a rectangular smoothing function, Section 2(h). The width of this function is the fractional Q-value resolution for each detector. Default values are used in the program but can be overwritten. Data points are then obtained from every 0.05\AA^{-1} Q-value point in the spectrum. These values are listed, plotted and, if required, punched to cards. The namelist &QEQUAL is described in Section 3(j).

(h) Data smoothing options

Two options exist for smoothing data in the program and can both be specified in the &CONTRL list described in Section 3(f).

- (i) SMOOTH=T, will smooth the vanadium and background patterns.
- (ii) CAN=T, will smooth the container pattern.

The routine SMTH removes the peak due to the Linac Cell I neutron booster. This is observed in Cell II between 2550 and 2750 μsecs , after the firing of the electron pulse. The routine linearly interpolates the pattern between the two intensities at 2550 μsecs and 2750 μsecs .

A rectangular smoothing function is then convoluted with the data. The width of this function is equal to the incident neutron pulse width and is thus proportional to the time-of-flight channel number.

The smoothed intensity $I_s(\bar{t})$ is given by

$$I_s(\bar{t}) = \frac{\sum_{t_1}^{t_2} I(t) \Delta t}{t_2 - t_1} \left[\begin{array}{l} t_1 = \bar{t} - w\bar{t} \\ t_2 = \bar{t} + w\bar{t} \end{array} \right] \quad \dots (23)$$

t_1 and t_2 are the lower and upper time limits and w is the fractional pulse width. The default value for w is 0.1, this can be overwritten in the name list, &CONTRL. SMTH plots graphs of each pattern after smoothing which are compared with the input data.

The use of the smoothing option is not advisable if there are Bragg peaks present in the data.

3. The format of the input data

(a) Use of the NAMELIST statement

The IBM function NAMELIST is used to input the majority of the program control data. This function is described in greater detail in [9]. Briefly, a list of variables is specified in the program and read into the program in a simple format, e.g. the list called LINAC is read as follows

```
&LINAC NRUN=1, ID=390, TFP=4.615, ....., &END
```

The first column of each card must be blank and the keywords LINAC and END must be preceded by Ampersands. The variables can be listed in any order. If a variable is not listed the program uses a default option. Logical variables such as ABSORB can be assigned values by the statements ABSORB=.TRUE. or ABSORB=T.

Multiple values may be input in two ways, e.g.

```
NC = 0,0,0,0,1,0,0,0,
```

```
or NC = 4*0,1,3*0,
```

All data relevant to the recorded data will be written onto the header block of the magnetic tape, e.g. monitors, counter angles etc. These data can also be overwritten by the input list described in this section. A minimum default input case is shown in section 4 together with a maximum input case.

All namelist parameters are printed on channel 13 immediately after they have been read.

(b) The calling routine &LINAC

&LINAC has the following variables of which the majority are default values written on the control block of the magnetic tape.

Variable	Description	Program-supplied value
<u>VOLUME</u>	'Name of magnetic tape' in apostrophes e.g. 'A3CMPH'	No default
<u>NC(8)</u>	Number of counters at each angle	(8*1)
<u>TRANS(8)</u>	If .TRUE. sample was studied in transmission If .FALSE. sample was studied in reflection (Applies to flat-plate experiments only)	.TRUE.

Unless there is a special reason, from this point the remaining variables need not be coded.

Variable	Description	Program-supplied value
NRUN	No. of sets of data to be analysed	1
ID	Initial timing delay in microseconds	Read from tape
TFP	Total flight path in metres	Read from tape
SFP	Second flight path in metres	Read from tape
CA(8)	Counter angles in degrees	Read from tape
ITAPE	7 or 9-track input tape	9
<u>EQUALQ</u>	If .TRUE. the routine QBIN is called and the data will be placed in equal Q-steps	.TRUE.
<u>MON</u>	If .TRUE. monitors will be read from tape If .FALSE. monitors will be read from cards	.TRUE.
DEAD	If .TRUE. deadtime corrections are applied	.TRUE.
NDEAD	No. of dead channels in TOF scaler	Read from tape
CHAN	Width of TOF channels in microseconds (integer)	Read from tape
NCTRS	No. of counters written on tape	Read from tape

The program then reads a list of runs required which must be on the magnetic tape. The list is in free format so that the last run number must be followed by a slash. These runs are read from the magnetic tape and then stored on a disk for random access. The magnetic tape input channel is 10 and the disk channel is 1. There are ITMAX (≤ 80) runs.

e.g. &LINAC VOLUME='A3CMPH',NC=3*1,5*0,&END
 2101 2102 2103 2104 2105 2109 2107 2108 2200
 2250 2760/

or if the control record on the tape is incorrect;

 &LINAC VOLUME='A3CMPH',NC=3*1,5*0,MON=F,CA=15.,25.,38.,
 5*0., ID=236,&END
 2101 2102 2103 2104/

(c) The title and run numbers

The program from this point onwards is called NRUN times with the following variables.

TITLE 72 characters describing the experiment (18A4)

Run Number, Run type (1 to 4), Monitors for each counter if MON=F (Free Format Input)

If the monitors are to be read from the magnetic tape then input;

Run Number, Run type

The last run must have a negative number on input, e.g.

2110	1
2111	2
2113	3
-2114	4

The program will use this as a sentinel and then reset it positively to its true value.

The run types are:

1. Sample + Can
2. Can
3. Vanadium + Background
4. Background

All runs of the same type will be added together including their monitors.

There are $JMAX < 80$ runs acceptable

e.g.	24610	1	Three sample runs
	24620	1	One can run
	24630	1	One vanadium run
	24611	2	Three background runs
	24612	3	
	24613	4	
	24623	4	
	-24633	4	

(d) The scattering cross-sections via the routine READ1

READ1 is called three times to input the scattering cross-section versus energy mesh for the sample, container and vanadium.

e.g. Energy, Cross-section, Sentinel (2F10.0,I1)

Sentinel = -1 for the final card, up to a maximum of 40 cards. The program sets the integers IMAX1, IMAX2 and IMAX3 as the sizes of the arrays. The energy is in eV and the Cross-section is in barns/molecule.

e.g. 0. 5.13 1 If only one card is provided for each type the program will execute more quickly.

(e) **The absorption cross-sections &SIGMA**

The three absorption cross-sections are read into the program via the namelist &SIGMA.

&SIGMA SABS = Sample Absorption Cross-section
CABS = Can Absorption Cross-section
VABS = Vanadium Absorption Cross-section
SCOH = Sample Coherent Scattering Cross-section

Absorption cross-sections are in barns/molecule at 2200 m/sec and are usually taken from BNL 325 [4].

e.g. &SIGMA SABS=3.9, CABS=4.98, VABS=4.98, SCOH=22.8, &END

(f) **The control statement, &CONTRL**

The namelist &CONTRL specifies all the options used by the program. Default values are specified for all variables.

Variable	Description	Default Value
PRINT	List all input data	F
PLOT	Plot graphs	T
PUNCH	Punch output data	F
SCATTR	Use scattering cross-section in ABSORP	F
ABSORB	Apply absorption corrections	T
Q	Compute Q-scale \AA^{-1}	F
TOF	Compute Time-of-flight scale μsec	F
LAMBDA	Compute Wavelength scale \AA	F
CRYOST	Is sample in vacuum enclosure?	F
SMOOTH	Smooths vanadium and background	F
CAN	Smooths container	F
W	Pulse width for smoothing option $0 < W < 1.0$.1
EXPO	Uses exponential scattering formalism	F
SMQ	Punches $S_m(Q)$ to cards and puts $S_m(Q)$ into equal Q.steps	T

If .FALSE. does these operations for $\left. \frac{d\sigma}{d\Omega} \right|_{\text{eff}}$

e.g. &CONTRL PRINT=T, Q=T, SMOOTH=T, &END.

(g) Control data for graphs &SCALE

The scale of the graphs of S(Q) can be specified at this stage if desired.

&SCALE SQMAX=8 Values, SQMIN=8 Values, XMAX=8 Values,
XMIN=8 Values, &END

SQMAX(1)=YMAX for counter 1

SQMIN(2) =YMIN for counter 2

XMAX(3) =XMAX for counter 3 etc.

The graphs are scaled automatically if these values are zero.

e.g. &SCALE SQMIN=8*0., SQMAX=2.,2.5,6*3., &END

(h) The sizes and geometry of the sample and vanadium &SIZES, &DENSTY

The namelist &SIZES specifies all the shapes and dimensions of the sample, can and vanadium.

RADIUS defines the dimensions of either a cylinder or plate depending on the variables SROD, SPLATE, VROD, VCOIL and VPLATE

SROD = Sample is a cylinder (F)

SPLATE = Sample is a plate (F)

VROD = Vanadium is a cylinder (F)

VCOIL = Vanadium is an annular coil (F)

VPLATE = Vanadium is a plate (F)

If the sample is a cylinder, i.e. SROD=T, then;

RADIUS(1)=Sample radius in cm.

RADIUS(2)=Can radius (external) in cm.

RADIUS(3)=Increment in radius for absorption integral in cm.

$\left[\frac{\text{RADIUS}(1)}{\text{RADIUS}(3)} \right]$ and $\left[\frac{\text{RADIUS}(2)}{\text{RADIUS}(3)} \right]$ must be integers ≤ 20

If the sample is a plate, i.e. SPLATE=T, then;

RADIUS(1)=Thickness of sample in cm.

RADIUS(2)=Outer thickness of can in cm. [RADIUS(2) > RADIUS(1)]

RADIUS(3)=Angle of normal to plate with the incident beam in degrees.

In transmission RADIUS(3)=0. and in general $0 \leq \text{RADIUS}(3) \leq 90$.

If the Vanadium is a cylinder, i.e. VROD=T, then;

RADIUS(4)=Vanadium rod radius in cm.

RADIUS(5)=Not used.

RADIUS(6)=Increment in radius for absorption correction in cm.

$$\left[\frac{\text{RADIUS}(4)}{\text{RADIUS}(6)} \right] \text{ must be an integer } \leq 20$$

If the Vanadium is an annular coil, i.e. VCOIL=T, then;

RADIUS(4)=Inner radius of vanadium coil in cm.

RADIUS(5)=Outer radius of vanadium coil in cm.

RADIUS(6)=Increment in radius for absorption correction in cm.

$$\left[\frac{\text{RADIUS}(4)}{\text{RADIUS}(6)} \right] \text{ and } \left[\frac{\text{RADIUS}(5)}{\text{RADIUS}(6)} \right] \text{ must be integers } \leq 20.$$

If the Vanadium is a plate, i.e. VPLATE=T, then;

RADIUS(4)=Thickness of vanadium plate in cm.

RADIUS(5)=Not used.

RADIUS(6)=Angle of normal to plate with the incident beam in degrees.

$$0 < \text{RADIUS}(6) \leq 90.$$

WIDTH=Beam width in cm.

HEIGHT=Beam height in cm.

A second namelist &DENSTY specifies the densities of the sample, can and vanadium.

SDENS = Sample density (gm.cm⁻³)

CDENS = Can density (gm.cm⁻³)

VDENS = Vanadium density (gm.cm⁻³)

SMW = Sample Molecular Weight

CMW = Can Molecular Weight

VMW = Vanadium Molecular Weight (50.942)

e.g. &SIZES RADIUS = .5,.55,.05,.6,.7,.05, WIDTH = 2.5, HEIGHT = 2.5, VROD=T,
SROD = T, &END

or &SIZES RADIUS = .5,.55,30.,.1,.2,30., WIDTH = 2.5, HEIGHT = 2.5,
SPLATE = T, VPLATE = T, &END

&DENSTY SDENS = 6.15., CDENS = 6.1, VDENS = 6.1,

SMW = 69., CMW = 50.9, VMW = 50.9, &END

(i) **Placzek corrections &PLZCK**

The namelist &PLZCK provides input of the mean kinetic energy of the molecule and the effective mass. If these are both zero no corrections are applied.

&PLZCK

EBAR = Kinetic energy in meV (0.)

ANU = Effective mass in A.M.U. (1.0E + 3)

(j) **Equal Q-step calculation &QEQUAL**

Variable	Description	Default value
YMIN(8)	Minimum value of y-axis in graph)	0. provides automatic scaling
YMAX(8)	Maximum y-axis value)	
SCALE	Scale factor i.e. $S(Q) = \text{SCALE} * S(Q)$	1
PUNCH	Punches $S_m(Q)$ or $\left. \frac{d\sigma}{d\Omega} \right _{\text{eff}}$ (depends on SMQ in &CONTRL)	F
QSTEP	Increment in Q-value	0.05 \AA^{-1}

In all the data input sections the program attempts to check the form of the data and will print messages if the data is unsuitable, e.g. if $[\text{RADIUS}(1)/\text{RADIUS}(3)]$ is >20 or if a flat plate sample is parallel to the beam. At this stage the program may now recycle starting with Section 3(c) again.

4. How to run the program (including a sample set of input data as used for liquid nitrogen)

The first example shows the minimum default input data required for a 9-track tape data set with all the control information correctly typed onto the header block. Counter angles, flight paths, initial delay and all information for &LINAC is read from the header of the first run. The monitors are read from each header. The second example shows the maximum default with every parameter input via the NAMELIST statements.

Default case

```
//G.SYSIN DD *
```

```
&LINAC NC=1,1,1,0, TRANS=4*T, &END
```

```
24779 24699 25128 25127 /
```

```
LIQUID NITROGEN 77K JHCLARKE UNIVERSITY OF KENT
```

```
24779 1
```

```
24699 2
```

```
25128 3
```

```
-25127 4
```

```

.001    22.8    1    SAMPLE SCATTERING X-SECTION
.001    5.13    1    CAN SCATTERING X-SECTION
.001    5.13    1    VANADIUM SCATTERING X-SECTION
&SIGMA SABS=3.7,CABS=4.98,VABS=4.98,SCOH=22.206,&END
&CONTRL Q=T,CRYOST=T,&END
&SCALE &END
&SIZES RADIUS=.55,.6,.05,.675,.72,.045,WIDTH=2.5,HEIGHT=2.5,
SROD=T,VCOIL=T,&END
&DENSTY SDENS=.81,CDENS=6.1,VDENS=6.81,SMW=28.,CMW=50.9,VMW=50.,
&END
&PLZCK ANU=17.,&END
&QEQUAL SCALE=.5,&END
/*

```

No default case

```

//G.SYSIN DD *
&LINAC NRUN=1,ID=390,TFP=4.615,SFP=0.4,ITAPE=9,CA=14.,28.,58.,
150., 150.,58.,28.,14.,NC=1,1,1,1,1,1,1,1,EQUALQ=T,CHAN=2,
NCTRS=8,VOLUME='BG7MPH',MON=F,TRANS=8*T,&END
24779 24699 25128 25127 /
LIQUID NITROGEN 77K JHCLARKE UNIVERSITY OF KENT
24779 1 32861 32861 32861 32861 32861 32861 32861 32861
24699 2 98290 98290 98290 98290 98290 98290 98290 98290
25128 3 70305 70305 70305 70305 70305 70305 70305 70305
-25127 4 68271 68271 68271 68271 68271 68271 68271 68271
.001    22.8
1.00    22.8    1
.001    5.13
1.00    5.13
2.00    5.13    1
0.001   5.13
1.000   5.13
2.000   5.13    1
&SIGMA SABS=3.7,CABS=4.98,VABS=4.98,SCOH=22.206,&END
&CONTRL PRINT=F,PLOT=T,PUNCH=F,SCATTR=F,ABSORB=T,Q=T,TOF=F,
LAMBDA=F,RECOIL=F,CRYOST=T,SMOOTH=T,CAN=T,W=.1,
EXPO=F,SMQ=T,&END

```

```

&SCALE SQMAX=2.,2.,2.,2.,2.,2.,2.,2.,2.,SQMIN=0.,0.,0.,0.,0.,0.,0.,
0.,XMAX=5.,10.,20.,35.,0.,0.,0.,0.,XMIN=8*0.,&END
&SIZES RADIUS=.55,.6,.05,.675,.72,.045,WIDTH=2.5,HEIGHT=2.5,
SROD=T,VCOIL=T,SPLATE=F,VPLATE=F,VROD=F,&END
&DENSITY SDENS=.81,CDENS=6.1,VDENS=6.81,SMW=28.,CMW=50.9,
VMW=50.9,&END
&PLZCK ANU=14.,EBAR=0.,&END
&QEQUAL YMIN=0.,0.,0.,0.,0.,0.,0.,0.,YMAX=2.,2.,2.,2.,2.,2.,
2.,2.,PUNCH=F,SCALE=.5,&END
/*

```

On the Harwell computer the program can be executed as follows:

```

//UIDxxx JOB (,HMPH,2,360,,7,1,,2000,1,,0,5),NAME
/*SETUP      31UMPH
/**MAGTAPE A3CMPH FP/...READ ONLY../FP
// EXEC LINDA,TAPE=A3CMPH,SEQ=1,
// PARM=*P="5" *L="YES" *T="TITLE"
//SYSIN DD *
(DATA)
/*

```

The procedure is an in-line catalogued procedure and is listed in Section 7. The parameters are as follows;

- (1) UID = User identifier code on the Harwell computer.
- (2) 31UMPH = Demountable Disk containing the program LINDA.
- (3) A3CMPH = Archive magnetic tape.
- (4) TAPE = A3CMPH, this expands into the full IBM tape control cards.
- (5) SEQ = 1,2 etc., this expands into the file on the magnetic tape e.g. LABEL=(SEQ,SL).
- (6) PARM = *P="5" etc is the input for the Harwell Ghost System [10].

5. An Explanation of the Form of the Output Data

An initial output page lists the information provided in &LINAC and also lists each run and its disposition on disk as it is found.

For each set of data the title is printed in a box at the top of the first page. The list of runs with their identifiers, monitors, etc. is printed, followed by the absorption cross-sections. The options

specified in &CONTRL are then printed followed by the sample, can and vanadium dimensions. Number densities and Placzek correction constants follow with the scattering cross-section versus energy meshes.

As each run is read off disk, a log is written on channel 12 specifying its control numbers and locations. For each sample and counter, mean and total values of counts per monitor are listed. The Paalman and Pings correction terms are tabulated for every 10th channel followed by the size of the Placzek correction terms P_1 , P_2 and P_3 .

Q and S(Q) are printed in two columns followed by Q and $\left. \frac{d\sigma}{d\Omega} \right|^{eff}$. This sequence is repeated for each counter. A running log of the computing time and the state of the graph plotter is also printed. Figures 3-5 show the input spectra for the program, the computed Paalman and Pings correction terms and $\left. \frac{d\sigma}{d\Omega} \right|^{eff}$ as plotted by the program for liquid nitrogen [11]. The form of the prepared data control block is given below.

LINAC Liquids Machine - Magnetic tape header block as prepared by DATIN

Position	Contents	Origin
1	No. of blocks for present sample	Calculated
2	No. of time channels per detector	Type in (default 2048)
3	Run number	Type in
4	Day)	
)	
5	Month)	From DOS
)	(Disk operating system)
6	Year)	
7	Sample No.	Calculated from interface
8	Total number of samples	Type in (default 1)
9	No. of counters	Type in (default 8)
10	Channel width in $1/10 \mu s$	(default 20)
11	Initial delay in $1/10 \mu s$	Type in
12	Total flight path in mm	(default 4750)
13	Second flight path in mm	(default 460)
14	Dead time in $1/10 \mu s$	(default 30)
15		
16		

Position	Contents	Origin
17-24	Monitors etc. for Ctr 1	
25-32	" " " 2	
33-40	" " " 3	
41-48	" " " 4	
49-56	" " " 5	
57-64	" " " 6	
65-72	" " " 7	
73-80	" " " 8	
81-100	Users name Type in	
128 →	General text	

For Each Counter

Position	Contents	Origin
1	Angle (1/100 degree)	Type in (default values)
2	Time (1/50 sec)	Calculated
3	prf	Calculated
4	mon 1	Calculated
5	mon 2	Calculated
6	mon 3	Calculated
7	mon 4	
8	mon 5	

6. Glossary of variable names

A(2048)	Sample + Can run and finally $\frac{d\sigma}{d\Omega}$ array \equiv SA.
AB(60,20)	$\alpha_{nm} + \beta_{nm}$ in Paalman and Pings [3] \equiv IARR.
ABSORB	If true, applies absorption corrections.
ABSORP	Subroutine to calculate Paalman and Pings correction terms [3].
ACC1(54)	A_{cc} array in Paalman and Pings [3] for sample and can.
ACS1(54)	A_{cs} array in Paalman and Pings [3] for sample and can.
ACS2(54)	A_{cs} array in Paalman and Pings [3] for vanadium.
ADUM	Unity.
ANU, ANO, ANØ	Atomic Mass.
AS(60,20)	$\alpha_{nm} + \beta_{nm} - \sigma_{nm}$ in Paalman and Pings [3] \equiv IARR.
ASS1(54)	A_{ss} array in Paalman and Pings [3] for sample and can.
ASS2(54)	A_{ss} array in Paalman and Pings [3] for vanadium.
B(2048)	Can data array \equiv SB.
BARN1	Function to generate cross-section for time channel IT from E, SIGMA arrays.
B2CON	Absorption cross-section constant = $.0022/TFP(\mu s.m^{-1})$.
B2C1	Absorption constant for can.
B2S1	Absorption constant for sample.
B2V1	Absorption constant for vanadium.
C(2048)	Vanadium + background run \equiv SC.
CA(8)	Counter angle in degrees, then changed to half-angle in radians.
CABS	Can absorption cross-section at 2200 ms^{-1} (barns).
CAN	If true, smooths can scattering.
CDENS	Can density (g cm^{-3}).
CHAN	Channel width in microseconds.
CMW	Can molecular weight.
CONTRL	Control data input list.
CRYOST	If true, computes cryostat-configuration absorption corrections.
CSUM(4)	Counts per monitor, etc. (working array).

