

Lecture HDG-2: Modelling and Simulating Accelerator Magnets



TECHNISCHE
UNIVERSITÄT
DARMSTADT

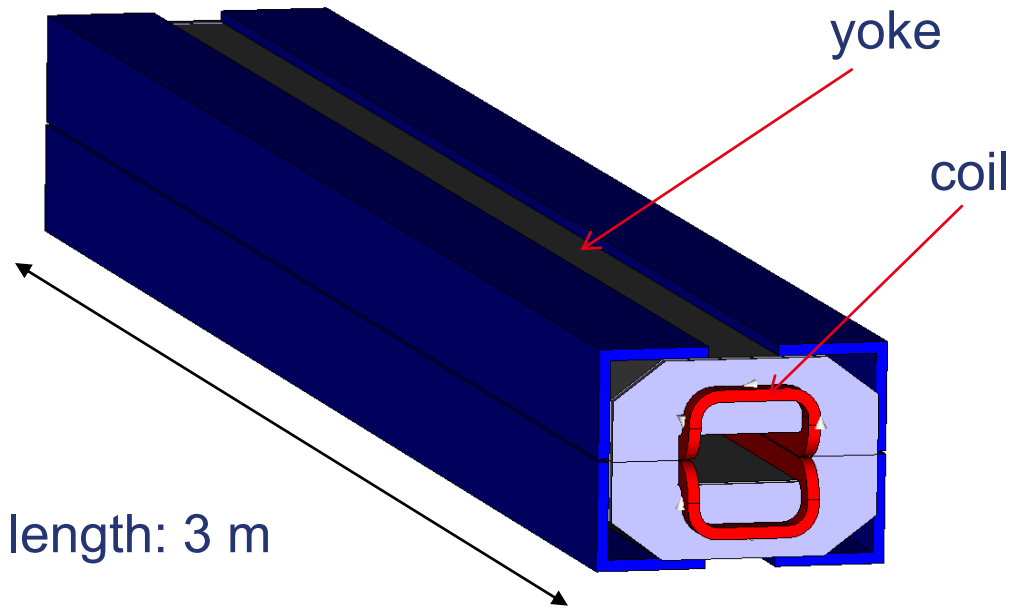
Prof. Dr.-Ing. Herbert De Gersem

CERN Accelerator School 2023

Sankt-Pölten, Austria, 20 November - 1 December 2023

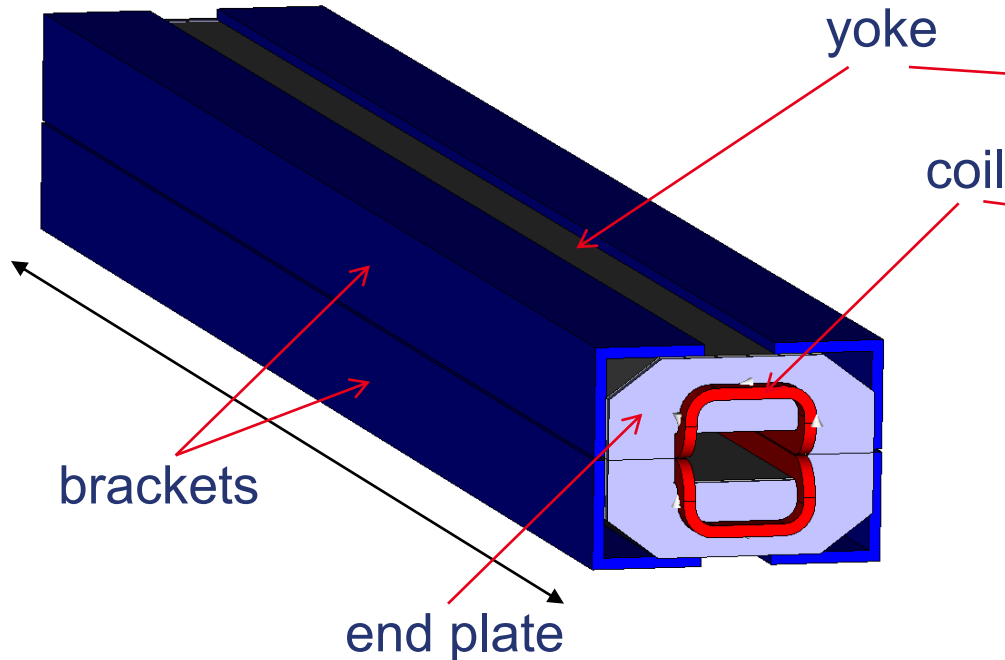


Example: accelerator magnet



comparably simple ?