D(2048)	Background data array \equiv SD.
DASH	-
DATE1 * 1(12)	Date in control record (ASCII) DATE1(1-12) \equiv JAY1(13-24)
DATE2 * 1(12)	Date in control record (EBCDIC).
DAY	Day of month.
DEAD	If true, applies deadtime corrections.
DEADT	Subroutine to apply deadtime corrections to data.
DENSTY	Number-density input list.
DISC	Routine to retrieve run from archive disk and sum monitors and machine pulses.
DRAW	Graph plotting subroutine.
DUMR	Dummy radius for vanadium rod.
EBAR	Mean energy of molecule.
ENU(60,20)	$\eta_{nm} + \nu_{nm}$ in Paalman and Pings [3] \equiv IARR.
EQUALQ	If true, computes equal Q-value data for $S_m(Q)$ or $\frac{d\sigma}{d\Omega}$ depending on the value of SMQ.
EXPO	If true, uses exponential scattering formalism.
EOCON1	Energy constant.
E1(40)	Energy array for SIGMA1.
E2(40)	Energy array for SIGMA2.
E3(40)	Energy array for SIGMA3.
FORM(20)	Free format input array ON02A.
FPI	$(4\pi) \ 4 \times 3.14159$.
FPIS	$(4\pi^2) \ 4 \times 3.14159^2$.
HCHAN	Half-channel width (μ s).
HEIGHT	Height of neutron beam (cm).

IARR(16384)	Data record on magnetic tape.
	IARR(1-16384) \equiv JAY3 * 1(1-65536)
	IARR(1-1200) \equiv AB(1,1)
	IARR(1-6144) \equiv WK(1-6144)
	IARR(1201-2400) \equiv SI(1,1)
	IARR(2401-3600) \equiv AS(1,1)
	IARR(3601-4800) \equiv ENU(1,1)
	IARR(4801-6000) \equiv NU(1,1)
	IARR(6001-8192) \equiv R(1-2192)
ICHNL	No. of time-channels per counter.
ICON(256)	Control record of magnetic tape.
	ICON(1-128) \equiv JAY1 * 1(1-512)
	ICON(129-512) \equiv JAY2 * 1(1-512)
ID	Initial delay in microseconds.
IDUM	Dummy.
IMAX1	Size of E1 and SIGMA1.
IMAX2	Size of E2 and SIGMA2.
IMAX3	Size of E3 and SIGMA3.
INC	Counter number in DO loops.
ITAPE	Number of input tape 7, 8, 9.
ITIND	Working integer.
ITMAX	Number of runs archived to disk.
JAY1 * 1(512)	Control record \equiv ICON(256).
JAY2 * 1(512)	
JAY3 * 1(65536)	Data \equiv IARR(16384).
JCY, JJJ	Run counters.
JMAX	Number of runs to be processed in this cycle.
JOBNAM * 8	Alphanumeric text-name of computer job.
JSHIFT	Working array shift.

LAMBDA	If true, computes wavelength scale.
LINAC	Spectrometer data input list.
M(8,80)	Monitor count for counter (1-8) run (1-80).
MON	If true, monitors are read from magnetic tape control record. If false, from cards.
MONTH	Month of year.
MPRF(8,80)	Machine pulses for counter (1-8) run (1-80).
NBLKS	Number of blocks on tape.
NC(8)	On-off switch for (1-8) counters.
NCPK	Number of tof channels per array element of ASS1 etc.
NCTRS	Number of detectors on the magnetic tape file.
NDEAD	Number of dead channels.
NM(8,80)	Monitor count array as read from archive.
NMPRF(8,80)	Machine pulse array as read from archive.
NRMAX	Maximum number of archive runs.
NRUN	Number of cycles of data.
NTRN(80)	List of input run numbers for archive disk.
NU(60,20)	ν_{nm} in Paalman and Pings [3] \equiv IARR.
OJOHNA	Modified Harwell routine to give tabular lineprinter output.
PI	(π) 3.14159.
PLOT	If true, plot all graphs.
PLZCK	Placzek input list.
PRINT	If true, print raw summed data.
PUNCH	If true, punches $S_m(Q)$ or $\frac{d\sigma}{d\Omega}$ to cards depending on value of SMQ.
P1,P2,P3,P4	Placzek correction terms.
Q	If true, computes Q-scale.
QK(1200)	Q-scale in QBIN routine.
R(2192)	Radius array in ABSORP (working array) \equiv IARR.
RADIUS(6)	Dimensions of sample, can and vanadium.

RADIUS(1)	Radius of sample or thickness of sample.
RADIUS(2)	Outer radius of can or outer thickness of sample.
RADIUS(3)	Increment for integral or angle of normal to beam.
RADIUS(4)	Radius of vanadium rod or thickness of vanadium plate, or inner radius of coil.
RADIUS(5)	Outer radius of coil. Not used.
RADIUS(6)	Increment in integral or angle of normal to beam.
RATIO(2048)	Working array and finally, S(Q) array.
RD	Initial delay μ s.
READ1	Reads E1,2,3 and SIGMA1, 2 and 3.
SA,SB,SC,SD	Single elements of arrays A,B,C,D.
SABS	Sample absorption cross-section at 2200 ms^{-1} (barns).
SCALE	Graph scale input list.
SCATTR	If true, uses scattering cross-sections (SIGMA1-3) in ABSORP.
SCOH	Sample coherent cross-section (barns).
SDENS	Sample density (g.cm^{-3}).
SFP	Second flight path in metres.
SI(60,20)	σ_{nm} in Paalman and Pings [3] \equiv IARR.
SIGMA	Absorption cross-section input list.
SIGMA1(40)	Scattering cross-section of sample array.
SIGMA2(40)	Scattering cross-section of container array.
SIGMA3(40)	Scattering cross-section of vanadium array.
SIZES	Sample dimensions etc. data input list.
SMOOTH	If true, smooths vanadium and background.
SMTH	Subroutine to smooth an array of data.
SMW	Sample molecular weight.
SMQ	If true, punches $S_{\text{m}}(Q)$, if false, $\frac{d\sigma}{d\Omega}$.
SPLATE	If true, sample is a plate.
SQMAX(8)	Maximum value of S(Q) for counter (1-8) for graph.
SQMIN(8)	Minimum value of S(Q) for counter (1-8) for graph.

SROD	If true, sample is a cylinder.
SST	$\sin (CA)^2$.
STAR	*
SUM(4,8,80)	No. of counts for sample type (1-4), counter (1-8) and run sequence (1-80).
T(2048)	Working array and Q, time-of-flight or wavelength array.
TAPE7	If true, data is input on PDP-4 magnetic tape.
TAPE8	If true, data is input from PDP-4 archive tape.
TAPE9	If true, data is input from PDP-11 archive tape.
TBEG,TEND,TDIFF	Elapsed time-constants.
TEXT * 1(192)	Alphanumeric text in control record (ASCII).
TEXT(1-192) =	JAY1(321-512).
TFP	Total flight path in metres.
TITLE(18)	72 character title.
TOF	If true, computes time-of-flight scale.
TXT * 1(80)	Alphanumeric text in control record (EBCDIC).
TYPE(80)	(1-4) run-type of run number RUN.
VABS	Vanadium absorption cross-section at 2200 ms^{-1} (barns).
VCOIL	If true, vanadium is an annulus.
VDENS	Vanadium density (g cm^{-3}).
VMW	Vanadium molecular weight.
VOLUME * 8	Alphanumeric text and name of magnetic tape volume.
VOLSP	Volume term for sample plate.
VOLSR	Volume term for sample cylinder.
VOLVC	Volume term for vanadium coil.
VOLVP	Volume term for vanadium plate.
VOLVR	Volume term for vanadium rod.
VPLATE	If true, vanadium is a plate.
VROD	If true, vanadium is a cylinder.
W	Smoothing width.

WIDTH	Width of neutron beam (cm).
WK(6144)	Working array in QBIN routine.
X	Ratio used in recoil correction $\left(\frac{\text{scattered neutron velocity}}{\text{incident neutron velocity}} \right)$.
XMAX(8)	Maximum and minimum values for X-axes in graphs.
XMIN(8)	
YEAR	Year.
Z	Zero.

7. LISTING OF CATALOGUED FARWELL PROCEDURE LINCA

```

//LINDA PROC TAPE=A3CMPH,TAPE7=7JRELA,FCS1='CUMMY.',SEQ=1,POS2=
// EXEC PGM=DISKPGM,CCND=EVEN,REGION=390K
//***** LINDA PROGRAM ON DISC MPH *****
//STEPLIB DD DSN=LCAD.MPH.JHCLINDA,VCL=REF=MPH,DISP=SHR
//***** CARD PUNCH *****
//SYSPCH DD SYSOLT=B,DCB=BLKSIZE=80
//***** SCRATCH DISC FILES FOR INPLT DATA *****
//FT01FC01 DD DISP=(NEW,DELETE),DSN=88DATA,VCL=REF=SCRATCH,
// SPACE=(CYL,(5,1),RLSE),CCB=(RECFM=VES,LRECL=1028,BLKSIZE=12340)
//***** CARD READER *****
//FT05FC01 DD DCNAME=SYSIN
//***** LINEPRINTER *****
//FT06FC01 DD SYSOLT=A,DCB=(RECFM=FA,BLKSIZE=133)
//***** CARD PUNCH *****
//FT07FC01 DD SYSOLT=B
//***** FILE FOR SUMMED COUNTERS *****
//FT08FC01 DD VCL=REF=SCRATCH1,SPACE=((8192,32),RLSE,CONTIG),DSN=88SUM
//***** ARCHIVE TAPE A3CMPH *****
//FT01FC01 DD &POS2,DISP=(OLD,KEEP),VCL=SER=8TAPE,
// LABEL=(8SEQ,SL),UNIT=(TAPE9,,DEFER),CSN=DATA.MPH.JHARCH,
// DCB=(RECFM=VS,LRECL=16388,BLKSIZE=16392,DEN=3)
//***** OUTPUT PRINT CHANNELS FOR LINEPRINTER *****
//FT11FC01 DD SYSOLT=A,DCB=(RECFM=FA,BLKSIZE=133)
//FT12FC01 DD SYSOLT=A,DCB=(RECFM=FA,BLKSIZE=133)
//FT13FC01 DD SYSOLT=A,DCB=(RECFM=FA,BLKSIZE=133)
//***** SCRATCH DISC FILE FOR EQUAL C-STEP *****
//FT14FC01 DD VCL=REF=SCRATCH1,SPACE=((8194,8),RLSE,CONTIG),CSN=88GRIN
//***** INPUT CHANNEL FOR 7-TRACK PDP-4 TAPE *****
//F1 DD 8POS1,UNIT=(TAPE7,,DEFER),VCL=SER=8TAPE7,DISP=(OLD,KEEP),
// DCB=(RECFM=F,BLKSIZE=768,DEN=0,CSFC=PS),LABEL=(2,NL)
//***** GHOST GRAPH PLOTTING JCL *****
//GRIDINX DD DISP=SHR,CSN=HAR,GRIDINX

//GRID DD VCL=REF=GRID,SPACE=(768,(2000,20),RLSE)
//SYSIN DD *
//M EXEC PGM=PPLP,REGION=140K,ACCT=GHCSTLF
//STEPLIB DD DSN=HAR.GHCSTLIB,DISP=SHR
//FT06FC01 DD SYSOLT=A
//SYSLDUMP DD SYSOLT=A
//FT49FC01 DD SYSOLT=A
//GRIDINX DD DSN=HAR,GRIDINX,DISP=SHR
//PRINT DD SYSOLT=A
//DDSP001 DD VOL=SER=SFCOL1,DISP=CLD,UNIT=3330
//DDSP002 DD VOL=SER=SFCOL1,DISP=CLD,UNIT=3330
//DD318COM DD VOL=SER=318COM,DISP=CLD,UNIT=3330
//DD319SYS DD VOL=SER=319SYS,DISP=CLD,UNIT=3330
//PROC PEND

```



```

C----- SPECTROMETER DATA ANALYSIS PROGRAM (LINDA) ----- 10
C==== MARK XLIV          5TH JANUARY 1976 ----- 20
C 30
C ***** 40
C * N1= NUMBER OF TIME-OF-FLIGHT CHANNELS PER COUNTER * 50
C * N2= NUMBER OF COUNTERS * 60
C * N3= TOTAL NUMBER OF RUNS * 70
C * N4= NUMBER OF TOTAL CROSS-SECTION VALUES * 80
C * N5= NUMBER OF INCREMENTS IN ABSORPTION INTEGRAL * 90
C * N6= NUMBER OF INTERPOLATION STEPS IN * 100
C * ABSORPTION CORRECTION TERMS * 110
C * N7= NUMBER OF Q-STEPS IN EQUAL Q-VALUE ROUTINE * 120
C ***** 130
C 140
C ***** 150
C * RATIO(N1) A(N1) B(N1) C(N1) D(N1) T(N1) * 160
C * SQMAX(N2) SQMIN(N2) XMAX(N2) XMIN(N2) * 170
C * RMC(N2,4) CA(N2) RPULSE(N2,4) * 180
C * M(N2,N3) MPRF(N2,N3) NM(N2,N3) NMPRF(N2,N3) SUM(4,N2,N3) * 190
C * NTRN(N3) TYPE(N3) RUN(N3) NSEQ(N3) * 200
C * SIGMA1(N4) SIGMA2(N4) SIGMA3(N4) E1(N4) E2(N4) E3(N4) * 210
C * AB(3*N5,N5) SI(3*N5,N5) AS(3*N5,N5) NU(3*N5,N5) ENU(3*N5,N5) * 220
C * ASS1(N6) ACC1(N6) ACS1(N6) ASS2(N6) ACS2(N6) * 230
C * QK(N7) RSK(N7) * 240
C ***** 250
C 260
C REAL NTP*8(4) / 'SAMPLE', 'CAN', 'VANADIUM', 'BACKGRND' /, 270
C * RATIO(2048),A(2048),B(2048),C(2048),D(2048),T(2048), 280
C * SUM(4,8,80)/2560*0./,RMC(8,4)/32*0./,RPULSE(8,4)/32*0./, 290
C * SIGMA1(40),SIGMA2(40),SIGMA3(40),E1(40),E2(40),E3(40), 300
C * SQMAX(8)/8*0./,SQMIN(8)/8*0./,XMAX(8)/8*0./,XMIN(8)/8*0./, 310
C * AB(60,20),SI(60,20),AS(60,20),ENU(60,20),NU(60,20), 320
C * ASS1(54)/54*1./,ACC1(54)/54*1./,ACS1(54)/54*1./, 330
C * ASS2(54)/54*1./,ACS2(54)/54*1./, 340
C * VOLUME*8 / 'UNKNOWN' /, 'JOBNAM' *8 / ' ' /, 350
C * CA(8)/8*0./,CSUM(4),RADIUS(6),TITLE(18),FORM(20),K(2192), 360
C * WK(6144),QK(1200),RSK(1200),DSN*8(3)/3*0 370
C 380
C INTEGER ICUN(256),IARR(16384),DAY,YEAR,CHAN/8/, 390
C * NTRN(30)/8*0./,RUN(80)/8*0./,TYPE(80)/30*0./,NSEQ(30)/8*0./, 400
C * M(8,80)/64*0./,MPRF(8,80)/64*0./,NM(8,80)/64*0./, 410
C * NMPRF(8,80)/64*0./,NC(8)/8*1/ 420
C 430
C LOGICAL PRINT/F/,PLOT/T/,PUNCH/F/,SCATTR/F/,ABSORB/T/,ERRORS/F/, 440
C * Q/F/,TOF/F/,LAMBDA/F/,RECOIL/F/,SMOOTH/F/,CAN/F/, 450
C * CRYOST/F/,EXPO/F/,SMQ/T/,ENABLE/F/,EQUALQ/T/,DEAD/F/, 460
C * SRUD/F/,SPLATE/F/,VRUD/F/,VPLATE/F/,VCOIL/F/, 470
C * MON/T/,TAPE7/F/,TAPE8/F/,TAPE9/T/,TRANS(8)/8*0./,TRANSM/F/, 480
C * JAY1*(512),JAY2*(512),JAY3*(65536), 490
C * TEXT*(1192),TXT*(180),DATE1*(12),DATE2*(12)/12*0 500
C 510
C EQUIVALENCE (A*(1,1),WK(1),QK(1),IARR(1),JAY3(1)), 520
C * (ICUN(1),JAY1(1)),(ICUN(129),JAY2(1)), 530
C * (TEXT(1),JAY1(321)),(DATE1(1),JAY1(13)), 540
C * (NCH,ICNL2),(CHAN,ICHNLW),(NBLKS,NBL), 550
C * (RSK(1),SI(1,1),IARR(1201)),(AS(1,1),IARR(2401)), 560
C * (ENU(1,1),IARR(3601)),(NU(1,1),IARR(4801)), 570
C * (K(1),IARR(6001)) 580
C 590
C DATA NRMAX,NRCON,NDFAD,JCY,JJJ,IDUM,ID,W,TFP,SFP/80,1,5*0,.1,2*0./, 600
C * ICUN1,Z,ADUM/2.0*9E0,1,1./, 610
C * PI,FP1,FP15/3.14159,12.566,39.478/, 620
C * EBAR,CBAR,RKEAR,ANU,AND,ANU/3*0.,3*1.E3/, 630
C * ITINO,ITAPE,NCTRS/1,9,0/, 640
C * STAN,DASH/'*','_'/ 650
C 660
C NAMLIST /LINAC/ NRCON,ID,TFP,SFP,ENABLE,ITAPE,CA,NC,EQUALQ, 670
C * NCTRS,CHAN,VOLUME,KPULSE,DEAD,NDEAD,MON,TRANS 680
C * /SIGMA/ SABS,CABS,VABS,SCUH 690
C * /SIZES/ RADIUS,WIDTH,HEIGHT,SRUD,SPLATE,VRUD,VCOIL,VPLATE 700
C * /DENSITY/SDENS,SMW,CDENS,CMW,VDENS,VMW 710
C * /PLZCK/ EBAR,CBAR,RKBAR,ANU,AND,ANU 720
C * /SCALE/ SQMAX,SQMIN,XMAX,XMIN 730
C * /CONTRL/PRINT,PLOT,PUNCH,SCATTR,ABSORB,Q,TOF,LAMBDA, 740
C * ERRORS,RECOIL,CRYOST,SMOOTH,CAN,W,EXPO,SMQ 750
C 760
C----- READ IN LINAC CONTROL PARAMETERS /LINAC/ ----- 770
C READ (5,LINAC) 780
C WRITE(13,LINAC) 790

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IF(ITAPE.EQ.7)TAPE7=.TRUE.
IF(ITAPE.EQ.9)TAPE9=.TRUE.
IF(ITAPE.NE.9)TAPE9=.FALSE.
C
C----- FILE FOR SUMMED COUNTERS AND EQ -----
DEFINE FILE 8(32,2,48,U,IV8),14(8,2,49,U,IV14)
C
C----- COMPUTE HEADER INFORMATION & GRAPH PLOTTER HEADER -----
CALL ZAI7AS(DAY,MONTH,YEAR)
CALL ZAI8AS(TIME)
CALL ZAI7AS(JOBNAM)
CALL ZVJ1AD(10,VOLUME,DSN)
CALL FILM (1)
CALL GHFROR(1)
CALL CSPACE(0.,1.414,0.,1.)
CALL PSPACE(.1,1.35,.1,.95)
CALL PLACE (20,20)
CALL TYPECS('LINAC LIQUIDS SPECTROMETER DATA',31)
CALL PLACE (27,25)
CALL TYPECS('PROGRAM RUN AT ',15)
CALL TYPECS(TIME,8)
CALL TYPECS(' ON ',4)
CALL TYPEPI(DAY)
CALL TYPECS(' ',1)
CALL TYPECS(MONTH,4)
CALL TYPECS(' ',1)
CALL TYPEPI(YEAR)
CALL CTRMAG(1)
C
WRITE(6,10)DAY,MONTH,YEAR,TIME,JOBNAM,VOLUME,DSN
1. FORMAT(/,T1,'TOTAL SCATTERING LIQUIDS SPECTROMETER',
* 'ALL SINGING,ALL DANCING DATA ANALYSIS PROGRAM',
* ' RUN ON ',13,1X,A4,I5,' AT ',A8,/,
* T1,'JOBNAME IS ',A8,/,
* T1,'MAGTAPE VOLUME IS ',A8,/,
* T1,'DATA SET NAME IS ',5A8,/,
* T1,'PROGRAM MK XLIV 5TH JANUARY 1976 (J.H.CLARKE)')
C
C----- CHECK COUNTER OPTIONS -----
IF(NC(1).EQ.0.AND.NC(2).EQ.0.AND.
* NC(3).EQ.0.AND.NC(4).EQ.0.AND.
* NC(5).EQ.0.AND.NC(6).EQ.0.AND.
* NC(7).EQ.0.AND.NC(8).EQ.0) GOTO163
2. IF(TAPE9)REWIND1
C
C----- READ LIST OF RUNS REQUIRED FOR PROCESSING -----
READ(5,*)NTRN
DO 30 I=1,NRMAX
IF(NTRN(I).EQ.0)GOTO4
30 CONTINUE
C
C----- SET MAXIMUM NO. OF RUNS FOR SPOOLING (ITMAX) -----
40 ITMAX=1-1
WRITE(6,5)ITAPE,ITMAX
WRITE(12,6)(NTRN(I),I=1,ITMAX)
IF(MON)WRITE(6,7)
IF(.NOT.MON)WRITE(6,8)
50 FORMAT(/,T10,'NUMBER OF RUNS SPOOLED FROM',I2,'-TRACK TAPE ',
* 'TO SCRATCH DISK IS',I5,/,
* T1,'SER CHANNEL 12 FOR TAPE READING LOG')
60 FORMAT(/,T10,'TAPE SPOOLING LOG OUTPUT CHANNEL 12',/,
* T1,'RUN NUMBERS (IN ORDER OF ASKING)',/,
* '(T10,1,110,/)')
70 FORMAT(/,T10,'MONITORS WILL BE READ FROM MAGTAPE CONTROL RECORD')
80 FORMAT(/,T10,'MONITORS WILL BE READ FROM INPUT CARDS',/)
C
C----- READ FIRST CONTROL RECORD -----
C----- READ PDP4 7-TRACK MAGNETIC TAPE -----
90 IF(TAPE7)CALL KPDP47(1,1,ICUN,0,0,0)
C----- READ PDP11 9-TRACK TAPE -----
IF(TAPE9)READ(11,END=29)ICUN
NBLKS=ICUN(1)
IF(TAPE9)ICUN(2)=NBLKS*128
C
C----- CHECK END OF TAPE -----
IF(ICUN(3).EQ.9999.OR.JJJ.GT.ITMAX)GOTO300
C----- COMPUTE DATE -----
IF(TAPE9)CALL ZAI5AS(DATE1,DATE2,I2,LDON,1,IERR)
WRITE(12,100)ICUN(3),ICUN(2),DATE2
100 FORMAT(1X,'RUN NO.',I1,' OF ',I6,' CHANNELS ON ',I2A1)

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C		1600
C	----- HUNT FOR RUN IN RUN LIST -----	1610
	DO 110 K2=1,ITMAX	1620
	IF(ICON(3).EQ.NTRN(K2))GO TO 120	1630
	110 CONTINUE	1640
C		1650
C	----- MOVE ON TO NEXT RECORD -----	1660
	IF(TAPE7)CALL RPDP47(2,1,0,0,0,0)	1670
	IF(TAPE9)READ(10,END=290)	1680
	GOTO90	1690
C		1700
C	----- RUN FOUND -----	1710
	120 WRITE(12,140)ICON(3)	1720
C	----- COMPUTE TEXT STRING FROM CONTROL RECORD -----	1730
	IF(TAPE9)CALL ZAOSAS(TEXT,TXT,80,LDONE,1,IERR)	1740
	IF(TAPE9)WRITE(11,130)ICON(3),DATE2,TXT	1750
	130 FORMAT(2X,'RUN NO. ',110,2X,12A1,2X,80A1)	1760
	140 FORMAT(1H+,T51,'*',110,' FOUND')	1770
C	----- IF 7 TRACK TAPE SKIP THIS SECTION -----	1780
	IF(.NOT.TAPE9)GOTO170	1790
	DO 160 K=1,8	1800
C	----- READ OFF ANY REMAINING RUN PARAMETERS FROM FIRST RUN ON TAPE -----	1810
	IF(JJJ.GT.1)GOTO150	1820
C		1830
C	----- COUNTER ANGLES FIRST -----	1840
	IF(CA(K).EQ.0.)CA(K)=FLOAT(ICON(9+8*K))*0.1	1850
C		1860
C	----- NOW THE MONITORS AND PRF PULSES IF MON HAS NOT BEEN SET TO FALSE -	1870
	150 IF(MON)NM(K,K2) =ICON(15+8*K)	1880
	IF(MON)NMPRF(K,K2)=ICON(11+8*K)	1890
	160 CONTINUE	1900
	IF(JJJ.GT.0)GOTO230	1910
C		1920
C	----- CHANNEL WIDTH, INITIAL DELAY, DEADTIME, NCTKS & FLIGHT PATHS -----	1930
	IF(CHAN.EQ.0) CHAN =ICON(10)/10	1940
	IF(ID.EQ.0) ID =ICON(11)/10	1950
	IF(NDEAD.EQ.0)NDEAD=ICON(14)/ICON(10)	1960
	IF(NCTRS.EQ.0)NCTRS=ICON(9)	1970
	IF(TFP.EQ.0.) TFP =FLOAT(ICON(12))*0.1	1980
	IF(SFP.EQ.0.) SFP =FLOAT(ICON(13))*0.1	1990
C		2000
C	----- IF THIS IS THE FIRST RUN READ OFF THEN PRINT OUT THE CONTROL DATA-	2010
C	----- OTHERWISE GOTO 230 AND READ IN RUN -----	2020
	170 IF(JJJ.GT.0)GOTO230	2030
	F=SFP/TFP	2040
	HCHAN=.5*FLOAT(CHAN)	2050
	RD=ID	2060
	RI=RD-HCHAN	2070
	WRITE(6,190)NRUN,ID,TFP,SFP,NDEAD	2080
	DO 180 K=1,NCTRS	2090
	IF(TRANS(K))WRITE(6,210)K,NC(K),CA(K)	2100
	IF(.NOT.TRANS(K))WRITE(6,200)K,NC(K),CA(K)	2110
	180 CONTINUE	2120
	190 FORMAT(/,110,'THERE ARE',I3,' SETS OF DATA TO BE ANALYSED',//,	2130
	* T10,'THE INITIAL TIMING DELAY IS',I4,' MICROSECONDS',//,	2140
	* T10,'THE FLIGHT PATH LENGTH IS',F6.3,' METRES',//,	2150
	* T10,'THE SECOND FLIGHT PATH IS',F6.3,' METRES',//,	2160
	* T10,'THERE ARE ',I2,' DEAD CHANNELS',//)	2170
	200 FORMAT(/,T10,'COUNTER POSITION NUMBER',I2,' HAS',I3,	2180
	* ' COUNTERS AT',F6.3,' DEGREES IN REFLECTION')	2190
	210 FORMAT(/,T10,'COUNTER POSITION NUMBER',I2,' HAS',I3,	2200
	* ' COUNTERS AT',F6.3,' DEGREES IN TRANSMISSION')	2210
C		2220
C	----- CONVERT TO RADIANS , HALF COUNTER ANGLE -----	2230
	DO 220 K=1,NCTRS	2240
	220 CA(K)=CA(K)*.00872664	2250
	230 JJJ=JJJ+1	2260
C		2270
C	----- READ RUN INTO CORE -----	2280
	DO 240 K=1,16304	2290
	240 IARR(K)=0	2300
C	----- 7-TRACK POP-4 TAPE -----	2310
	IF(TAPE7)CALL RPDP47(2,1,IARR,ICON(2),2,NER)	2320
	IF(.NOT.TAPE9)GOTO260	2330
C	----- 9-TRACK POP-11 TAPE -----	2340
	NCHNL=ICON(1)*128	2350
	READ(10,END=290)(IARR(K1),K1=1,NCHNL)	2360
C		2370
C	----- FUDGE FUNNY CHARACTERS -----	2380
	IARR(ICON(2))=IARR(ICON(2)-1)	2390

C		2400
C	---- CORRECT FOR ODD HIGH ORDER PART OF WORD CREATED WITH OLD DATIN	2410
	DO 250 J=1,NBLKS	2420
	JSHIFT=(J-1)*512	2430
	JAY3(1+JSHIFT)=JAY3(5+JSHIFT)	2440
250	JAY3(2+JSHIFT)=JAY3(6+JSHIFT)	2450
260	WRITE(12,27.)	2460
270	FORMAT(1H+,T63,*,READ FROM TAPE*)	2470
C		2480
C	---- WRITE RUN ONTO DISC 1 -----	2490
	WRITE(1)ICON,IASK	2500
	WRITE(12,28)(K2,ICON(3))	2510
280	FORMAT(1H+,T63,*,WRITTEN TO DISC AS FILE*,I3,*,RUN*,I10)	2520
C		2530
C	---- INCREASE RUN NUMBER BY 1 -----	2540
	JCY=JCY+1	2550
C	---- SEQUENCE NUMBER OF RUN NTRN(K2) ON SCRATCH DISC	2560
	NSEQ(K2)=JCY	2570
C		2580
C	---- SET UP ARRAY DIMENSIONS FOR DUMMY ARGUMENTS OF SUBPROGRAMS -----	2590
	IF(JCY.EQ.1.AND..NOT.TAPE9)ICNL2=ICON(2)	2600
	IF(JCY.EQ.1.AND..NOT.TAPE9)ICHNL=ICON(2)/NCTRS	2610
	IF(JCY.EQ.1.AND.TAPE9)ICNL2=ICON(1)*128	2620
	IF(JCY.EQ.1.AND.TAPE9)ICHNL=ICNL2/NCTRS	2630
	ICHNLW=CHAN	2640
C		2650
C	---- CHECK ARRAY OVERFLOW OR END OF RUN LIST -----	2660
	IF(JCY.GT.NRMAX.OR.JCY.GE.1TMAX)GOTO310	2670
C	---- READ IN NEXT RUN -----	2680
	GO TO 9.	2690
C		2700
C	---- END OF TAPE OR DATA SET -----	2710
291	WRITE(6,34.)	2720
300	WRITE(12,320)	2730
311	WRITE(6,330)	2740
320	FORMAT(T10,'9999 FOUND')	2750
330	FORMAT(T45,'*****')	2760
340	FORMAT(T10,'EOF MARK FOUND ON MAGNETIC TAPE')	2770
	ENDFILE 1	2780
C		2790
C	---- CYCLE OVER SETS OF INPUT DATA -----	2800
	IF(NRUN.EQ..)STOP	2810
	DO 1620 KRUN=1,NRUN	2820
	READ(5,300)ITITLE	2830
	WRITE(6,360)(STAR,I=1,83),TITLE,(STAR,I=1,83)	2840
	WRITE(6,370)(DASH,I=1,49)	2850
350	FORMAT(10A4)	2860
360	FORMAT(1H1,T3,8(A1,/,T30,A1,T109,A1,/,T30,A1,T34,10A4,T109,A1,/,	2870
	T3,,A1,T109,A1,/,T30,8(A1,/,/,T5,*,IDENTIFIER*,T20,*,RUN-NO.*,T33,	2880
	MON1,T43,*,MON2*,T53,*,MON3*,T63,*,MON4*,T73,*,MON5*,T83,*,MON6*,T93,	2890
	MON7,T1.3,*,MON8*)	2900
370	FORMAT(1H+,T5,1(A1,T2,7A1,T33,8(4A1,6X))	2910
C		2920
C	---- INITIALIZE VARIABLES -----	2930
	DO 400 K1=1,NRMAX	2940
	RUN(K1)=0	2950
	TYPE(K1)=0	2960
	DO 390 K2=1,3	2970
	M(K2,K1)=0	2980
	MPRF(K2,K1)=0	2990
	DO 380 K3=1,4	3000
38	SUM(K3,K2,K1)=0.	3010
390	CONTINUE	3020
400	CONTINUE	3030
	DO 420 K=1,4	3040
	CSUM(K)=0.	3050
	DO 410 L=1,8	3060
	RAC(L,K)=0.	3070
	RPULSE(L,K)=0.	3080
410	CONTINUE	3090
420	CONTINUE	3100
C		3110
C	---- INPUT RUN NO. MONITOR COUNT -----	3120
	DO 490 K=1,NRMAX	3130
	CALL DNRZA(FORM)	3140
	IF(.NOT.MON)READ(5,FORM)RUN(K),TYPE(K),(M(L,K),L=1,NCTRS)	3150
	IF(.NOT.MON)GOTO460	3160
	IF(MON)READ(5,FORM)RUN(K),TYPE(K)	3170
C		3180
C	---- FIND POSITION OF RUN(K) IN ARCHIVE LIST NTRN -----	3190

C-----	DON'T FORGET THAT LAST RUN IN LIST RUN(ITMAX) IS NEGATIVE -----	3200
	DO 450 K1=1,ITMAX	3210
	IF(IABS(RUN(K)).NE.NTRN(K1))GOTO440	3220
C		3230
C-----	SET MONITOR OF RUN(K) TO VALUE NM IN ARCHIVE LIST -----	3240
	DO 430 L=1,NCTRS	3250
	M(L,K)=NM(L,K1)	3260
	MPRF(L,K)=NMPRF(L,K1)	3270
	430 CONTINUE	3280
	440 IF(IABS(RUN(K)).EQ.NTRN(K1))GOTO460	3290
	450 CONTINUE	3300
C-----	LIST RUN NUMBERS AND MONITORS -----	3310
	460 WRITE(6,470)RTP(TYPE(K)),RUN(K),(M(L,K),L=1,NCTRS)	3320
	IF(TYPE(K).LT.0.OR.TYPE(K).GT.4)WRITE(6,480)RUN(K)	3330
	IF(TYPE(K).LT.0.OR.TYPE(K).GT.4)GOTO1620	3340
	470 FORMAT(T5,A8,T16,I10,T27,8I10)	3350
	480 FORMAT(T10,"RUN NUMBER",I10," HAS AN INVALID RUN TYPE INDICATOR")	3360
	IF(RUN(K).LT.0)JMAX=K	3370
C-----	CHECK FOR LAST RUN IN LIST AND RESET TO POSITIVE VALUE -----	3380
	IF(RUN(K).LT.0)GOTO500	3390
	490 CONTINUE	3400
	500 RUN(JMAX)=-RUN(JMAX)	3410
C		3420
C-----	INITIALIZE T -----	3430
	DO 510 K2=1,2048	3440
	510 T(K2)=0.	3450
C		3460
C-----	READ IN SCATTERING CROSS SECTION ARRAYS 1<IMAX<40 -----	3470
	CALL READ1(SIGMA1,E1,IMAX1)	3480
	CALL READ1(SIGMA2,E2,IMAX2)	3490
	CALL READ1(SIGMA3,E3,IMAX3)	3500
C		3510
C-----	READ ABSORPTION CROSS SECTIONS AND COHERENT CROSS SECTION /SIGMA/	3520
	READ(5,SIGMA)	3530
	WRITE(13,SIGMA)	3540
	WRITE(6,520)SABS,CABS,VABS,SCOH	3550
	520 FORMAT(/,T10,"ABSORPTION CROSS SECTION OF SAMPLE IS ",T65,F8.3,	3560
	*" BARNs",/,T10,"ABSORPTION CROSS SECTION OF CAN IS ",T65,F8.3,	3570
	*" BARNs",/,T10,"ABSORPTION CROSS SECTION OF VANADIUM IS",T65,F8.3,	3580
	*" BARNs",/,T10,"COHERENT SCATTERING CROSS SECTION OF MOLECULE IS"	3590
	* ,T65,F8.3," BARNs",/)	3600
C		3610
C-----	INPUT CONTROL CARD -----	3620
	READ (5,CONTRL)	3630
	WRITE(13,CONTRL)	3640
	IF(.NOT.PLOT)CALL GHPEN(0)	3650
	WRITE(6,530)	3660
	IF(PRINT) WRITE(6,540)	3670
	IF(PLOT) WRITE(6,550)	3680
	IF(.NOT.PLOT) WRITE(6,560)	3690
	IF(PUNCH) WRITE(6,570)	3700
	IF(SCATTR) WRITE(6,580)	3710
	IF(ABSORB) WRITE(6,590)	3720
	IF(CRYDST) WRITE(6,600)	3730
	IF(RECOIL) WRITE(6,610)	3740
	IF(ERRORS) WRITE(6,620)	3750