Example: GSI-SIS-100 magnet



length: 3 m

SIS100 dipole (prototype)

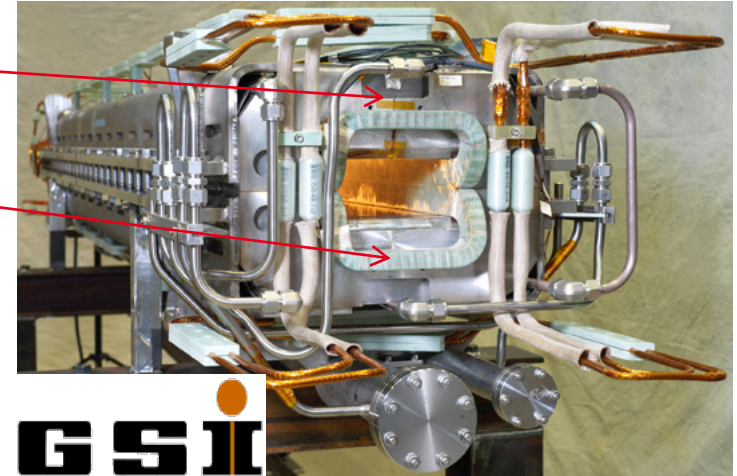
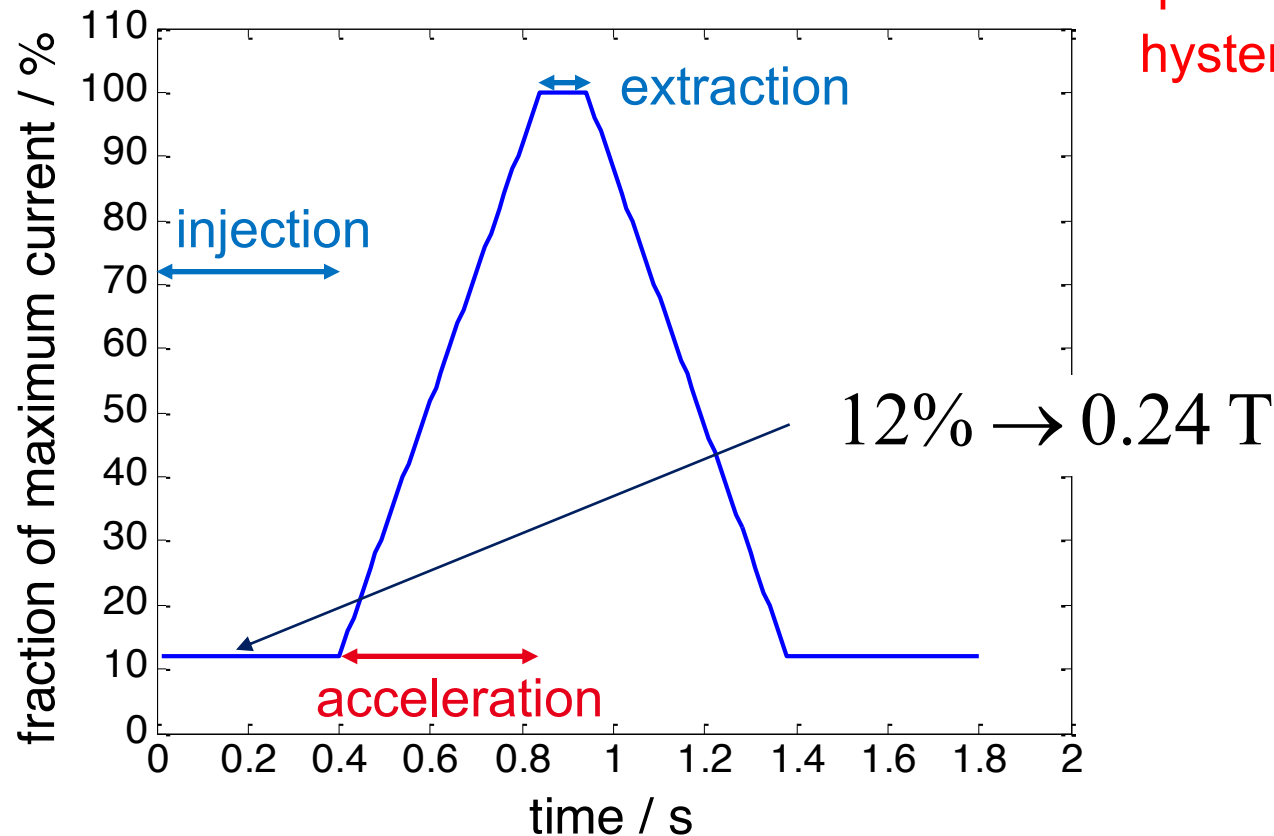


photo: J. Guse, GSI (www.gsi.de)

many geometric details
superconductive coils
helium cooling
mechanical deformation
radioactive hazards