	IF(SMOOTH) WRITE(6,630)	3760
	IF(CAN) WRITE(6,640)	3770
	IF(EXPD) WRITE(6,670)	3780
	IF(SMOOTH.OR.CAN)WRITE(6,650)W	3790
	IF(W.LE.2.OR.W.GE.1.)W=.1	3800
	IF(W.LE.2.OR.W.GE.1.)WRITE(6,660)	3810
C		3820
	530 FORMAT(T10,"PROGRAM WILL COMPUTE D(SIGMA)/D(OMEGA) AND S(Q) WITH P	3830
	*LAZCEK CORRECTIONS")	3840
	540 FORMAT(T10,"RAW COUNTS WILL BE LISTED")	3850
	550 FORMAT(T10,"RATIOS ETC. WILL BE PLOTTED")	3860
	560 FORMAT(T10,"GRAPHS WILL NOT BE PLOTTED")	3870
	570 FORMAT(T10,"RATIOS WILL BE PUNCHED TO CARDS")	3880
	580 FORMAT(T10,"SCATTERING CROSS SECTION USED IN ABSORPTION STEP")	3890
	590 FORMAT(T10,"ABSORPTION CORRECTIONS WILL BE APPLIED")	3900
	600 FORMAT(T10,"AIR BACKGROUND NOT SUBTRACTED FROM SAMPLE AND CAN")	3910
	610 FORMAT(T10,"RECOIL CORRECTIONS APPLIED")	3920
	620 FORMAT(T10,"STANDARD ERRORS WILL BE COMPUTED")	3930
	630 FORMAT(T10,"SMOOTHING WILL BE PERFORMED ON VANADIUM & BACKGROUND")	3940
	640 FORMAT(T10,"SMOOTHING WILL BE PERFORMED ON CAN")	3950
	650 FORMAT(T10,"SMOOTHING WIDTH W IS ",F6.3)	3960
	660 FORMAT(T10,"W RESET TO .05")	3970
	670 FORMAT(T10,"EXPONENTIAL SCATTERING FORMALISM USED")	3980
C		3990

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C-----READ MAXIMUM AND MINIMUM SCALE VALUES FOR GRAPH PLOTTING /SCALE/
READ(5,SCALE)
WRITE(13,SCALE)
DO 680 I=1,NCTRS
IF(SQMAX(I).NE.0.)WRITE(6,69)SQMAX(I),SQMIN(I),I
IF(XMAX(I).NE.0.)WRITE(6,70)XMAX(I),XMIN(I),I
680 CONTINUE
WRITE(6,71)CHAN
690 FORMAT(T10,'YMAX = ',F8.3,' YMIN = ',F8.3,' FOR COUNTER',I2)
70 FORMAT(T10,'XMAX = ',F8.3,' XMIN = ',F8.3,' FOR COUNTER',I2)
710 FORMAT(T10,'CHANNEL WIDTH IS ',I6,' MICROSECONDS')
4000
4010
4020
4030
4040
4050
4060
4070
4080
4090
4100
4110
C-----READ SAMPLE AND VANADIUM GEOMETRIES /SIZES/ -----
READ(5,SIZES)
WRITE(13,SIZES)
IF(.NOT.SPLATE)R3=2.5*RADIUS(3)
IF(.NOT.VPLATE)R4=2.5*RADIUS(4)
IF(((RADIUS(4).GT.R4.OR.RADIUS(5).GT.R4).AND.(VROD.OR.VCOIL)).OR.
* ((RADIUS(1).GT.R3.OR.RADIUS(2).GT.R3).AND.SROD))GOTO830
IF(SPLATE.AND.(RADIUS(2).LT.RADIUS(1)))GOTO870
IF(SROD) WRITE(6,720)(RADIUS(K),K=1,3)
IF(SPLATE)WRITE(6,730)(RADIUS(K),K=1,3)
IF(VROD) WRITE(6,740)RADIUS(4),RADIUS(6)
IF(VCOIL) WRITE(6,750)(RADIUS(K),K=4,6)
IF(VPLATE)WRITE(6,760)RADIUS(4),RADIUS(6)
WRITE(6,770)HEIGHT,WIDTH
IF(RADIUS(3).EQ.90.OR.RADIUS(6).EQ.90)GOTO850
4120
4130
4140
4150
4160
4170
4180
4190
4200
4210
4220
4230
4240
4250
4260
4270
C----- COMPUTE PLATE ANGLES IN RADIANS -----
IF(SPLATE)RADIUS(3)=RADIUS(3)*PI/180.
IF(VPLATE)RADIUS(6)=RADIUS(6)*PI/180.
4280
4290
4300
4310
C
72. FORMAT(T10,'RADIUS OF SAMPLE IS ',T50,F7.4,' CM.',/,
* T10,'RADIUS OF CAN (OUTER) IS',T50,F7.4,' CM.',/,
* T10,'INCREMENT IN ABSORPTION INTEGRAL IS',T50,F7.4,
* T10,'CYLINDRICAL SAMPLE GEOMETRY')
4320
4330
4340
4350
730 FORMAT(T10,'THICKNESS OF SAMPLE PLATE IS',T50,F7.4,' CM.',/,
* T10,'THICKNESS OF SAMPLE +CAN IS ',T50,F7.4,' CM.',/,
* T10,'ANGLE OF SAMPLE NORMAL TO BEAM IS',T50,F7.4,' DEGS.',/
* T10,'FLAT PLATE SAMPLE GEOMETRY')
4360
4370
4380
4390
74. FORMAT(T10,'RADIUS OF VANADIUM ROD IS ',T50,F7.4,' CM.',
* /,T10,'INCREMENT IN ABSORPTION INTEGRAL IS',T50,F7.4,' CM.',
* /,T10,'VANADIUM STANDARD HAS CYLINDRICAL GEOMETRY')
4400
4410
4420
750 FORMAT(T10,'RADIUS OF VANADIUM COIL (INNER) IS',T50,F7.4,' CM.',/,
* T10,'RADIUS OF VANADIUM COIL (OUTER) IS',T50,F7.4,' CM.',/,
* T10,'INCREMENT IN ABSORPTION INTEGRAL IS',T50,F7.4,' CM.',
* /,T10,'VANADIUM STANDARD IS IN FORM OF COIL')
4430
4440
4450
4460
760 FORMAT(T10,'THICKNESS OF VANADIUM PLATE IS',T50,F6.3,' CM.',/,
* T10,'ANGLE OF VANADIUM NORMAL TO BEAM IS',T50,F6.3,' DEGS.',
* /,T10,'VANADIUM STANDARD IS IN FORM OF A FLAT PLATE')
4470
4480
4490
77. FORMAT(T10,'HEIGHT OF BEAM IS',F6.3,' CM.',/,
* T10,'WIDTH OF BEAM IS',F6.3,' CM.')
4500
4510
4520
C----- INPUT NUMBER DENSITIES OF SAMPLE,CAN AND VANADIUM -----
READ(5,DENSTY)
WRITE(13,DENSTY)
RHOS=.6123*SDENS/SMW
RHOC=.6123*CDENS/CMW
RHODV=.6123*VDENS/VMW
WRITE(6,780)SDENS,SMW,RHOS,CDENS,CMW,RHOC,VDENS,VMW,RHODV
4530
4540
4550
4560
4570
4580
4590
780 FORMAT(T10,'SAMPLE DENSITY IS ',T30,F8.3,' GM./C.C.',
* 'MOLECULAR WEIGHT IS',T68,F9.3,
* T80,'NUMBER DENSITY IS ',T98,F8.5,/,
* T10,'CAN DENSITY IS ',T30,F8.3,' GM./C.C.',
* 'MOLECULAR WEIGHT IS',T68,F9.3,
* T80,'NUMBER DENSITY IS ',T98,F8.5,/,
* T10,'VANADIUM DENSITY IS',T30,F8.3,' GM./C.C.',
* 'MOLECULAR WEIGHT IS',T68,F9.3,
* T80,'NUMBER DENSITY IS ',T98,F8.5,/)
4600
4610
4620
4630
4640
4650
4660
4670
4680
4690
C----- READ PARAMETERS FOR PLACZEK CORRECTIONS -----
READ(5,PLZCK)
WRITE(13,PLZCK)
IF(AND.NE.1.0E+3)ANU=AND
IF(ANG.NE.1.0E+3)ANU=ANG
WRITE(6,790)EBAR,CBAR,RKBAR,ANU
790 FORMAT(T10,'MEAN KINETIC ENERGY OF MOLECULE IS',F10.5,' MILLI EV ',
* /,T10,'MEAN VALUE OF CBAR IS',F10.5,' ',/,
* T10,'MEAN VALUE OF KBAR IS',F10.5,' EV ',/,
* T10,'EFFECTIVE MOLECULAR MASS IS',E12.3,' A.M.U.')
4700
4710
4720
4730
4740
4750
4760
4770
4780
4790

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C		4800
C	----- PRINT SCATTERING CROSS SECTION/ENERGY MESHES -----	4810
	WRITE(6,800)	4820
	CALL OJUHNA(E1,SIGMA1,IMAX1,1,6,6,'EF',' SIGMA S',6)	4830
	WRITE(6,810)	4840
	CALL OJUHNA(E2,SIGMA2,IMAX2,1,6,6,'EF',' SIGMA C',6)	4850
	WRITE(6,820)	4860
	CALL OJUHNA(E3,SIGMA3,IMAX3,10,6,6,'EF',' SIGMA V',6)	4870
800	FORMAT(//,T10,'SAMPLE SCATTERING CROSS SECTION/ENERGY MESH')	4880
810	FORMAT(//,T10,'CAN SCATTERING CROSS SECTION/ENERGY MESH')	4890
820	FORMAT(//,T10,'VANADIUM SCATTERING CROSS SECTION/ENERGY MESH')	4900
	GOTO890	4910
C		4920
C	----- CYLINDRICAL SAMPLE ERROR -----	4930
830	WRITE(6,840)	4940
840	FORMAT(' **', ' RADII OF SAMPLES/DELTA R IS GREATER THAN 20')	4950
	WRITE(6,SIZES)	4960
	GOTO162L	4970
C		4980
C	----- PLATE SAMPLE ERROR -----	4990
850	WRITE(6,860)RADIUS(3),RADIUS(6)	5000
860	FORMAT(T10,'**** SAMPLE IS PARALLEL TO BEAM, THETA(SAMPLE)=' ,F6.3,	5010
	* ' THETA(VANADIUM)=' ,F6.3)	5020
	WRITE(6,SIZES)	5030
	GOTO162L	5040
870	WRITE(6,880)RADIUS(2),RADIUS(1)	5050
880	FORMAT(T10,'**** (SAMPLE+CAN) WIDTH IS GREATER THAN SAMPLE WIDTH')	5060
	WRITE(6,SIZES)	5070
	GOTO162L	5080
C		5090
C	----- COMPUTE SECANTS OF PLATE ANGLES COSS AND COSV -----	5100
890	IF(SPLATE)COSS=1./COS(RADIUS(3))	5110
	IF(VPLATE)COSV=1./COS(RADIUS(6))	5120
C		5130
C	----- CHECK FOR FORM OF DATA OUTPUT -----	5140
	IF(Q) WRITE(6,900)	5150
	IF(TOF) WRITE(6,910)	5160
	IF(LAMBDA)WRITE(6,920)	5170
900	FORMAT(/,T10,'DATA IS PRESENTED IN FORM OF Q-VALUES',/)	5180
910	FORMAT(/,T10,'DATA IS PRESENTED IN TIME OF FLIGHT VALUES',/)	5190
920	FORMAT(/,T10,'DATA IS PRESENTED IN WAVELENGTH VALUES',/)	5200
C		5210
C	----- SET UP ODD VARIABLES -----	5220
	R1=RADIUS(1)	5230
	R2=RADIUS(2)	5240
	R3=RADIUS(3)	5250
	R4=RADIUS(4)	5260
	R5=RADIUS(5)	5270
	R6=RADIUS(6)	5280
	IF(VROD) DUMK=R4+R6	5290
	IF(VPLATE) DUMK=R4*1.1	5300
	IF(.NOT.ABSORB)GOTO930	5310
C	----- BZCON=TIME IN MICRO SECONDS FOR ABSORPTION X-SECTION -----	5320
	BZCON=.0022/TFP	5330
	BZS1=SABS*BZCON	5340
	BZC1=CABS*BZCON	5350
	BZV1=VABS*BZCON	5360
C		5370
C	----- LOOP OVER ALL COUNTERS WRITING THEM TO DISC 8 -----	5380
930	DO 1010 INC=1,NCTRS	5390
	IF(NC(INC).EQ.0)GOTO1010	5400
	DO 940 K=1,2048	5410
	A(K)=0.	5420
	B(K)=0.	5430
	C(K)=0.	5440
940	D(K)=0.	5450
C		5460
C	----- READ OFF RUNS FROM SCRATCH DISC AND SUM TOGETHER -----	5470
C	----- ACCORDING TO TYPE K=1,2,3 OR 4 -----	5480
	J=1	5490
950	K=TYPE(J)	5500
	NR=RUN(J)	5510
	GOTO(960,970,980,990),K	5520
C		5530
C	----- READ OFF SAMPLE AND CAN RUN,RETURNS WITH RUN ADDED IN TO ARRAY A -	5540
C	----- ,MONITORS FROM M INTO RMC AND PRF PULSES FROM MPRF INTO RPULSE ---	5550
960	CALL DISC(A,IARR,NR,ICHLN,INC,ICON,SUM,K,J,RMC,&950,&1000,NTRN,M,	5560
	* MPRF,RPULSE,JMAX,NSEQ)	5570
970	CALL DISC(B,IARR,NR,ICHLN,INC,ICON,SUM,K,J,RMC,&950,&1000,NTRN,M,	5580
	* MPRF,RPULSE,JMAX,NSEQ)	5590

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980 CALL DISCIC,IARR,NR,ICHNL,INC,ICON,SUM,K,J,RMC,&950,&1000,NTRN,M, 5600
* MPRF,RPULSE,JMAX,NSEQ) 5610
990 CALL DISCID,IARR,NR,ICHNL,INC,ICON,SUM,K,J,RMC,&950,&1000,NTRN,M, 5620
* MPRF,RPULSE,JMAX,NSEQ) 5630
C 5640
C----- PUT A,B,C,D TO DISC 8 ----- 5650
1100 WRITE(8*4*INC-3)A 5660
WRITE(8*4*INC-2)B 5670
WRITE(8*4*INC-1)C 5680
WRITE(8*4*INC)D 5690
1110 CONTINUE 5700
ENDFILE 8 5710
C 5720
DO 1600 INC=1,NCTRS 5730
TBEG=ZAC2AS(DUMMY) 5740
IF(NC(INC).EQ.0)GOTO1600 5750
FINU(8*4*INC-3) 5760
IF(Q) GOTO1660 5770
IF(TOF) GOTO1620 5780
IF(LAMBDA)GOTO1640 5790
C 5800
C----- PRODUCE TIME CHANNELS ----- 5810
1020 DO 1030 I=1,ICHNL 5820
1030 T(I)=R1+FLOAT(ICHNLW*I) 5830
GOTO1100 5840
C 5850
C----- PRODUCE WAVELENGTH VALUES ----- 5860
1040 CON2=TFP*252.7 5870
DO 1050 I=1,ICHNL 5880
1050 T(I)=(R1+FLOAT(ICHNLW*I))/CON2 5890
GOTO1100 5900
C----- PRODUCE Q VALUES ----- 5910
C 5920
1060 IF(.NOT.RECOIL)GOTO1070 5930
C----- RECOIL CORRECTION ----- 5940
X=1.-COS(CA(INC)*2.+ARSIN(SIN(CA(INC)*2.)/ANU)) 5950
X=SQRT(1.-2.*ANU*X/(ANU+1.))**2) 5960
C----- APPLY CENTRE OF MASS TRANSFORMATION ----- 5970
C3=1587.761*TFP*((1.-F)*X+F)*SQRT(X*X+1.-2.*X*COS(CA(INC)*2.))/X 5980
DCA=CA(INC)*114.591D 5990
1070 IF(.NOT.RECOIL)C3=3175.5218*SIN(CA(INC))*TFP 6000
C----- Q-SCALE ----- 6010
DO 1090 K=1,ICHNL 6020
IF(K.EQ.1.AND.RECOIL)WRITE(6,1080)X,DCA 6030
1080 FORMAT(T1,'RATIO OF V2 TO V1 IS',F6.3,' AT',F6.3,' DEGREES') 6040
1090 T(K)=C3/(R1+FLOAT(CHAN*K)) 6050
C 6060
C----- SET UP AN ARRAY OF 54 PAALMAN AND PINGS TERMS ----- 6070
C----- CHECK TO SEE IF WE HAVE DOWNSTREAM MONITOR ----- 6080
1100 IF(CA(INC).EQ.0.)TRANSM=.TRUE. 6090
IF(CA(INC).NE.0.)TRANSM=.FALSE. 6100
IF(TRANSM)GOTO1150 6110
IF(.NOT.ABSORB)GOTO1130 6120
TCON=K1 6130
DO 1110 I=1,20 6140
K(I)=0. 6150
DO 1110 J=1,64 6160
AB(J,I)=0. 6170
SI(J,I)=0. 6180
AS(J,I)=0. 6190
NU(J,I)=0. 6200
ENU(J,I)=0. 6210
1110 CONTINUE 6220
C 6230
C----- # OF CHANNELS PER ARRAY ELEMENT (NCPK) ----- 6240
NCPK=10*ICHNL/512 6250
CHAN2=FLOAT(CHAN*NCPK) 6260
IF(IMAX1.EQ.1)B1S=SIGMA1(1) 6270
IF(IMAX2.EQ.1)B1C=SIGMA2(1) 6280
IF(IMAX3.EQ.1)B1V=SIGMA3(1) 6290
DO 1120 K=1,54 6300
TCON=TCON+CHAN2 6310
C 6320
C----- ABSORPTION X-SECTIONS FOR ARRAY ELEMENT (B2S,B2C & B2V) ----- 6330
B2S =TCON*B2S1 6340
B2C =TCON*B2C1 6350
B2V =TCON*B2V1 6360
C 6370
C----- CHECK FOR SCATTERING CROSS SECTION SHORT CUT ----- 6380
IF(IMAX1.GT.1)B1S=BARN1(K,SIGMA1,E1,K1,TFP,CHAN,1) 6390

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IF(IMAX2.GT.1)B1C=BARN1(K,SIGMA2,E2,RI,TFP,CHAN,2)
IF(IMAX3.GT.1)B1V=BARN1(K,SIGMA3,E3,RI,TFP,CHAN,3)
C
C----- SAMPLE ABSORPTION CORRECTION TERMS -----
CALL ABSORP(B1S,B2S,B1C,B2C,RHOS,RHOC,R1,R2,R3,ASS1(K),ACCI(K),
* ACS1(K),CA(INC),1,AB,SI,AS,ENU,NU,R,ABSORB,SCATTR,
* SPLATE,VPLATE,TRANS(INC))
C
C----- VANADIUM ROD CORRECTION TERMS -----
IF(VKOD)CALL ABSORP(B1V,B2V,Z,Z,RHOV,Z,R4,DUMK,R6,ASS2(K),ADUM,
* ACS2(K),CA(INC),2,AB,SI,AS,ENU,NU,R,ABSORB,
* SCATTR,SPLATE,VPLATE,TRANS(INC))
C
C----- VANADIUM COIL CORRECTION TERMS -----
IF(VCOIL)CALL ABSORP(Z,Z,B1V,B2V,Z,Z,RHOV,R4,R5,R6,ADUM,ASS2(K),
* ADUM,CA(INC),2,AB,SI,AS,ENU,NU,R,ABSORB,
* SCATTR,SPLATE,VPLATE,TRANS(INC))
C
C----- VANADIUM PLATE CORRECTION TERMS -----
IF(VPLATE)CALL ABSORP(B1V,B2V,Z,Z,RHOV,Z,R4,DUMR,R6,ASS2(K),ADUM,
* ADUM,CA(INC),2,AB,SI,AS,ENU,NU,R,ABSORB,
* SCATTR,SPLATE,VPLATE,TRANS(INC))
1120 CONTINUE
C
C----- WRITE ABSORPTION CORRECTION TERMS -----
1130 FIND(8*4*INC-3)
WRITE(6,1140)
WRITE(6,1150)(ASS1(K),ACCI(K),ACS1(K),ASS2(K),ACS2(K),
* ASS1(K+1),ACCI(K+1),ACS1(K+1),ASS2(K+1),ACS2(K+1),K=1,54,2)
1140 FORMAT(/,T10,'PAALMAN AND PINGS ABSORPTION CORRECTION TERMS ',
* 'ARE:',//,T11,'ASS1',T18,'ACCI',T25,'ACS1',T32,'ASS2',T39,
* 'ACS2',T46,'ASS1',T53,'ACCI',T60,'ACS1',T67,'ASS2',T74,'ACS2')
1150 FORMAT(T8,10F7.4)
C
C----- RECOVER A,B,C,D -----
1160 READ(8*4*INC-3)A
READ(8*4*INC-2)B
READ(8*4*INC-1)C
READ(8*4*INC)D
C
C----- LIST COUNTS, MONITORS AND COUNTS PER MONITOR -----
WRITE(6,1170)
1170 FORMAT(/,T10,'COUNTS, MONITORS, PULSES & COUNTS PER MONITOR',//)
C
C----- LOOP OVER RUN TYPE K=1,2,3,4 -----
DO 1180 K=1,4
CSUM(K)=0.
C
C----- LOOP OVER RUN SEQUENCE ON DISC J=1,2,...JMAX -----
DO 1180 J=1,JMAX
SK=SUM(K,INC,J)
MPRFK=MPRF(INC,J)
MK=M(INC,J)
IF(SK.GT.0.1.AND.MK.GT.0)CPM=SK/FLOAT(MK)
IF(SK.GT.0.1)WRITE(6,1210)SK,MK,MPRFK,CPM,RTP(K),INC,RUN(J),J
1180 CSUM(K)=CSUM(K)+SK
C
C----- PRINT MONITORS AND SUMMED COUNTS FOR EACH COUNTER -----
WRITE(6,1220)INC,(RMC(INC,K),K=1,4),INC,CSUM,INC,
* (RPULSE(INC,L),L=1,4)
C
C----- PRINT COUNTS PER MONITOR -----
DO 1190 K=1,4
1190 CSUM(K)=CSUM(K)*.01/RMC(INC,K)
WRITE(6,1230)INC,CSUM
C
C----- PRINT COUNTS PER PULSE -----
DO 1200 K=1,4
IF(RPULSE(INC,K).EQ.0)CSUM(K)=0.
IF(RPULSE(INC,K).EQ.0)GOTO1200
CSUM(K)=CSUM(K)*RMC(INC,K)/RPULSE(INC,K)*100.
1200 CONTINUE
WRITE(6,1240)INC,CSUM
C
1210 FORMAT(T10,'SUM=',F12.0,' MONITOR=',I10,' PRF=',I10,
* 'SUM/MON=',F12.5,' TYPE=',A8,' COUNTER=',I2,
* 'RUN=',I10,' NO.',I2)
1220 FORMAT(/,T10,'MONITOR COUNTS FOR CTR:',I2,
* 'S+C',F10.0,' U',F10.0,' V+B',F10.0,' B',F10.0,/,
* T10,'SUMMED COUNTS FOR CTR:',I2,

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*          * S+C°,F10.3°, C°,F10.0°, V+B°,F10.0°, B°,F10.0,/,      7200
*          T10,°PKF PULSES   FOR CTR:°,I2,                          7210
*          * S+C°,F10.3°, C°,F10.3°, V+B°,F10.3°, B°,F10.3,/)      7220
1230 FORMAT(T10,°COUNTS/MONITOR FOR CTR:°,I2,                      7230
*          * S+C°,F10.3°, C°,F10.3°, V+B°,F10.3°, B°,F10.3,/)      7240
1240 FORMAT(T10,°COUNTS/PULSE   FOR CTR:°,I2,                      7250
*          * S+C°,F10.3°, C°,F10.3°, V+B°,F10.3°, B°,F10.3,/)      7260
C-----
C----- LIST RAW DATA -----
ICHNL1=(ICHNL/6)+1
IF(.NOT.PRINT)GOTO1290
WRITE(13,1250)INC
CALL OJOHNA(T,A,ICHNL,ICHNL1,4,6,°FF°,°S+C      °,13)
WRITE(13,1260)INC
CALL OJOHNA(T,B,ICHNL,ICHNL1,4,6,°FF°,°CAN      °,13)
WRITE(13,1270)INC
CALL OJOHNA(T,C,ICHNL,ICHNL1,4,6,°FF°,°V+B      °,13)
WRITE(13,1280)INC
CALL OJOHNA(T,D,ICHNL,ICHNL1,4,6,°FF°,°BACK    °,13)
1250 FORMAT(IH1,°SAMPLE+CAN RUN:°COUNTER°,I3)
1260 FORMAT(IH1,°CAN RUN:°COUNTER°,I3)
1270 FORMAT(IH1,°VANADIUM+BACKGROUND RUN:°COUNTER°,I3)
1280 FORMAT(IH1,°BACKGROUND RUN:°COUNTER°,I3)
1290 SIG1=SIGMA(1)
C-----
C----- APPLY DEAD TIME CORRECTIONS -----
CALL DEADT(RATIO,A,ICHNL,NDEAD,RPULSE,NCTRS,INC,DEAD,RMC,1)
CALL DEADT(RATIO,B,ICHNL,NDEAD,RPULSE,NCTRS,INC,DEAD,RMC,2)
CALL DEADT(RATIO,C,ICHNL,NDEAD,RPULSE,NCTRS,INC,DEAD,RMC,3)
CALL DEADT(RATIO,D,ICHNL,NDEAD,RPULSE,NCTRS,INC,DEAD,RMC,4)
DO 1300 K=1,ICHNL
1300 RATIO(K)=0.
      A(1)=1.
      B(1)=1.
      C(1)=1.
      D(1)=1.
C-----
C----- PLOT RAW DATA -----
IF(.NOT.PLOT)GOTO1310
CALL DRAW(,T,A,11,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,LAMBDA,
*      ABSORB,XMAX,XMIN)
CALL DRAW(,T,B,12,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,LAMBDA,
*      ABSORB,XMAX,XMIN)
CALL DRAW(,T,C,12,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,LAMBDA,
*      ABSORB,XMAX,XMIN)
CALL DRAW(,T,D,12,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,LAMBDA,
*      ABSORB,XMAX,XMIN)
1310 IF(TRANSM)GOTO1320
IF(CAN)CALL FRAME
IF(CAN)CALL SCALES
IF(CAN)CALL BORDER
C-----
C----- SMOOTH CONTAINER -----
IF(CAN)CALL SMTH(B,RATIO,T,ICHNL,CHAN,RD,W)
IF(SMOOTH.AND..NOT.CAN)CALL FRAME
IF(SMOOTH.AND..NOT.CAN)CALL SCALES
IF(SMOOTH.AND..NOT.CAN)CALL BORDER
C-----
C----- SMOOTH VANADIUM AND BACKGROUND -----
IF(SMOOTH)CALL SMTH(C,RATIO,T,ICHNL,CHAN,RD,W)
IF(SMOOTH)CALL SMTH(D,RATIO,T,ICHNL,CHAN,RD,W)
IF(.NOT.CAN.AND..NOT.SMOOTH)GOTO1320
CALL CTRMAG(1)
CALL PLACE(20,10)
CALL TYPECS(°SMOOTHED °,9)
CALL TYPECS(°COUNTER°,9)
CALL TYPENI(INC)
CALL PLACE(20,2)
CALL TYPECS(TITLE,72)
C-----
C----- DUMMY NO. TO SCRATCH DISC -----
1320 IF(EQUALQ)WRITE(14°INC)NC(INC)
IF(EQUALQ)WRITE(12,1330)INC,NC(INC)
1330 FORMAT(1X,°NC(INC) WRITTEN TO DISC #14 FOR COUNTER°,I3,° AS°,I3)
C-----
C----- PLACZEK CONSTANTS -----
IF(TRANSM)GOTO1480
ECON2=TFP*SIN(CA(INC))
ECON2=1./(ECON2*ECON2+ECON1)

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TEND=ZALZAS(DUMMY)
TDIFF=TEND-TSEG
WRITE(6,1340)INC,TDIFF
1340 FORMAT(/,T10,'COUNTER',13,' ABSORPTION + DISC SPOOLING',
* ' TAKES',F10.5,' SECS')
C
C----- COMPUTE PLAZCEK TERMS -----
C----- RATIO OF PATH LENGTHS (F) AND SIN**2(THETA) (SST) -----
SST=SIN(CA(INC))
SST=SST*SST
RANO=1./ANU
RN=.83
P1=-2.*SST*RANO*(1.-F*(1.-2.*RN))
P2=2.*SST*RANO**2*(1.-F*(1.-2.*RN))*(1.+2.*F*RN)*SST
P3=EBAR*(COS(CA(INC)*2.)-2.*F*(1.+2.*RN)*(1.-2.*F*(1.+RN))*SST)*
* 1.9366
P4=1.+P1+P2
WRITE(6,1350)P1,P2,P3
1350 FORMAT(/,T10,'PLAZCEK TERMS ARE:',3F10.5)
C
C----- COMPUTE RHO*SIGMA TERMS -----
IF(.NOT.EXPD)GOTO1360
IF(VROD )VOLVR=RHOV*R4*1.570796
IF(VCOIL )VOLVC=RHOV*(R5-R4*R4/R5)*1.570796
IF(SKOD )VOLSR=RHOS*R1*1.570796
1360 IF(VPLATE)VOLVP=RHOV*R4*COSSV
IF(SPLATE)VOLSP=RHOS*R1*COSS
IF(EXPD )GOTO1370
IF(SKOD )VOLSR=RHOS*R1*R1*3.141592654
IF(VROD )VOLVR=RHOV*R4*R4*3.141592654
IF(VCOIL )VOLVC=RHOV*(R5*R5-R4*R4)*3.141592654
C
C----- PLOT ABSORPTION CORRECTION TERMS -----
1370 CALL FRAME
CALL MAP (AMINI(T(1),T(ICHNL)),AMAXI(T(1),T(ICHNL)),.5,1.(5)
CALL WINDOW(AMINI(T(1),T(ICHNL)),AMAXI(T(1),T(ICHNL)),.5,1.(5)
CALL SCALES
CALL BORDER
CALL CTRMAG(1 )
CALL PLACE(24,2)
CALL TYPECS(TITLE,72)
CALL CTRMAG(15)
CALL PLACE(40,45)
CALL TYPECS('PAALMAN AND PINGS CORRECTION TERMS: COUNTER',42)
CALL TYPENI(INC)
CALL CTRMAG(1)
RIRT =1./FLOAT(NCPK)
C
C----- SET UP PAALMAN AND PINGS TERMS FOR EACH CHANNEL -----
RTIME=R1
DO 1450 K=1,ICHNL
C----- CHOOSE ELEMENT OF ARRAY -----
J =(K-1)/NCPK+1
RK =FLOAT(K-(J-1)*NCPK-1)*RIRT
JP1 =J+1
ASS =ASS1(J)+RK*(ASS1(JP1)-ASS1(J))
ACC =ACC1(J)+RK*(ACC1(JP1)-ACC1(J))
ACS =ACS1(J)+RK*(ACS1(JP1)-ACS1(J))
ASV =ASS2(J)+RK*(ASS2(JP1)-ASS2(J))
ASV2=1.
CALL PLOTNC(T(K),ASS,43)
CALL PLOTNC(T(K),ACC,43)
CALL PLOTNC(T(K),ACS,43)
CALL PLOTNC(T(K),ASV,43)
CALL PLOTNC(T(K),ASV2,43)
C
C----- CHECK TO SEE IF BACKGROUND IS TO BE SUBTRACTED FROM -----
C----- (SAMPLE AND CAN) AND CAN SEPARATELY -----
SC=C(K)
SD=D(K)
IF(CRYOST)GOTO1380
SA=A(K)-SD
SB=B(K)-SD
GOTO1390
1380 SA=A(K)
SB=B(K)
C
C----- FINISHED WITH A,B,C & D -----
1390 IF(.NOT.ASSORB)GOTO1400
TOP=(SA-SB*ACS/ACC)/ASS

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BOTTOM=(SC-SD)/ASV
GOTO1410
1410 TOP=SA-SA
BOTTOM=SC-SD
C
C---- ZERO DIVIDE CHECK FOR VANADIUM -----
1410 IF(BOTTOM.LE..00001)WRITE(6,1420)INC,K,BOTTOM,SC,SD
IF(BOTTOM.LE..00001)GOTO1450
1420 FORMAT(T1,'VANADIUM < .00001 FOR COUNTER',I3,' CHANNEL',I5,
A * BOTTOM =',F12.5,' SC=',F12.5,' SD=',F12.5)
RATIO(K)=TOP/BOTTOM
B1S=SIGMA1(I)
B1V=SIGMA3(I)
C
C---- CORRECT FOR AREA OF SAMPLE AND VANADIUM STANDARD -----
IF(.NOT.EXPO)GOTO1430
IF(SROD )RATIO(K)=RATIO(K)/(2.*R1)
IF(SPLATE)RATIO(K)=RATIO(K)/WIDTH
IF(VROD )RATIO(K)=RATIO(K)*R4
IF(VCOIL )RATIO(K)=RATIO(K)*R5
IF(VPLATE)RATIO(K)=RATIO(K)*WIDTH
IF(SROD )RATIO(K)=RATIO(K)/(1.-EXP(-B1S*VOLSR))
IF(SPLATE)RATIO(K)=RATIO(K)/(1.-EXP(-B1S*VOLSP))
IF(VROD )RATIO(K)=RATIO(K)*(1.-EXP(-B1V*VOLVR))
IF(VCOIL )RATIO(K)=RATIO(K)*(1.-EXP(-B1V*VOLVC))
IF(VPLATE)RATIO(K)=RATIO(K)*(1.-EXP(-B1V*VOLVP))
1430 IF(EXPO)GOTO144
IF(VROD )RATIO(K)=RATIO(K)*B1V*VOLVR
IF(VCOIL )RATIO(K)=RATIO(K)*B1V*VOLVC
IF(VPLATE)RATIO(K)=RATIO(K)*B1V*VOLVP
C
C---- COMPUTE D(SIGMA)/D(OMEGA) -----
1440 IF(EXPO.AND.(SROD.OR.SPLATE))A(K)=RATIO(K)*.0795774715*B1S
IF(.NOT.EXPO.AND.SROD ) A(K)=RATIO(K)*.0795774715/VOLSR
IF(.NOT.EXPO.AND.SPLATE ) A(K)=RATIO(K)*.0795774715/VOLSP
C
C---- COMPUTE S(Q) -----
RTIME=RTIME+CHAN
QS=ELCON2*RTIME**2
RATIO(K)=1.+(A(K)*FP1-B1S*(P4+P3*QS))/SCDH
1450 CONTINUE
C
C---- PRINT OUT S(Q) AND D(SIGMA)/D(OMEGA) -----
WRITE(6,1460)INC
CALL OJHNA(T,RATIO,ICHNL,ICHNL1,4,5,'FF','S(Q) ',6)
WRITE(6,1470)INC
CALL OJHNA(T,A,ICHNL,ICHNL1,4,5,'FF','DS/DW ',6)
1460 FORMAT(1H1,T1,'S(Q) FOR COUNTER',I3)
1470 FORMAT(1H1,T1,'DS/DW FOR COUNTER',I3)
C
C---- COMPUTE, LIST AND PLOT TRANSMISSION RATIOS FOR SAMPLE AND VANADIUM
1480 IF(.NOT.TRANS)GOTO1540
CON4=1./(TFP*252.7)
DO 1490 K=1,ICHNL
C==== WAVELENGTH SCALE =====
T(K)=(R1+FLOAT(CHAN*K))*CON4
C---- SAMPLE/CONTAINER -----
RATIO(K)=A(K)/B(K)
C---- VANADIUM/BACKGROUND -----
1490 A(K)=C(K)/D(K)
C
C---- LIST -----
WRITE(6,1500)INC
CALL OJHNA(T,RATIO,ICHNL,ICHNL1,4,5,'FF','SAMPLE ',6)
WRITE(6,1510)INC
CALL OJHNA(T,A,ICHNL,ICHNL1,4,5,'FF','VANADIUM',6)
1500 FORMAT(1H1,T1,'TRANSMISSION RATIO FOR SAMPLE COUNTER',I3)
1510 FORMAT(1H1,T1,'TRANSMISSION RATIO FOR VANADIUM',I3)
C
C---- PLOT RATIOS -----
CALL DRAW(3,T,RATIO,INC,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,LAMBDA,
* ABSORB,XMAX,XMIN)
C==== COMPUTE TRANSMISSION RATIO FROM CROSS SECTIONS IN READ1 AND ASIGMA
C==== ABSORPTION CROSS SECTION CONSTANT =====
B2S2=B2S1/CON4
C==== SCATTERING CROSS SECTION IN SHORT CUT CASE OF ONE VALUE IN READ1 =
IF(IMAX1.EQ.1)B1S2=SIGMA1(I)
VOLSP=-RHOS*R1*COUSS
VOLSR=-RHOS*R1*1.571796
DO 1520 K=1,ICHNL

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C==== SCATTERING CROSS SECTION FROM READ1 ARRAYS SIGMA AND E ===== 9600
IF (IMAX1.GT.1)B1S2=BARN1(K,SIGMA1,E1,RI,TFP,CHAN,1) 9610
C==== FIRST FLAT PLATE CASE ===== 9620
IF(SPLATE)RATIO(K)=EXP(VOLSP*(B2S2*T(K)+B1S2)) 9630
C==== SECONDLY ROD WITH EFFECTIVE THICKNESS PI*RADIUS/2 ===== 9640
IF(SROD )RATIO(K)=EXP(VOLSR*(B2S2*T(K)+B1S2)) 9650
1520 CONTINUE 9660
C==== NOW PLOT AS A LINE ON MEASURED RATIO ===== 9670
CALL PTPLOT(T,RATIO,1,ICHNL,-43) 9680
C 9690
C==== REPEAT SEQUENCE FOR VANADIUM STANDARD ===== 9700
CALL DRAW(4,T,A,INC,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,LAMBDA, 9710
* ABSORB,XMAX,XMIN) 9720
B2V2=B2V1/CON4 9730
VOLVP=-RHOV*R4*COVS 9740
VOLVR=-RHOV*R4*1.571796 9750
VOLVC=-RHOV*(R5-R4*R4/R5)*1.570796 9760
IF (IMAX3.EQ.1)B1V2=SIGMA3(1) 9770
DO 1530 K=1,ICHNL 9780
IF (IMAX3.GT.1)B1V2=BARN1(K,SIGMA3,E3,RI,TFP,CHAN,3) 9790
IF(VPLATE)RATIO(K)=EXP(VOLVP*(B2V2*T(K)+B1V2)) 9800
IF(VROD )RATIO(K)=EXP(VOLVR*(B2V2*T(K)+B1V2)) 9810
IF(VCOIL )RATIO(K)=EXP(VOLVC*(B2V2*T(K)+B1V2)) 9820
1530 CONTINUE 9830
CALL PTPLOT(T,RATIO,1,ICHNL,-43) 9840
GOTO1550 9850
C 9860
C 9870
C----- PLOT ----- 9880
1540 IF(.NOT.PLOT)GOTO1550 9890
CALL DRAW(1,T,RATIO,INC,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF, 9900
* LAMBDA,ABSORB,XMAX,XMIN) 9910
CALL DRAW(2,T,A ,INC,ICHNL,SQMAX,SQMIN,TITLE,SIG1,Q,TOF, 9920
* LAMBDA,ABSORB,XMAX,XMIN) 9930
C 9940
C----- PUNCH ----- 9950
1550 IF(.NOT.PUNCH)GOTO1580 9960
DO 1560 I=1,ICHNL,12 9970
II=(I/12)+1 9980
IF(.NOT.SMQ)WRITE(7,1570)(A(I+K-1),K=1,12),11 9990
1560 IF(SMQ)WRITE(7,1570)(RATIO(I+K-1),K=1,12),II 10000
1570 FORMAT(12F6.3,18) 10010
C 10020
C----- WRITE S(Q) OR DS/DW TO SCRATCH DISC ----- 10030
1580 IF(EQUALQ.AND.SMQ)WRITE(14*INC)NC(INC),RATIO 10040
IF(EQUALQ.AND..NOT.SMQ)WRITE(14*INC)NC(INC),A 10050
WRITE(6,1590) 10060
1590 FORMAT(T10,'DATA FILE WRITTEN TO DISC #14') 10070
C 10080
C----- END TIMING SEQUENCE ----- 10090
TEND =ZAQZAS(DUMMY) 10100
TDIFF=TEND-TBEG 10110
WRITE(6,1610)INC,TDIFF 10120
1600 CONTINUE 10130
1610 FORMAT(T10,'COMPLEAT COUNTER',I3,' TAKES ',F10.5,' SECONDS') 10140
C 10150
C----- EQUAL QBIN SUBROUTINE ----- 10160
IF(.NOT.TRANS)CALL QBIN(TITLE,ICHNL,RI,CHAN,CA,TFP,NCTRS,RATIO, 10170
* T,D,WK,QK,RSK,NC,EQUALQ) 10180
1620 CONTINUE 10190
CALL GREND 10200
STOP 10210
C 10220
C----- ERROR MESSAGE WHEN ALL COUNTERS HAVE BEEN SWITCHED OFF ----- 10230
1630 WRITE(6,1640) 10240
1640 FORMAT(T10,'*****',/,T10,'DU YOU REALLY WANT TO SWITCH OFF ALL YOUR CO 10250
*****',/,T10,'PROGRAM HAS RESET COUNTER 1 NC(1) TO 1 AND WILL 10260
*UNTERS ???',/,T10,'PROGRAM HAS RESET COUNTER 1 NC(1) TO 1 AND WILL 10270
A CONTINUE',/) 10280
NC(1)=1 10290
GOTO2 10300
END 10310
FUNCTION BARN1(IT,S,E,RI,TFP,ICHNLW,N) 10310
C 10311
C----- FUNCTION (BARN1) TO FIND SCATTERING CROSS-SECTION AS A FUNCTION 10312
C----- OF TIME CHANNEL (IT) FROM THE CROSS-SECTION ARRAY (SIGMA) VERSUS 10313
C----- ENERGY (E) ----- 10314
C----- INITIAL DELAY (RI) MICROSECONDS ----- 10316
C----- TOTAL FLIGHT PATH (TFP) METRES ----- 10317
C----- CHANNEL WIDTH (ICHNLW) MICROSECONDS ----- 10318

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C---- SAMPLE TYPE (N) 1 TO 3 (SAMPLE,CAN,VANADIUM) ----- 10319
C 10320
REAL CON5/5225.87,S(1),E(1) 10330
C---- CONVERT TIME OF FLIGHT TO ENERGY IN EV ----- 10340
CHANL=FLOAT(ICHNLW*11) 10350
SPEED=TFP/(RI+CHANL) 10360
DE=CON5*SPEED*SPEED 10370
C---- CHECK LOWER ENERGY END OF MESH ----- 10380
J=1 10390
IF(DE.LT.E(1))WRITE(6,40)DE,N 10100
10 J=J+1 10110
C---- CHECK UPPER ENERGY END OF MESH ----- 10120
IF(J.GT.40)WRITE(6,50)DE,N 10130
IF(DE-E(J))30,21,10 10140
20 BARN1=S(J) 10150
RETURN 10160
C---- LINEARLY INTERPOLATE FOR FUNCTION ----- 10170
30 JM1=J-1 10180
BARN1=S(JM1)+(S(J)-S(JM1))*(DE-E(JM1))/(E(J)-E(JM1)) 10190
40 FORMAT(' ***** ENERGY MESH DOES NOT GO LOW ENOUGH IN ENERGY RANGE 10200
1 AT ',E12.3,' EV FOR SAMPLE TYPE ',I3) 10210
50 FORMAT(' ENERGY MESH DOES NOT GO HIGH ENOUGH IN ENERGY RANGE AT ', 10220
1 E12.3,' EV FOR SAMPLE TYPE ',I3) 10230
RETURN 10240
END 10250
SUBROUTINE OJOHNA (X,Y,M,NC,NSX,NSY,NF,H,IOUTP) 10210
C 10211
C---- MODIFIED HARWELL LIBRARY ROUTINE (OAJ3A) ----- 10212
C---- WILL PRINT X AND Y ARRAYS OF M ELEMENTS IN NC COLUMNS----- 10213
C---- NSX FIGURES IN X, NSY FIGURES IN Y ----- 10214
C---- 'FF' 'EF' 'FE' 'EE' FORMATS (NF) ----- 10215
C---- HEADER CAPTION (H) OF 8 CHARACTERS ----- 10216
C---- OUTPUT CHANNEL (IOUTP) ----- 10217
C 10218
REAL*4 X(1),Y(1),H*8 10230
INTEGER*2 F1(16)/*(1X,00( 4X,0PF00. 00,2X ,1PE00. 00))*/, 10240
A F2(11)/*( 00X,A8, 00( 00X,A8))*/,NFL,NF,CO/* ,0*/,C1/* ,1*/, 10250
B PF/*PF*/,PE/*PE*/,FF/*FF*/,FE/*FE*/,EF/*EF*/ 10260
INTEGER*4 MXFW/60/,LLL/128/ 10270
LOGICAL*1 LF(2) 10280
EQUIVALENCE (NFL,LF(1)) 10290
NFL=NF 10100
IF(NF.EQ.FF.OR.NF.EQ.FE) GO TO 20 10110
10 NXDEC=MAX0(NSX-1,0) 10120
NXW=NXDEC+7 10130
F1(6)=C1 10140
F1(7)=PE 10150
GO TO 30 10160
20 CALL OAJ3B (X,M,NXW,NXDEC,NSX) 10170
IF(NXW.GT.MXFW) GO TO 10 10180
F1(6)=C1 10190
F1(7)=PF 10200
30 CALL OAJ3C (F1,8,NXW) 10210
CALL OAJ3C (F1,10,NXDEC) 10220
IF(NF.EQ.FF.OR.NF.EQ.EF) GO TO 50 10230
40 NYDEC=MAX0(NSY-1,0) 10240
NYW=NYDEC+7 10250
F1(13)=C1 10260
F1(14)=PE 10270
GO TO 60 10280
50 CALL OAJ3B (Y,M,NYW,NYDEC,NSY) 10290
IF(NYW.GT.MXFW) GO TO 40 10300
F1(13)=C1 10310
F1(14)=PF 10320
60 CALL OAJ3C (F1,15,NYW) 10330
CALL OAJ3C (F1,17,NYDEC) 10340
NCOL=LLL/(NXW+NYW+6) 10350
IF(NCOL.EQ.0) GO TO 140 10360
CALL OAJ3C (F1,3,NCOL) 10370
K=NYW+NXW-2 10380
J=NXW+NYW/2+4 10390
CALL OAJ3C (F2,2,J) 10400
CALL OAJ3C (F2,8,K) 10410
CALL OAJ3C (F2,6,NCOL-1) 10420
K=NCOL 10430
IM=(M-1)/NC+1 10440
IK=(IM-1)/K+1 10450
IT=M-(IM-1)*NC 10460
ITAB=0 10470
II=NC 10480

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      I3=NC*(K-1)
      NC3=NCOL
70  IF(IK.LE.0)RETURN
      IF(IK.GT.1) GO TO 90
80  I1=IT
      I3=(I1-1)*NC
      NC3=IM
90  WRITE(IOUTP,F2) (H,J=1,NC3)
      DO 100 I=1,I1
          I2=ITAB+I
          I4=I2+I3
100  WRITE(IOUTP,F1) (X(J),Y(J),J=I2,I4,NC)
      IF(IM.EQ.1.OR.I1.EQ.NC) GO TO 120
      I31=I3-NC
      I11=I1+1
      DO 110 I=I11,NC
          I2=ITAB+I
          I4=I2+I31
110  WRITE(IOUTP,F1) (X(J),Y(J),J=I2,I4,NC)
120  ITAB=ITAB+NC*K
      IK=IK-1
      IM=IM-K
      WRITE(IOUTP,130)
130  FORMAT(' ')
      GO TO 70
140  WRITE(IOUTP,150)
150  FORMAT('0 ***** OJOHNA ERROR: FIELD WIDTHS OF COLUMNS TOO WIDE FOR
*PAGE')
      WRITE(IOUTP,160) LF(1),NXW,NXDEC,LF(2),NYW,NYDEC
160  FORMAT('          FORMATS X: ',A1,I2,',',I2,' Y: ',A1,I2,',',I2)
      RETURN
      END
      SUBROUTINE DRAW(IW,X,Y,J,IMAX,SQMAX,SQMIN,TITLE,SIG1,Q,TOF,
* LAMBDA,ABSORB,XMAX1,XMIN1)