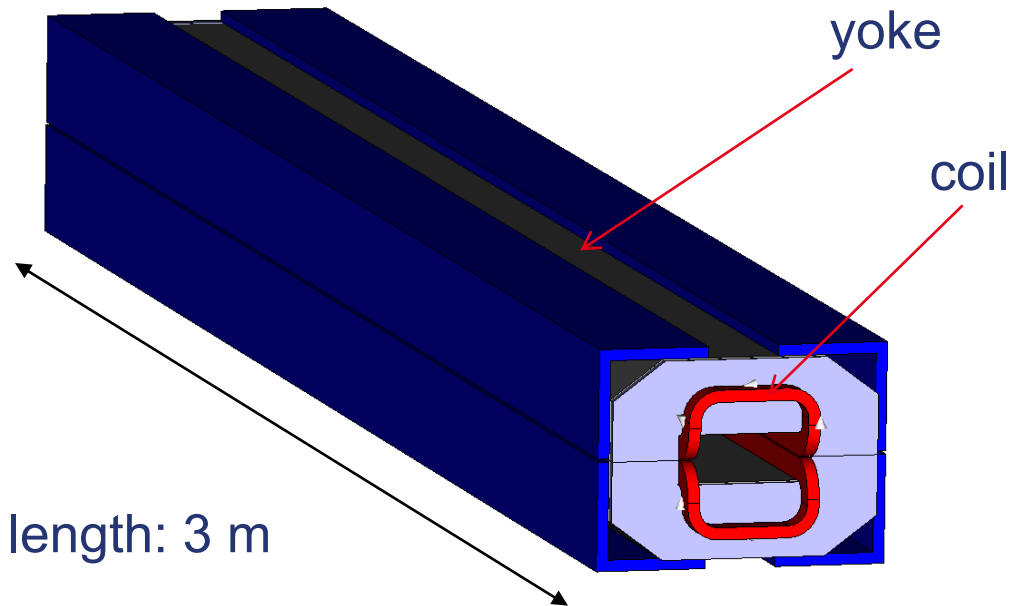
Example: GSI-SIS-100 magnet

excitation profile



eddy currents
quench of superconductors
hysteresis

Example: accelerator magnet



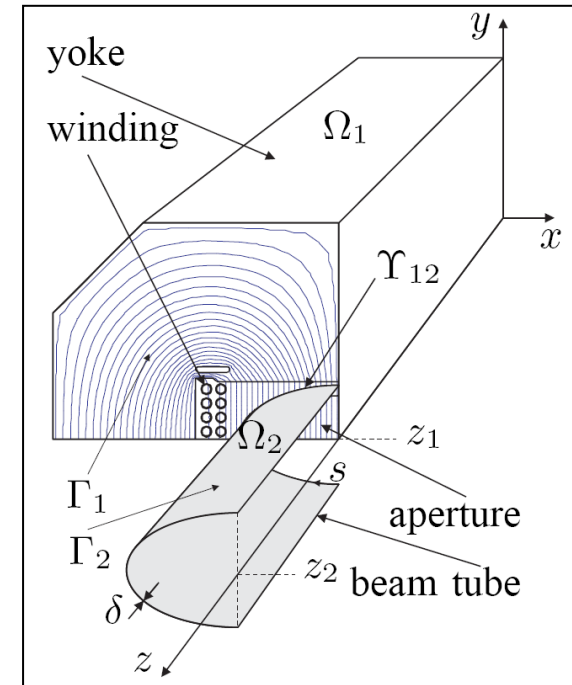
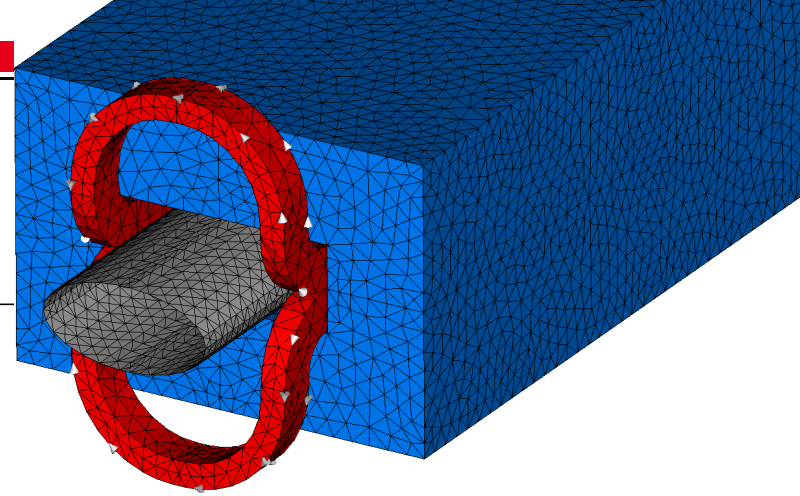
~~comparably simple ?~~



unexpected complexity !

Overview

- magnet simulation (standard 3D FE solver)
- challenges
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hybrid models
- stochastic models
- conclusions



Magnetoquasistatic formulation



differential equation:

$$\nabla \times \left(\nu \nabla \times \vec{A} \right) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

reluctivity
magnetic vector potential
conductivity
applied current density

Discretisation in space

differential equation:
$$\nabla \times (\nu \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

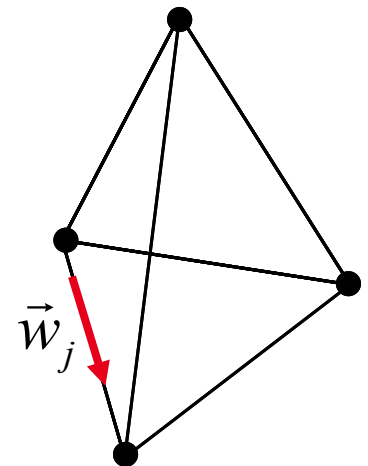
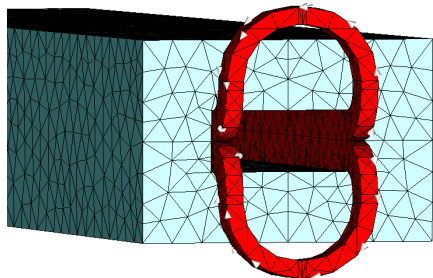
spatial discretisation



$$\vec{A} \approx \vec{A}_{\text{FE}} = \sum_j \hat{a}_j \vec{w}_j$$

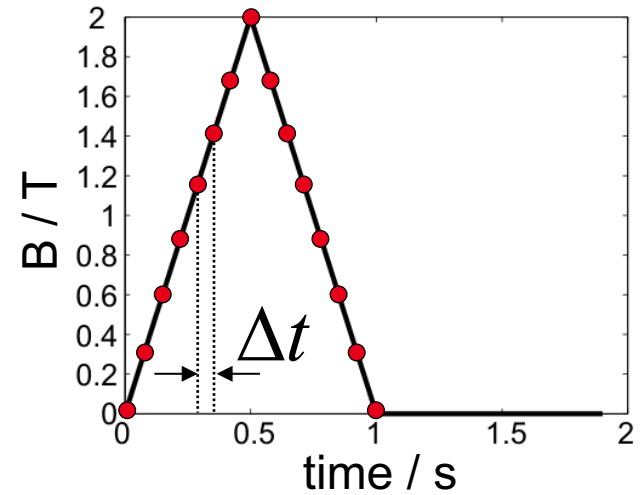
semi-discrete system:
$$\mathbf{K}_\nu \hat{\mathbf{a}} + \mathbf{M}_\sigma \frac{d\hat{\mathbf{a}}}{dt} = \hat{\mathbf{j}}_s$$

shape functions:
edge finite elements
(curl-conforming)