C
C---- ROUTINE PLOTS ARRAY (Y) AGAINST ARRAY (X) OF (IMAX) POINTS-----
C---- BETWEEN (XMIN1) AND (XMAX1) AND SQMIN AND SQMAX -----
C---- IW IS THE FUNCTION TYPE INDICATOR (1-4) S(Q),DS/DW,RATIOS -----
C---- TITLE IS ON EVERY GRAPH -----
C---- SIG1 IS THE MEAN VALUE FOR DS/DW GRAPHS -----
C---- Q,TOF AND LAMBDA INDICATE TYPE OF X-SCALE -----
C---- ABSORB INDICATES ABSORPTION CORRECTION FOR MESSAGE BOX ON GRAPH ---
C
      REAL X(248),Y(248),TITLE(18),SQMAX(8),SQMIN(8),XMAX1(8),XMIN1(8)
      INTEGER DAY,YEAR
      LOGICAL Q,TOF,LAMBDA,ABSORB
C
C---- J=11,12,13,14 ARE SAMPLE+CAN,CAN,VANADIUM+BACKGROUND & BACKGROUND--
      IF(J.GT.11)GOTO4
      YMIN=Y(MNOLA(Y(1),Y(2),IMAX))
      YMAX=Y(MXOLA(Y(1),Y(2),IMAX))*1.1
      XMIN=X(MNOLA(X(1),X(2),IMAX))
      XMAX=X(MXOLA(X(1),X(2),IMAX))
C
C---- SAMPLE ETC RUNS RAW DATA GOTO 4 -----
      IF(J.GT.8)GOTO3
      IF(SQMAX(J).LT..001)GOTO2
      YMAX=SQMAX(J)
      YMIN=SQMIN(J)
      WRITE(12,10)J,SQMAX(J),SQMIN(J)
10  FORMAT(1X,'COUNTER',13,' YMAX SET TO',F7.3,' YMIN SET TO',F7.3)
C
C---- PLOT DS/DW -----
20  IF(IW.EQ.2)YMIN=0.
      IF(IW.EQ.2)YMAX=SIG1*.5/3.14159
      IF(XMAX1(J).LT..001)GOTO30
      XMAX=XMAX1(J)
      XMIN=XMIN1(J)
30  IF(XMAX.LE.XMIN.OR.YMAX.LE.YMIN)RETURN
C
C---- OVERPLOT SAMPLE+CAN,CAN,VANADIUM+BACKGROUND AND BACKGROUND -----
40  IF(J.LT.12)CALL FRAME
      CALL MAP (XMIN,XMAX,YMIN,YMAX)
      CALL WINDOW(XMIN,XMAX,YMIN,YMAX)
      IF(J.GT.11)GOTO50
      CALL SCALES
      CALL BORDER
50  CALL CTRMAG(1)
      IF(J.GT.8)GOTO60

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C----- PLOT PATTERN ----- 10410
CALL PTPLLOT(X,Y,1,IMAX,43) 10420
60 IF(J.LE.8)GOTO70 10430
CALL CTRMAG(1) 10440
CALL PTPLLOT(X,Y,1,IMAX,37) 10450
CALL CTRMAG(1) 10460
70 IF(J.GT.11)RETURN 10470
C 10480
C----- POSITION TITLE ----- 10490
CALL PLACE (2,2) 10500
CALL TYPECS(TITLE,72) 10510
CALL PLACE (2,5) 10520
CALL CTRORI(1.) 10530
CALL CTRMAG(15) 10540
C 10550
C----- CHOOSE AND PRINT THE APPROPRIATE Y-AXIS CAPTION ----- 10560
IF(J.EQ.11)CALL TYPECS('SAMPLE,CAN,VANADIUM + BACKGROUND',32) 10570
CALL CTRORI(0.) 10580
IF(J.GT.8)GOTO90 10590
CALL CTRORI(1.) 10600
IF(IW.NE.2)GO TO 80 10610
CALL CTRSET(2) 10620
CALL TYPENC(14) 10630
CALL CTRSET(4) 10640
CALL TYPENC(29) 10650
CALL TYPENC(45) 10660
CALL CTRSET(2) 10670
CALL TYPENC(14) 10680
CALL CTRSET(3) 10690
CALL TYPENC(33) 10700
CALL CTRSET(1) 10710
80 IF(IW.EQ.1)CALL TYPECS('S(Q)',4) 10720
IF(IW.EQ.3)CALL TYPECS('SAMPLE TRANSMISSION RATIO',25) 10730
IF(IW.EQ.4)CALL TYPECS('VANADIUM TRANSMISSION RATIO',27) 10740
CALL TYPECS('FOR COUNTER ',13) 10750
CALL TYPENI(J) 10760
CALL CTRORI(0.) 10770
C 10780
C----- CHOOSE AND PRINT THE APPROPRIATE X-AXIS CAPTION ----- 10790
90 CALL PLACE(4,4) 10800
IF(IW.LT.3)GOTO100 10810
CALL TYPECS('LAMBDA ANGSTROMS',17) 10820
IF(IW.GE.3)GOTO110 10830
100 IF(Q) CALL TYPECS('Q RECIPROCAL ANGSTROMS',23) 10840
IF(TOF) CALL TYPECS('T.O.F. MICROSECONDS ',23) 10850
IF(LAMBDA)CALL TYPECS('LAMBDA ANGSTROMS ',23) 10860
110 IF(J.GT.8)RETURN 10870
C 10880
C----- DRAW BOX IN TOP RIGHT HAND CORNER AXIS CAPTION ----- 10890
YTOP=.8*YMAX+.2*YMIN 10900
XTOP=.8*XMAX+.2*XMIN 10910
CALL BOX(XTOP,XMAX,YTOP,YMAX) 10920
CALL CTRMAG(1) 10930
CALL POSITN(.9*XTOP+.1*XMAX,.9*YMAX+.1*YTOP) 10940
IF(.NOT.ABSORB)CALL TYPECS(' NO ABSORPTION CORRECTIONS ',33) 10950
IF(ABSORB) CALL TYPECS(' ABSORPTION CORRECTIONS ',33) 10960
CALL POSITN(.9*XTOP+.1*XMAX,.9*YMAX+.1*YTOP) 10970
CALL LINEFD(2) 10980
CALL TYPECS(' APPLIED',15) 10990
CALL POSITN(.9*XTOP+.1*XMAX,.9*YMAX+.1*YTOP) 11000
CALL LINEFD(4) 11010
CALL ZAIAS(DAY,MONTH,YEAR) 11020
CALL TYPENI(DAY) 11030
CALL TYPECS(' ',1) 11040
CALL TYPECS(MONTH,4) 11050
CALL TYPECS(' ',1) 11060
CALL TYPENI(YEAR) 11070
WRITE(12,12) 11080
120 FORMAT(1X,'GRAPH PLOTTED') 11090
RETURN 11100
END 11110
SUBROUTINE SMTH(A,B,C,ICHNL,CHAN,RD1,WIDTH) 11110
C 11120
C 11111
C----- SMOOTHS ARRAY (A) AS A FUNCTION OF ARRAY (C).----- 11113
C----- ELIMINATES BOOSTER PEAK AT 26.5 MICROSECONDS ----- 11114
C----- ICHNL POINTS IN ARRAY ----- 11115
C----- CHANNEL WIDTH IS (CHAN) MICROSECONDS ----- 11116
C----- INITIAL DELAY (RD1) MICROSECONDS ----- 11115
C----- WRITES INTO ARRAY (3) THEN WRITES BACK TO (A) THEN ZEROES (B)----- 11116

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C----- USES RECTANGULAR SMOOTHING FUNCTION PERCENTAGE WIDTH IS (WIDTH) -----11117
C                                                                                   11118
REAL A(ICHNL),B(ICHNL),C(ICHNL)                                                                                   11151
INTEGER CHAN                                                                                                       11160
C----- DEFINE 1 FOR 255. AND 275. MICROSECS. -----11170
I2550=(2500.-RDI)/CHAN+.5                                                                                       11180
I2750=(2700.-RDI)/CHAN+.5                                                                                       11190
RIMI=FLOAT(I2750-I2550)                                                                                         11100
OMW=1.-WIDTH                                                                                                     11110
OPW=1.+WIDTH                                                                                                     11120
RI=0.                                                                                                             11130
C                                                                                   11140
C----- CORRECT FOR BOOSTER -----11150
DO 10 I=1,ICHNL                                                                                                   11160
IF(I.GE.I2550.AND.I.LE.I2750)A(I)=A(I2550)+(A(I2750)-A(I2550))
A=FLOAT(I-I2550)/RIMI                                                                                           11170
10 CONTINUE                                                                                                       11180
DO 30 I=1,ICHNL                                                                                                   11190
SUM=0.                                                                                                           11200
C----- COMPUTE T1 AND T2 -----11220
RI=RI+1.                                                                                                         11230
I1=INT(RI*OMW+.5)                                                                                               11240
I2=INT(RI*OPW+.5)                                                                                               11250
IF(I1.LE.1)I1=2                                                                                                 11260
IF(I2.LE.1)I2=2                                                                                                 11270
IF(I2.GT.ICHNL)I2=ICHNL                                                                                       11280
C----- INTEGRATE A FROM T1 TO T2 AND STORE IN SUM -----11290
DO 20 J=I1,I2                                                                                                   11300
20 SUM=SUM+A(J)                                                                                                 11310
30 B(I)=SUM/FLOAT(I2-I1+1)                                                                                     11320
C----- PLOT SMOOTHED AND UNSMOOTHED ARRAYS A AND B -----11330
CALL CTRMAG(3)                                                                                                   11340
CALL PTPLOT(C,B,1,ICHNL,-43)                                                                                   11350
CALL PTPLOT(C,A,1,ICHNL,43)                                                                                   11360
C                                                                                   11370
C----- RESET ARRAY B TO A AND SET B TO ZERO -----11380
DO 40 I=1,ICHNL                                                                                                   11390
A(I)=B(I)                                                                                                       11400
40 B(I)=0.                                                                                                       11410
RETURN                                                                                                           11420
END                                                                                                             11430
SUBROUTINE DISC(A,IARR,NRUN,ICHNL,INC,ICON,SUM,K,J,RMC,*,*,
A NTRN,M,MPRF,RPULSE,JMAX,NSEQ)
C                                                                                   11430
C----- FINDS A RUN OF NAME:NRUN -----11440
C----- THERE ARE :ICHNL CHANNELS PER COUNTER,THE COUNTER NO. IS:INC -----11450
C----- READS RUN OFF THE DISC ADDS IT INTO ARRAY :A(ICHNL) -----11460
C----- RETURNS THE CONTROL RECORD:ICON(256) -----11470
C----- ADDS IN THE MONITOR COUNT TO ARRAY:RMC(INC,4) -----11480
C----- ADDS IN THE PRF PULSE TO ARRAY : RPULSE -----11490
C----- RUN TYPE :K 1,2,3 OR 4 -----11500
C----- ADDS IN A TO TOTAL COUNT :SUM(K,INC,JJ) -----11510
C----- INCREMENTS J AND RETURNS TO NEXT RUN OR TO REST OF PROGRAM -----11520
C                                                                                   11540
REAL A(2048),RMC*4(8,4),SUM*4(4,8,80),RPULSE(8,4)
INTEGER ICON(256),M(8,80),NTRN(80),NRMAX/80/,IARR(16384),
* MPRF(8,80),NSEQ(80)
C----- REWIND ALL DATA SETS -----11570
REWIND 1                                                                                                       11580
C----- DUMMY COUNT SUM -----11590
SK=SUM(K,INC,J)                                                                                                 11600
C----- LABEL SHIFT -----11610
KSHIFT=(INC-1)*ICHNL
IF(J.EQ.1)WRITE(12,10)
WRITE(12,20)NRUN,ICHNL,INC,J
10 FORMAT(/,1X,'LOG OF SCRATCH DISC OPERATIONS OUTPUT CHANNEL 12',/)
20 FORMAT(1X,'LOOKING FOR RUN',110,' OF',16,' CHANNELS COUNTER',
A 12,' RUN COUNTER',13)
DO 30 K1=1,NRMAX
C----- RUN IS THE K1 TH IN THE LIST AND IS IN POSITION NSEQ(K1) ON DISC
IF(NRUN.EQ.NTRN(K1))GOTO90
30 CONTINUE
WRITE(12,40)NRUN
40 FORMAT(1H+,T72,'RUN NUMBER',I13,' NOT FOUND IN INPUT RUN LIST')
GOTO140
50 WRITE(12,50)K2,NRMAX
60 FORMAT(1X,'END-OF-FILE FOUND RUN COUNTER K2=',I4,' NRMAX =',I3)
GOTO140
70 WRITE(12,80)K2,NRMAX
80 FORMAT(1X,'RUN NOT FOUND ON DISC K2=',I4,' NRMAX=',I3)

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GOTO140 11400
C----- READ CONTROL RECORD ----- 11410
90 NSEQ1=NSEQ(K1)-1 11420
IF(NSEQ1.EQ.0)GOTO110 11430
DO 100 K2=1,NSEQ1 11440
100 READ(1,END=50) 11450
110 READ(1,END=50)ICON,IARR 11460
WRITE(12,12)INRUN 11470
120 FORMAT(1H+,T72,'*RUN NUMBER*',I10,' * FOUND IN INPUT RUN LIST*') 11480
DO 130 K3=1,ICHNL 11490
COUNT=FLOAT(IARR(K3+KSHIFT)) 11500
C----- TRANSFER COUNTS TO ARRAY A AND ADD IN TO SUM (SK) ----- 11510
SK=SK+COUNT 11520
130 A(K3)=A(K3)+COUNT 11530
C----- SUM IN MONITOR COUNTS AND PRF PULSES ----- 11540
K PULSE(INC,K)=K PULSE(INC,K)+FLOAT(MPRF(INC,J)) 11550
RMC(INC,K)=RMC(INC,K)+FLOAT(M(INC,J)) 11560
SUM(K,INC,J)=SK 11570
140 IF(J.GE.JMAX)RETURN2 11580
J=J+1 11590
RETURN1 11600
END 11610
SUBROUTINE ABSORP(SSCAT,SABS,CSCAT,CABS,RHOS,RHOC,R1,R2,DELTAR, 11610
* ASS,ACC,ACS,THET,IROUTE,AB,SI,AS,ENU,NU,R,ABSORB,SCATTR,SPLATE, 11620
* VPLATE,TRANS) 11630
C
C----- COMPUTES PAALMAN AND PINGS TERMS FOR A CYLINDRICAL SAMPLE-----
C----- COMPUTES SIMILAR TERMS FOR A FLAT PLATE CONTAINER-----
C----- SSCAT : SAMPLE SCATTERING CROSS-SECTION -----
C----- SABS : SAMPLE ABSORPTION CROSS-SECTION -----
C----- CSCAT : CAN SCATTERING CROSS-SECTION -----
C----- CABS : CAN ABSORPTION CROSS-SECTION -----
C----- RHOS : SAMPLE NUMBER DENSITY -----
C----- RHOC : CAN NUMBER DENSITY -----
C----- R1 : SAMPLE RADIUS -----
C----- R2 : CAN RADIUS (OUTER) -----
C----- DELTAR : INCREMENT IN RADIUS -----
C----- R1 : SAMPLE THICKNESS -----
C----- R2 : (SAMPLE + CAN THICKNESS) -----
C----- DELTAR : ANGLE OF PLATE NORMAL TO BEAM -----
C----- IF CYLINDRICAL GEOMETRY (SRDOD,VROD, OR VCOIL)-----
C----- IF PLATE GEOMETRY (VPLATE OR SPLATE) -----
C----- ASS: PAALMAN AND PINGS SAMPLE ABSORPTION TERM -----
C----- ACC AND ACS : PAALMAN AND PINGS CAN AND CROSS ABSORPTION TERMS -----
C----- THET: ANGLE OF DETECTOR IN RADIANES -----
C----- IRDUTE (1,2) SAMPLE OR VANADIUM (SAVES TIME NOT CALCULATING ACS)-----
C----- AB,SI,AS,ENU,NU: INTEGRAL TERMS IN ROUTINE --EQUIVALENCED IN MAIN-----
C----- R : RADII OF SHELLS IN CYLINDRICAL SAMPLE INTEGRATION -----
C----- ABSORB: LOGICAL VARIABLE SWITCHING ON ABSORPTION -----
C----- SCATTR: LOGICAL VARIABLE SWITCHING ON SCATTERING CROSS-SECTION -----
C----- SPLATE, VPLATE: SAMPLE AND VANADIUM PLATE SWITCHES -----
C----- TRANS: LOGICAL VARIABLE SPECIFYING TRANSMISSION OR REFLECTION -----
C
REAL R(20),AB(60,20),SI(60,20),AS(60,20),ENU(60,20),NU(60,20), 11640
* PI/3.14159/,PIBY2/1.57073/,DRM/-.5/ 11650
LOGICAL ABSORB,SCATTR,SPLATE,VPLATE,YESACC,NOACC, 11660
*L1,L2,L3,L4,L5,L6,L7,L8,L9,L10,L11,L12,L13,L14,L15,L16,L17,L18,L19 11670
*,L20,L21,TRANS 11680
C----- IF THERE IS NO ABSORPTION CORRECTION REQUIRED PROGRAM 11690
C----- LOOPS OUT AFTER SETTING ALL PAALMAN AND PINGS TERMS 11100
C----- TO UNITY 11110
IF(.NOT.ABSORB)GOTO90 11120
IF(.NOT.SCATTR)SSCAT=.0 11130
IF(.NOT.SCATTR)CSCAT=.0 11140
C----- 20 ZONES, SAMPLE RADIUS:R1,CAN OUTER RADIUS:R2, 11150
C----- INCREMENT:DELTAR,ANGLE:THET(RADIANS) 11160
C-----CONSTANTS 11170