Discretisation in time

differential equation



spatial discretisation



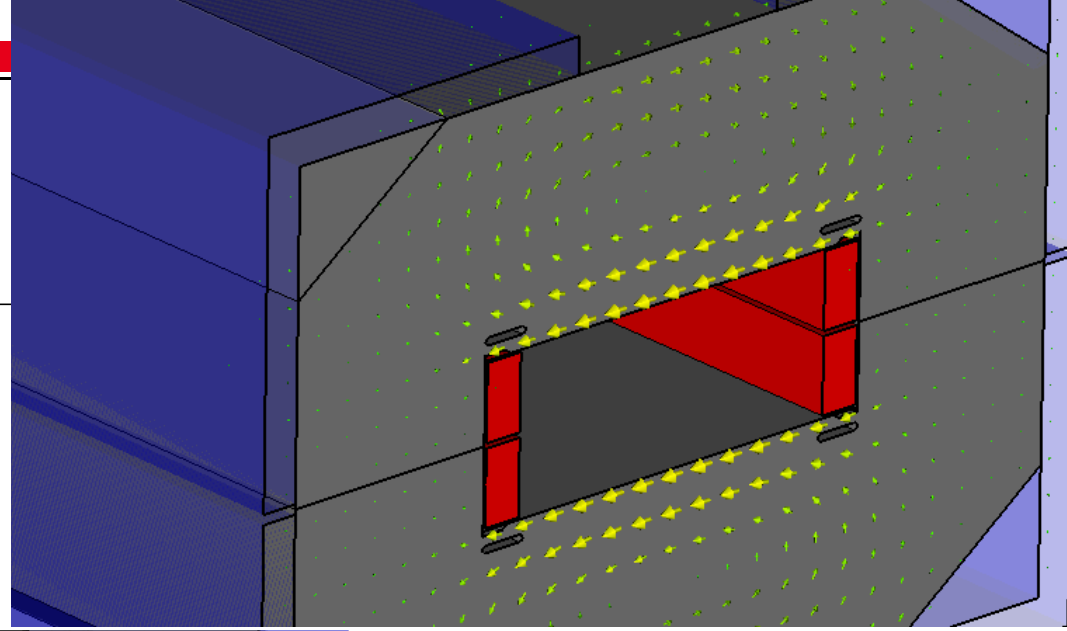
semi-discrete system: $\mathbf{K}_v \hat{\mathbf{a}} + \mathbf{M}_\sigma \frac{d\hat{\mathbf{a}}}{dt} = \hat{\mathbf{j}}_s$

temporal discretisation

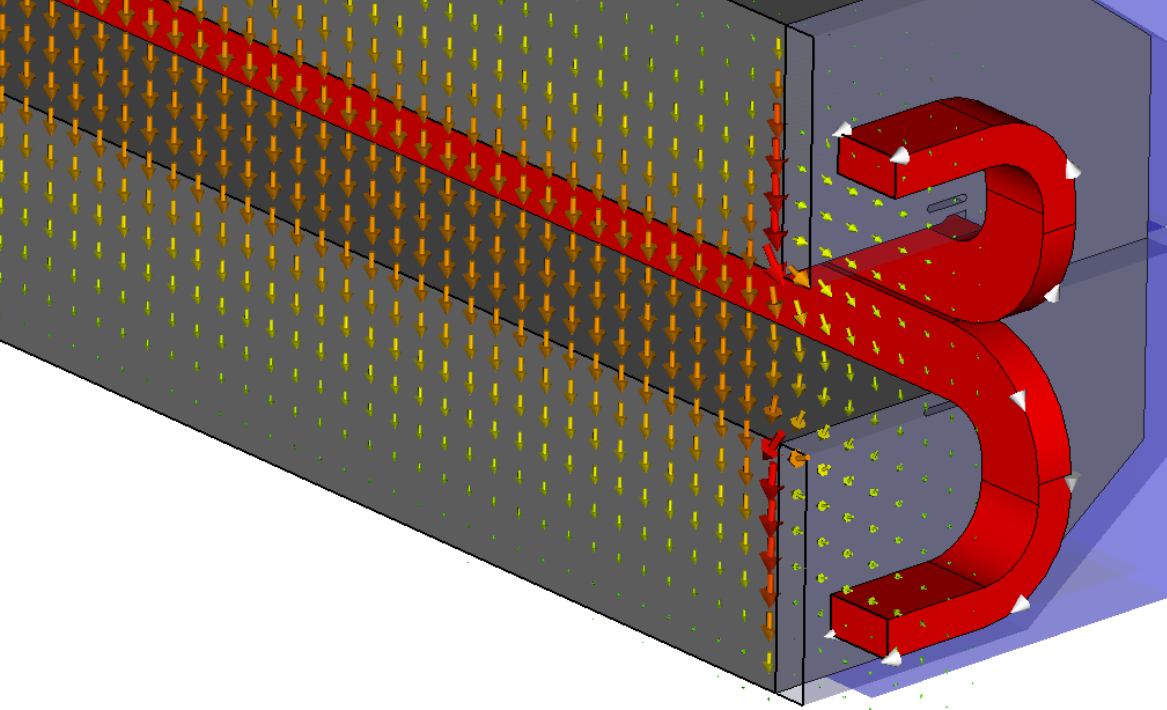


discrete system: $(\mathbf{K}_v + \alpha \mathbf{M}_\sigma) \hat{\mathbf{a}}_{k+1} = \text{RHS}$