ITHET=2.*THET 11180
TMPB2=THET-PIBY2 11190
TPPB2=THET+PIBY2 11200
C-----N*SIGMA (SAMPLE) OR MU(SAMPLE) 11210
STS=(SSCAT+SABS)*RHUS 11220
C-----N*SIGMA (CAN) OR MU(CAN) 11230
STC=(CSCAT+CABS)*RHOC 11240
C----- IF THE SAMPLE SPECIFIED IS A PLATE PROGRAM CALCULATES 11250
C----- DIFFERENT SET OF TERMS 11260
IF(SPLATE.OR.VPLATE)GOTO100 11270
C----- NO OF RINGS IN SAMPLE 11280
MR=R1/DELTAR+.1 11290
R10MR=R1/FLOAT(MR) 11300

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C-----NO OF RINGS IN SAMPLE AND CAN                                11310
      MMAX=R2/DELTAR+.1                                             11320
      R1SQ=R1*R1                                                    11330
      R2SQ=R2*R2                                                    11340
C-----COMMON FACTOR                                              11350
      FAK=.66666/FLOAT(MR*MR)                                       11360
      SINT=SIN(THET)                                                11370
      COST=COS(THET)                                                11380
      R1OCST=R1/COST                                                11390
C-----COMPUTE ALL TERMS ALPHA,BETA ETC.                          11400
      DRM=-.5                                                       11410
      DO 10 M=1,MMAX                                                11420
C:::::R(M)=(FLOAT(M)-.5)*R1OMR                                       11430
      DRM=DRM+1.                                                    11440
      R(M)=DRM*R1OMR                                               11450
      ROM=R(M)                                                       11460
      RHO=R1/ROM                                                     11470
      RSQ=ROM*ROM                                                    11480
      NMAX=3*M                                                       11490
      PONMAX=PI/FLOAT(NMAX)                                         11500
      DRN=-.5                                                       11510
      DO 10 N=1,NMAX                                               11520
C-----OMEGA(N,M)                                                 11530
      DRN=DRN+1.                                                    11540
C:::::ONM=TMPB2+(FLOAT(N)-.5)*PONMAX                                  11550
      ONM=TMPB2+DRN*PONMAX                                          11560
      SINOMT=SIN(ONM-THET)                                          11570
      SONM=SIN(ONM)                                                  11580
      SSONM=SONM*SONM                                               11590
      RSQSS=RSQ*SSONM                                               11600
      SOM2T=SIN(ONM-TTHET)                                          11610
      SSOM2T=SOM2T*SOM2T                                           11620
      RSQSSM=RSQ*SSOM2T                                            11630
C-----ALPHA(N,M)+BETA(N,M)                                       11640
      AB(N,M)=SQRT(R2SQ-RSQSS)+SQRT(R2SQ-RSQSSM)                   11650
C-----SIGMA(N,M)                                                 11660
      SI(N,M)=2.*ROM*SINOMT*SINT                                    11670
C-----ALPHA+BETA-SIGMA                                           11680
      AS(N,M)=AB(N,M)-SI(N,M)                                       11690
C-----CHECK VALIDITY OF NU                                       11700
      IF(ABS(SONM).LT.RHO)NU(N,M)=SQRT(R1SQ-RSQSS)                 11710
      IF(ABS(SONM).GE.RHO)NU(N,M)=0.                                11720
C-----CHECK ETA LIMITS AND GET ETA +NU                           11730
      IF(ABS(SOM2T).LT.RHO)ENU(N,M)=SQRT(R1SQ-RSQSSM)+NU(N,M)     11740
      IF(ABS(SOM2T).GE.RHO)ENU(N,M)=NU(N,M)                       11750
C-----10 CONTINUE                                                11760
C-----OMEGA LIMITS IN ZONE D,RLIMITS ARE (R(M)<R1)              11770
      DHIGH=TPPB2                                                    11780
      DLOW =TPPB2                                                    11790
      ASS=0.                                                         11800
      IF(RHOS.EQ.0.)GOTO30                                          11810
      DO 20 M=1,MR                                                  11820
      NMAX=3*M                                                       11830
      PONMAX=PI/FLOAT(NMAX)                                         11840
      FU=1.-1./FLOAT(2*M)                                           11850
      DRN=-.5                                                       11860
      DO 20 N=1,NMAX                                               11870
      DRN=DRN+1.                                                    11880
C:::::ONM=TMPB2+(FLOAT(N)-.5)*PONMAX                                  11890
      ONM=TMPB2+DRN*PONMAX                                          11900
C----- COMPUTE ASS IN ZONE D                                       11910
      IF(ONM.LE.DHIGH.AND.ONM.GE.DLOW)ASS=ASS                      11920
      A +FU*EXP(-STS*(ENU(N,M)-SI(N,M)))-STC*(AB(N,M)-ENU(N,M))) 11930
      20 CONTINUE                                                  11940
      ASS=ASS+FAK                                                    11950
C-----30 IF(RHOS.EQ.0.)ASS=1.                                     11960
      ACC=0.                                                         11970
      ACS=0.                                                         11980
C-----CONSTANT                                                  11990
      FAK=FAK/(R2SQ/R1SQ-1.)                                         12000
C *****                                                           12010
C * SET UP LIMITS FOR OMEGA AND R(M) IN EACH ZONE A1,AC,B0,B1, & C * 12020

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C      * ALL ZONES HAVE TOPMOST LIMIT OF R2                      * 11110
C      * ZONES B0 AND C HAVE UPPER LIMIT OF R10CST <R1/COS(THET)> * 11120
C      * ZONES A1,B1 AND C HAVE LOWER LIMIT OF R1                * 11130
C      * ZONES A0 AND B1 HAVE LOWER LIMIT OF R10CST             * 11140
C      * COMPUTE NON M-DEPENDENT TERMS FIRST                     * 11150
C      *****                                                    * 11160
C      A1HIGH=DHIGH                                              11170
C      A1LOW =DLOW                                              11180
C      CLOW =DLOW                                              11190
C      YESACC=KHOC.NE.O.                                         11200
C      NOACC=KHOC.EQ.O.                                         11210
C----- SUM OVER MK                                           11220
C      MMIN=MR+1                                               11230
C      DO 80 M=MMIN,MMAX                                       11240
C----- COMPUTE M-DEPENDENT TERMS                               11250
C      ROM=R(M)                                               11260
C      A1LOW =ARSIN(R1/ROM)                                     11270
C      A1HIGH=-A1LOW                                          11280
C      B1HIGH=A1LOW                                           11290
C      B1LOW =TTHET-PI+A1LOW                                   11300
C      B1HIGH=A1LOW                                           11310
C      B1LOW =-A1LOW                                          11320
C      CHIGH =B1LOW                                           11330
C      FU=1.-1./FLOAT(2*M)                                     11340
C      NMAX=3*M                                               11350
C      PONMAX=PI/FLOAT(NMAX)                                   11360
C----- SUM OVER N                                           11370
C      DRN=-.5                                               11380
C      DO 80 N=1,NMAX                                         11390
C      DRN=DRN+1.                                             11400
C----- COMPUTE OMEGA                                         11410
C      ONM=TMPB2+(FLOAT(N)-.5)*PONMAX                          11420
C      ONM=TMPB2+DRN*PONMAX                                    11430
C----- COMPUTE ACC AND ACS                                    11440
C----- CHECK FOR EACH ZONE IN TURN                            11450
C----- CALCULATE DUMMY ARRAY VALUES                          11460
C      ASN =AS(N,M)                                           11470
C      STCASN=FU*EXP(-STC*ASN)                                  11480
C      TNU =2.*NU(N,M)                                         11490
C      STSTNU=EXP(-STS*TNU)                                    11500
C      SCASTN=FU*EXP(-STC*(ASN-TNU))                           11510
C      TENU =2.*ENU(N,M)                                       11520
C      SCASTE=FU*EXP(-STC*(ASN-TENU))                          11530
C      L1=ONM.LE.A1HIGH                                        11540
C      L2=ONM.GE.A1LOW                                        11550
C      L3=ONM.LE.A1HIGH                                        11560
C      L4=ONM.GE.A1LOW                                        11570
C      L5=ROM.GE.R10CST                                       11580
C      L6=ONM.LE.B1HIGH                                        11590
C      L7=ONM.GE.B1LOW                                        11600
C      L8=ROM.LE.R10CST                                       11610
C      L9=ROM.LE.R2                                           11620
C      L10=ONM.LE.B1HIGH                                       11630
C      L11=ONM.GE.B1LOW                                       11640
C      L12=ONM.LE.CHIGH                                       11650
C      L13=ONM.GE.CLOW                                       11660
C      L14=ROM.LE.R2                                           11670
C-----                                                        11680
C      ZONE A1                                                 11690
C      IF(.NOT.(L1.AND.L2))GOTO40                               11700
C      IF(YESACC)ACC=ACC+STCASN                                11710
C      ACS=ACS+STCASN                                         11720
C-----                                                        11730
C      ZONE A0                                                 11740
C      40 IF(.NOT.(L3.AND.L4.AND.L5))GOTO50                    11750
C      IF(YESACC)ACC=ACC+STCASN                                11760
C      ACS=ACS+STCASN                                         11770
C-----                                                        11780
C      ZONE B0                                                 11790
C      50 IF(.NOT.(L6.AND.L7.AND.L8.AND.L9))GOTO60            11800
C      IF(YESACC)ACC=ACC+SCASTN                                11810
C      ACS=ACS+SCASTN*STSTNU                                   11820
C-----                                                        11830
C      ZONE B1                                                 11840
C      60 IF(.NOT.(L10.AND.L11.AND.L5))GOTO70                  11850
C      IF(YESACC)ACC=ACC+SCASTN                                11860
C      ACS=ACS+SCASTN*STSTNU                                   11870
C-----                                                        11880
C      ZONE C                                                 11890
C      70 IF(.NOT.(L12.AND.L13.AND.L14.AND.L8))GOTO80         11900

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                IF (YESACC) ACC=ACC+SCASTE
                ACS=ACS+SCASTE*EXP(-STS*TENU)
80 CONTINUE
   ACS=ACS*FAK
   ACC=ACC*FAK
   IF (NOACC) ACC=1.
   GOTU110
C----- RETURN STATE FOR NO ABSORPTION
90 ASS=1.
   ACC=1.
   ACS=1.
   GOTU110

C
C *****
C * FLAT PLATE ABSORPTION TERMS *
C * CTHMPH = COS(2THETA-PHI) *
C * CTHPPH = COS(2THETA+PHI) *
C * CPTTMP= COS(PHI)*COS(2THETA-PHI) *
C * CPTTPP= COS(PHI)*COS(2THETA+PHI) *
C * CPMTMP= COS(PHI)-COS(2THETA-PHI) *
C * CPMTTP= COS(PHI)-COS(2THETA+PHI) *
C *****
C
100 CTH=COS(TTHET)
    CPHI=COS(DELTA)
C==== CHECK FOR SYMMETRIC SCATTERING CASE IN TRANSMISSION =====
    TPHI=2.*PHI
    IF ((TPHI.LE.TTHET+.01).OR.(TPHI.GE.TTHET-.01)).AND.TRANS)GOTO140
    CTHMPH=COS(TTHET-DELTA)
    CTHPPH=COS(TTHET+DELTA)
    CPTTMP=CPHI*CTHMPH
    CPTTPP=CPHI*CTHPPH
    CPMTMP=CPHI-CTHMPH
    CPMTTP=CPHI-CTHPPH

C
C----- SAMPLE TERMS FOR AS -----
    R1ST5=R1*STS
    TM1=-R1ST5/CPHI
    TM2=-R1ST5/CTHMPH
    TM3=-R1ST5*((1./CPHI)-(1./CTHPPH))

C
C----- CAN TERMS FOR AC -----
C----- THICKNESS OF CAN WALL *STC -----
    R2MR1C=(R2-R1)*STC*.5
    TN1=-R2MR1C/CPHI
    TN2=-R2MR1C/CTHMPH
    TN3=-R2MR1C*((1./CPHI)-(1./CTHPPH))

C
C----- A1 AND A2 TERMS IN TRANSMISSION -----
C----- DIVIDE BY ZERO CHECK -----
    L15=THET.LE..785398
    L16=THET.GT..785398
    L15=TRANS
    L16=.NOT.TRANS
    L17=R1ST5.NE.0.
    L19=R2MR1C.NE.0.
    L20=1ROUTE.EQ.1
    L21=1ROUTE.EQ.2
    IF(L15.AND.L17)A2=CPTTMP*(EXP(TM1)-EXP(TM2))/(R1ST5*CPMTMP)
    IF(L15.AND.L19.AND.L2 )
    *
    * A1=CPTTMP*(EXP(TN1)-EXP(TN2))/(R2MR1C*CPMTMP)

C----- A1 AND A2 TERMS IN REFLECTION -----
    IF(L16.AND.L17)A2=CPTTPP*(EXP(TM3)-1.)/(R1ST5*CPMTTP)
    IF(L16.AND.L19.AND.L20)
    *
    * A1=CPTTPP*(EXP(TN3)-1.)/(R2MR1C*CPMTTP)

C
C *****
C * SET UP ASS, ACS & ACC TERMS FROM A1 AND A2 *
C * IN TRANSMISSION *
C * ASS=A1**2*A2 *
C * ACC=1. *
C * ACS=A2 *
C * IN REFLECTION *
C * ASS=A1**2*A2 *
C * ACC=(1.+A1**2)*.5 *
C * ACS=(1.+(A1*A2)**2)*.5 *
C *****
C
    IF(.NOT.L19)A1=1.
    IF(.NOT.L17)A2=1.

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12660
12670
12680
12690
12700

```

```

IF(L21)A1=1. 12710
IF(L15)ASS=A1*A1*A2 12720
IF(L15)ACC=1. 12730
IF(L15)ACS=A2 12740
IF(L16)ASS=A1*A1*A2 12750
IF(L16)ACC=(1.+A1*A1)*.5 12760
IF(L16)ACS=(1.+A1*A1*A2*A2)*.5 12770
C----- DIVIDE BY ZERO PATCH ----- 12780
IF(.NOT.L17)ASS=1. 12790
IF(.NOT.L19)ACC=1. 12800
IF(L21)ACC=1. 12810
IF(L21)ACS=1. 12820
C----- RESET EVERYTHING ----- 12830
110 DO 130 K=1,20 12840
R(K)=1. 12850
DO 120 J=1,60 12860
AB(J,K)=1. 12870
SI(J,K)=0. 12880
AS(J,K)=0. 12890
NU(J,K)=0. 12900
ENU(J,K)=1. 12910
120 CONTINUE 12920
130 CONTINUE 12930
RETURN 12940
C==== SYMMETRIC SCATTERING CASE ===== 12950
140 A2=EXP(-R1*STS/CPH1) 12960
A1=EXP(-(R2-R1)*STC*.5/CPH1) 12970
IF(STC.EQ.0.)A1=1. 12980
IF(STS.EQ.0.)A2=1. 12990
ASS=A1*A1*A2 13000
ACC=1. 13010
ACS=A2 13020
GOTO110 13030
END 13040
SUBROUTINE DEADT(R,A,ICHNL,NDEAD,RPULSE,NCTRS,INC,DEAD,RMC,KI) 13050
C
C----- APPLIES DEADTIME CORRECTIONS AND CORRECTS FOR MONITOR COUNTS -----
C----- R : CORRECTION FACTOR ARRAY -----
C----- A : DATA ARRAY -----
C----- ICHNL : NUMBER OF CHANNELS IN ARRAY -----
C----- NDEAD : NUMBER OF DEAD CHANNELS -----
C----- RPULSE : NUMBER OF MACHINE PULSES FIRED -----
C----- NCTRS : NUMBER OF DETECTORS USED (UNNECESSARY WHEN USING MK2
C----- SPECTROMETER ,AS ALL DETECTORS HAVE INDIVIDUAL BUFFERS) -----
C----- INC : CURRENT COUNTER NUMBER -----
C----- DEAD : LOGICAL VARIABLE DESCRIBING DEAD TIME SWITCH -----
C----- RMC : MONITOR COUNT ARRAY -----
C----- KI : SAMPLE TYPE (1,2,3,4) SAMPLE,CAN,VANADIUM OR BACKGROUND -----
C
REAL A(ICHNL),R(ICHNL),RPULSE(3,4),RMC(8,4) 13060
LOGICAL DEAD 13070
DO 10 I=1,ICHNL 13080
R(I)=1. 13090
C----- DIVIDE BY MONITORS ONLY IF NO DEADTIME CORRECTION ----- 13100
IF(.NOT.DEAD.OR.NDEAD.EQ.0.OR.RPULSE(INC,KI).EQ.0.)GOTO40 13110
CALL FRAME 13120
CALL MAP(0.,FLOAT(ICHNL),0.95,1.1) 13130
CALL WINDOW(0.,FLOAT(ICHNL),0.95,1.1) 13140
CALL SCALES 13150
CALL BORDER 13160
CALL POSITN(FLOAT(ICHNL/3),1.07) 13170
CALL TYPECS('DEAD TIME CORRECTION FACTOR',28) 13180
CALL POSITN(0.,1.) 13190
DO 30 I=1,ICHNL 13200
SUM=0. 13210
N1=I-NDEAD 13220
N2=I-1 13230
IF(N1.LE.0)N1=1 13240
DO 20 J=N1,N2 13250
SUM=SUM+A(J) 13260
R(I)=1./(1.-SUM/RPULSE(INC,KI)) 13270
30 CALL JOIN(FLOAT(I),R(I)) 13280
C----- CORRECT FOR MONITOR COUNTS ----- 13290
40 DO 50 K=1,ICHNL 13300
50 A(K)=A(K)*R(K)*100000./RMC(INC,KI) 13310
RETURN 13320
END 13330
SUBROUTINE READ(S,E,IMAX) 13340
C----- READ IN SCATTERING CROSS SECTION V ENERGY ARRAYS 13350
C----- ROUTINE RETURNS VALUES OF CROSS SECTION,ENERGY & # OF POINTS 13360

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REAL S(1),E(1) 13340
DO 20 I=1,40 13350
READ(5,10)E(I),S(I),K 13360
10 FORMAT(2F10.0,I1,59X) 13370
C-----K IS SENTINEL FOR END OF DATA 13380
IF(K.EQ.1)GO TO 41 13390
20 CONTINUE 13100
WRITE(6,30) 13110
30 FORMAT('*** > THAN 40 SCATTERING CROSS SECTION VALUES IN MESH **') 13120
STOP 13130
40 IMAX=1 13140
RETURN 13150
END 13160
SUBROUTINE QBIN(TITLE,ICHNL,RID,CHAN,CA,TFP,NCTRS,T,SQ,D,W,Q,RSQ, 13110
* NC,EQUALQ) 13120
C
C----- PUTS DATA INTO EQUAL WIDTH Q-BINS -----
C----- TITLE : TITLE FOR GRAPHS ETC. -----
C----- ICHNL : NUMBER OF CHANNELS IN ARRAY -----
C----- RID : INITIAL DELAY -----
C----- CHAN: CHANNEL WIDTH IN MICROSECONDS -----
C----- CA : COUNTER ANGLE -----
C----- TFP : TOTAL FLIGHT PATH IN METRES -----
C----- NCTRS : NUMBER OF DETECTORS -----
C----- T : TIME OF FLIGHT ARRAY -----
C----- SQ : S(Q) ARRAY READ FROM SCRATCH DISC AS WRITTEN IN MAIN PROGRAM -----
C----- D : ARRAY FOR SPLINE FITTING ROUTINE -----
C----- W : ARRAY FOR SPLINE FITTING ROUTINE -----
C----- Q : Q-SCALE ARRAY -----
C----- RSQ : EQUAL Q-BIN DATA -----
C----- NC : COUNTER ON/OFF SWITCH FOR EACH DETECTOR POSITION -----
C----- EQUALQ: LOGICAL VARIABLE TO SWITCH ROUTINE ON/OFF -----
C
REAL T(2048),SQ(2048),Q(1200),RSQ(1200),D(2048),W(6144),CA(8), 13130
* TITLE(8),YMAX(8)/8*0./,QSTEP/.05/,SCALE/1./,XMIN(8)/8*0./ 13140
* ,XMAX(8)/8*0./,WIDTH(8)/8*.015/ 13150
INTEGER NC(8),IMAX(8),CHAN 13160
LOGICAL PUNCH/F/,PLOT/T/,EQUALQ 13170
NAMELIST/QEQUAL/ YMIN,YMAX,XMIN,XMAX,QSTEP,SCALE,PUNCH,PLOT,WIDTH 13180
C 13190
IF(.NOT.EQUALQ)GOTO170 13120
N=ICHNL-1 13110
C----- GRAPHS ----- 13120
CALL GHPEN(1) 13130
CALL FRAME 13140
CALL CTRMAG(15) 13150
CALL PLACE(20,20) 13160
CALL TYPECS('EQUAL-Q STEP OPTION',19) 13170
CALL PLACE(20,25) 13180
CALL TYPECS('MARK VI 16TH JUNE 1975',22) 13190
C 13200
C----- TIMING SEQUENCE ----- 13210
TBEG=ZAGZAS(DUMMY) 13220
C 13230
C----- Q-SCALE CONSTANT ----- 13240
CONQ=TFP*3175.5216 13250
WRITE(6,10) 13260
10 FORMAT(1H1,T10,'EQUAL Q-STEP PROGRAM MARK VII 4TH DECEMBER 1975') 13270
READ(5,QEQUAL) 13280
WRITE(13,QEQUAL) 13290
CSCALE=.1*SCALE 13300
HQSTEP=.5*QSTEP 13310
CQSTEP=.1*QSTEP 13320
C 13330
C----- TOP SCALE ----- 13340
DO 20 K1=1,ICHNL 13350
20 T(K1)=RID+FLOAT((K1-1)*CHAN) 13360
C 13370
C----- LOOP OVER ALL COUNTERS ----- 13380
DO 130 INC=1,NCTRS 13390
IF(INC(INC).EQ.0)GOTO130 13400
CON1=CONQ*SIN(CA(INC)) 13410
C 13420
C----- READ S(Q) OR DS/DW FROM SCRATCH DISC ----- 13430
READ(14'INC,ERR=150)INC(INC),(SQ(K1),K1=1,ICHNL) 13440
C 13450
C----- COMPUTE YMAX AND PRINT OUT HEADINGS ----- 13460
IFYMAX(INC).EQ.0.)YMAX(INC)=SCALE*3. 13470
WRITE(6,30)QSTEP,SCALE,YMAX(INC),INC,NC(INC),WIDTH(INC),XMAX(INC) 13480
30 FORMAT(/,T10,'Q-STEP IS ',F5.2,' RECIPROCAL ANGSTROMS', 13490

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*      /,T10,%SCALE FACTOR IS ',F5.3,                13550
*      /,T10,%YMAX IS ',F5.3,                        13510
*      /,T10,%COUNTER NUMBER ',I2,% NC=',I3,        13520
*      /,T10,%SMOOTHING WIDTH IS ',F5.4,            13530
*      /,T10,%MAXIMUM Q-VALUE IS ',F6.3)            13540
C
C==== FIT TO SPLINE=====
CALL T8.4A(N,T,SQ,D,W)                                13570
C==== COMPUTE EQUAL Q AND PLOT =====
QMX=CON1/T(1)                                          13590
QMN=CON1/T(ICHNL)                                     13600
IF(XMAX(INC).NE.0.)QMX=XMAX(INC)                      13610
IF(XMIN(INC).NE.0.)QMN=XMIN(INC)                     13620
IJ=-2                                                 13630
C==== LOOP OVER ALL Q-BINS =====
DO 50 J=1,1200                                        13640
Q(J)=FLOAT(J)*QSTEP                                  13650
RSQ(J)=0.                                             13660
IF(Q(J).LT.QMN)QDT050                                13670
IF(Q(J).GT.QMX)QDT060                                13680
QJM=Q(J)-QSTEP                                       13690
C==== SUM OVER WIDTH OF Q-BIN =====
DO 40 K=1,100                                        13710
QJM=QJM+QSTEP                                        13720
40 RSQ(J)=RSQ(J)+TGO1B(IJ,N,T,SQ,D,CON1/QJM)        13730
C==== APPLY SCALING FACTOR =====
RSQ(J)=RSQ(J)*CSCALE                                13740
50 CONTINUE                                           13750
60 IQMAX(INC)=J                                       13760
C
C==== SMOOTH WITH WIDTH FUNCTION PROPORTIONAL TO Q-RESOLUTION =====
RI=0.                                                 13770
MAX=IQMAX(INC)                                       13780
C==== CYCLE OVER EACH Q-VALUE =====
DO 80 K=1,MAX                                        13790
OMW=1.-WIDTH(INC)*Q(K)                               13800
OPW=1.+WIDTH(INC)*Q(K)                               13810
RI=RI+1.                                             13820
C==== UPPER AND LOWER ELEMENTS OF INTEGRATION =====
I1=INT(RI*OMW+.5)                                    13830
I2=INT(RI*OPW+.5)                                    13840
IF(I1.LE.1)I1=2                                     13850
IF(I2.LE.1)I2=2                                     13860
IF(I2.GT.MAX)I2=MAX                                  13870
C==== INTEGRATE =====
DO 70 J=I1,I2                                        13880
70 SUM=SUM+RSQ(J)                                    13890
C==== NORMALISE =====
80 D(K)=SUM/FLOAT(I2-I1+1)                            13900
DO 90 K=1,MAX                                        13910
90 RSQ(K)=D(K)                                       13920
C==== REST RSQ ARRAY TO REQUIRED VALUE =====
DO 100 K=1,2048                                     13930
100 RSQ(K)=0.                                        13940
C==== CLEAR D ARRAY =====
C
C==== PLOT GRAPHS =====
CALL FRAME                                           13950
CALL MAP(0.,QMX,1.,YMAX(INC))                        13960
CALL WINDOW(0.,QMX,0.,YMAX(INC))                    13970
CALL SCALES                                          13980
CALL BORDER                                          13990
C----- CAPTION -----
CALL CTRMAG(1)                                       14000
CALL PLACE(2,40)                                     14010
CALL CTRORI(1)                                       14020
CALL TYPECS('SM(Q)',5)                              14030
CALL CTRORI(0)                                       14040
CALL PLACE(20,2)                                     14050
CALL TYPECS(TITLE,72)                                14060
CALL TYPECS(' COUNTER ',9)                          14070
CALL TYPENI(INC)                                    14080
CALL CTRMAG(15)                                     14090
CALL PLACE(40,45)                                    14100
CALL TYPECS('Q RECIPROCAL ANGSTROMS',23)            14110
CALL CTRMAG(5)                                       14120
C
C----- LIST,PLOT,PUNCH AND WRITE EQUAL Q-STEP DATA TO DISC -----
CALL OJUNA(Q,RSQ,IQMAX(INC),IQMAX(INC)/6+1,4,6,'FF',%SM(Q) ',6) 14130
CALL PTPLOT(Q,RSQ,1,IQMAX(INC),43)                  14140

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```

11300 NOMAX=IOMAX(INC)
11310 IF(PUNCH)WRITE(7,11)((RSO(K2-(K1-1)),KI=1,8),K2,K2=1,NOMAX,8)
11320 WRITE(14,INC)RSQ
11330 TEND=ZALZAS(DUMMY)-TBEG
11340 WRITE(6,120)TEND
11350 FORMAT(8F9.3,18)
11360 110 FORMAT(11D,TIME SO FAR IS ,F10.5, SECONDS*)
11370 120 CONTINUE
11380
11390 C----- PLOT ALL COUNTERS ON ONE GRAPH -----
11400 FIND(14,1)
11410 CALL FRAME
11420 CALL SCALES
11430 CALL BORDER
11440 CALL CTMAG(6)
11450 DO 14, INC=1,NCTRS
11460 IF(INC(INC).EQ.0)GOTO140
11470 READ(14,INC)RSQ
11480 IF(INC.LI.NCTRS)FIND(14,INC+1)
11490 CALL PTPLOT(Q,RSQ,1,IOMAX(INC),INC)
11500 140 CONTINUE
11510 RETURN
11520 150 WRITE(6,150)
11530 160 FORMAT(11,DISC READ ERROR*)
11540 RETURN
11550 170 READ(5,REQUAL)
11560 WRITE(13,REQUAL)
11570 RETURN
11580 END

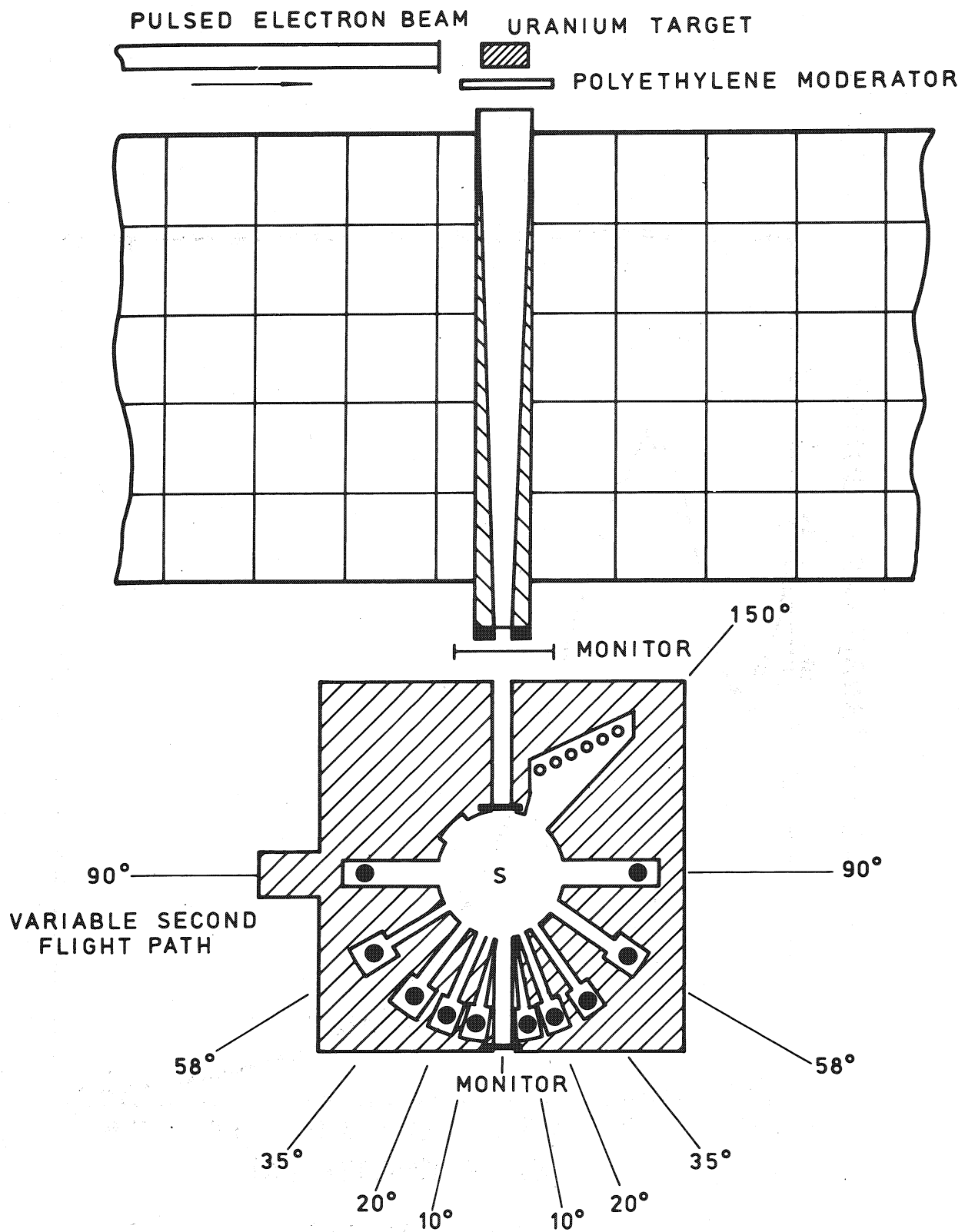
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Acknowledgements

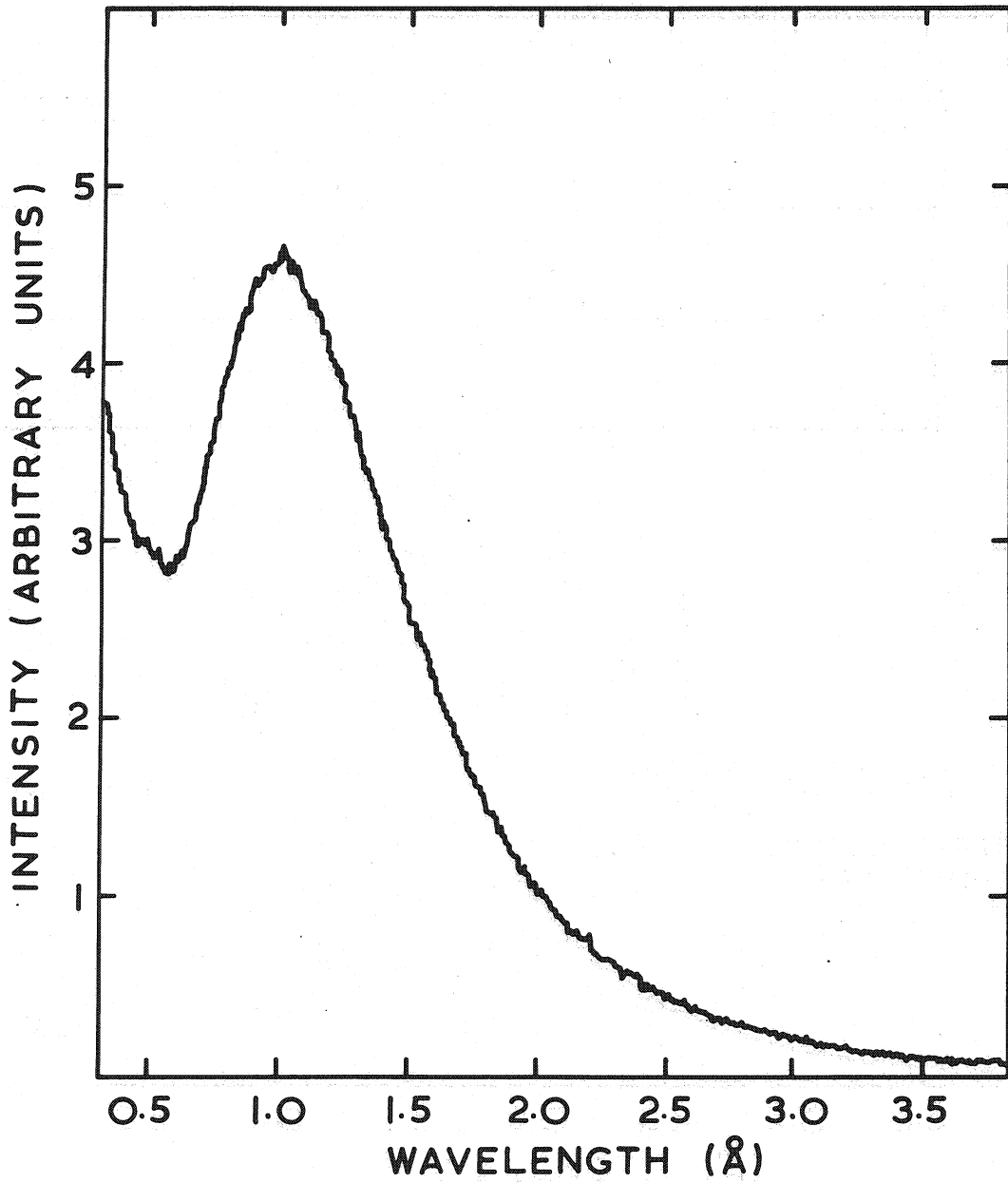
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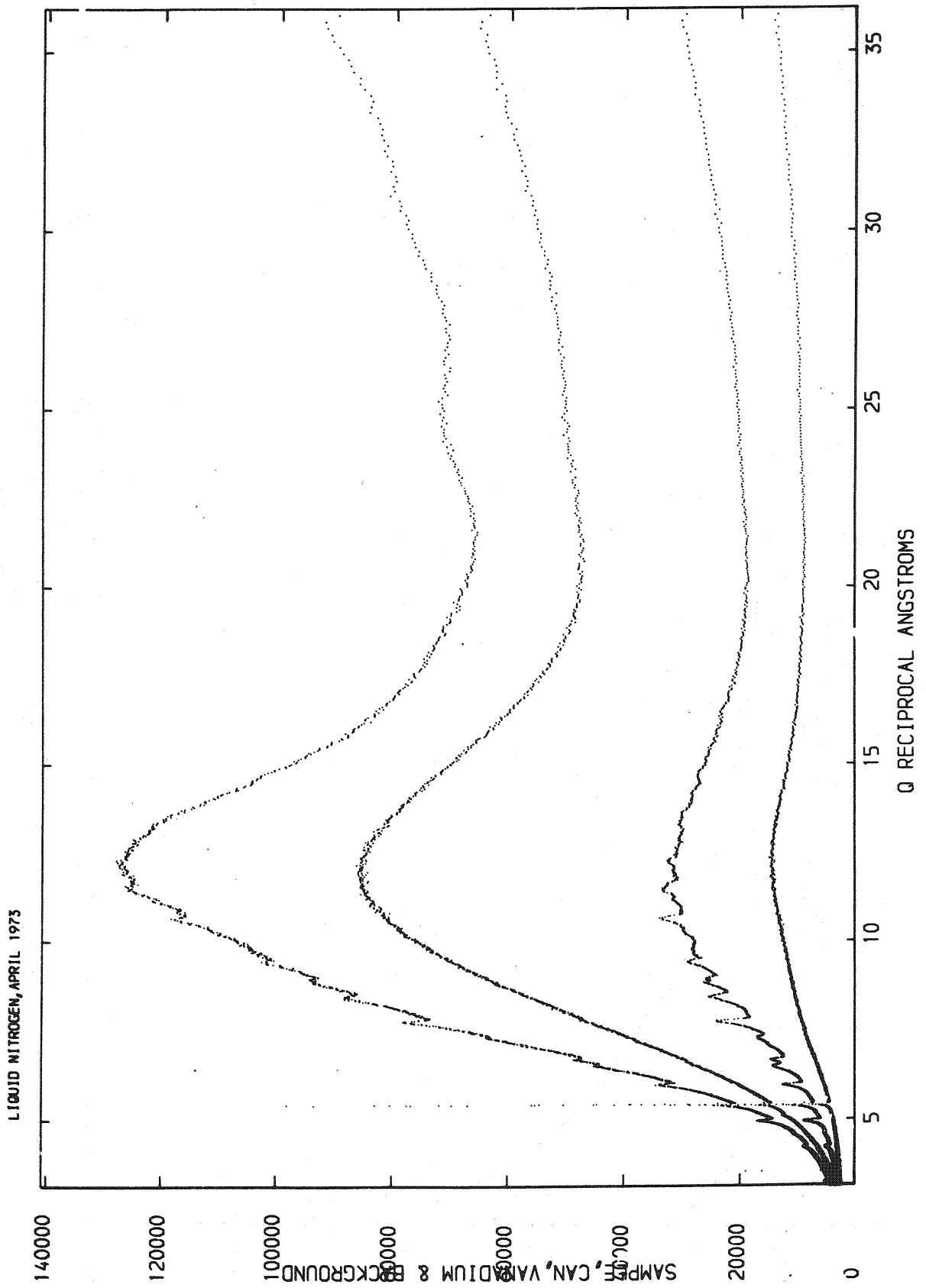
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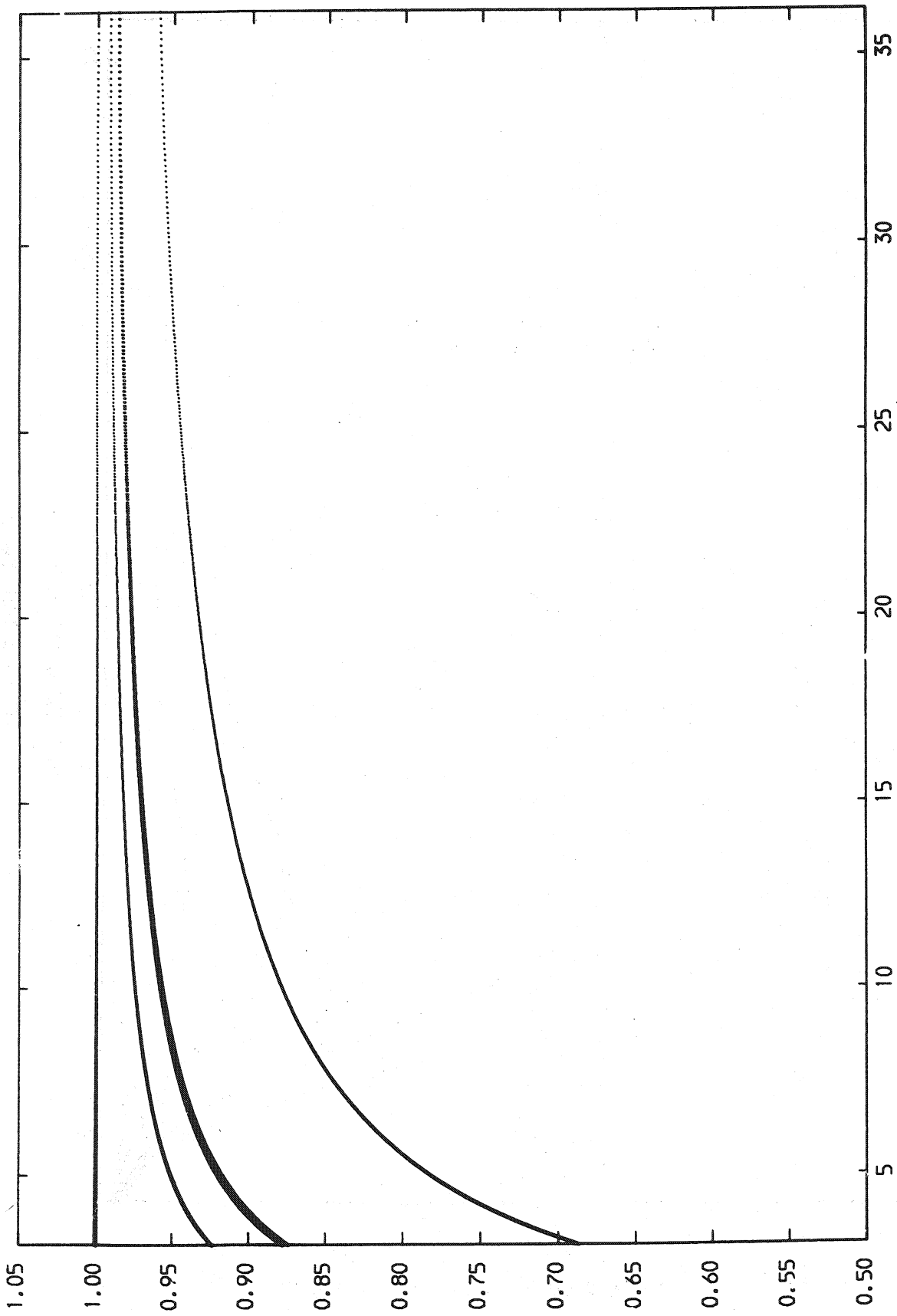
AERE - R 8121 Fig. 1



AERE - R 8121 Fig. 2
The energy distribution of the incident beam.



AERE - R 8121 Fig. 3
The input spectra for the program normalised for monitor counts.

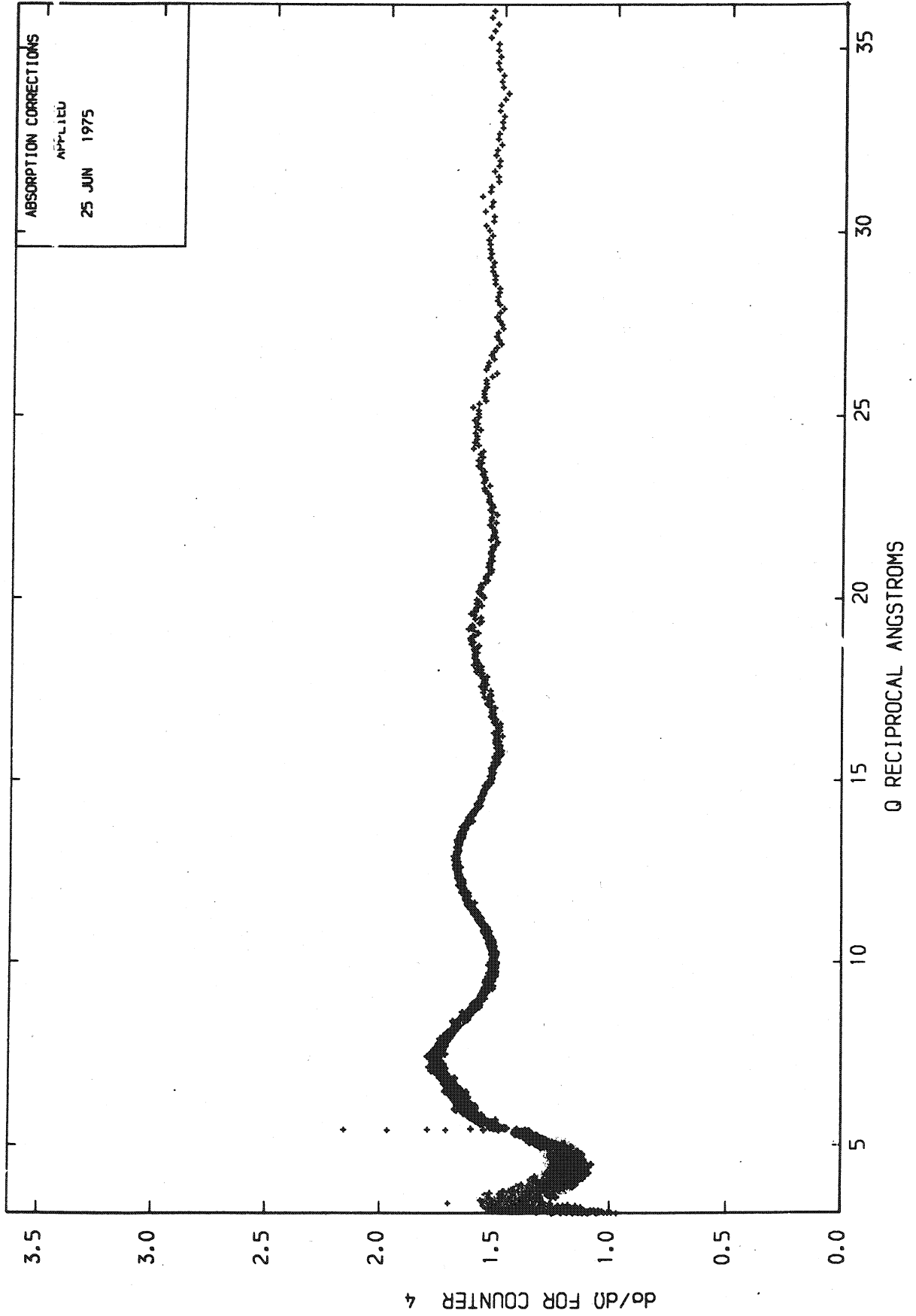


PAALMAN AND PINGS CORRECTION TERMS, COUNTER 4

AERE - R 8121 Fig. 4

The computed Paalman and Pings correction terms.

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AERE - R 8121 Fig. 5
 $d\sigma/d\Omega$ for liquid nitrogen as computed by the program ($\theta = 150^\circ$).