Results



magnetic field



eddy currents
in the end plane

simulation by
CST EMStudio®

Electromagnetic field solvers

- commercial
or academic
or freeware
- low-frequency
and/or high-frequency
- circuit
and/or 2D fields
and/or 3D fields
- problem specific
or multi-purpose
- electromagnetic fields
and/or multi-physics
- cheap or expensive



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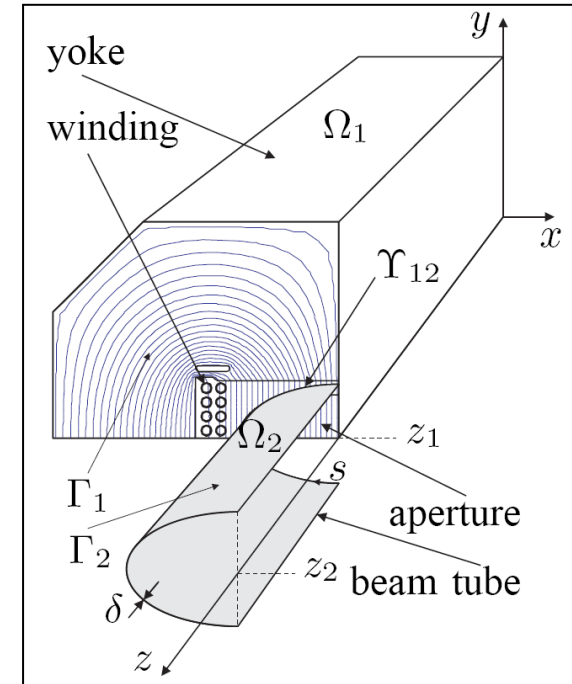
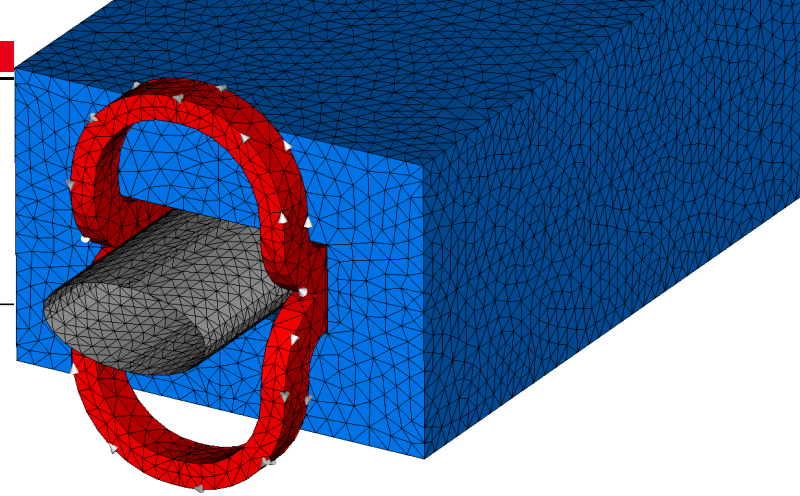
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Overview

- magnet simulation (standard 3D FE solver)
- **challenges**
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hybrid models
- stochastic models
- conclusions



Challenge 1: Detailed geometry

yoke

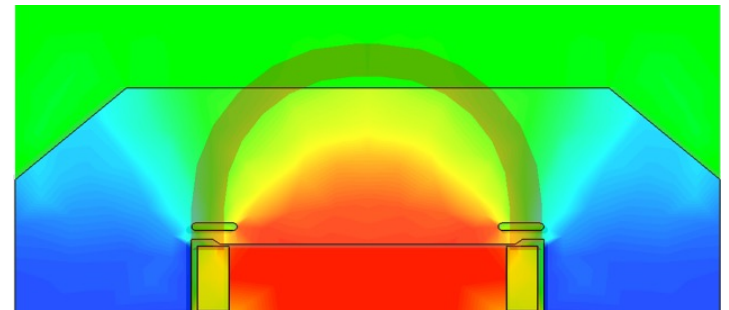
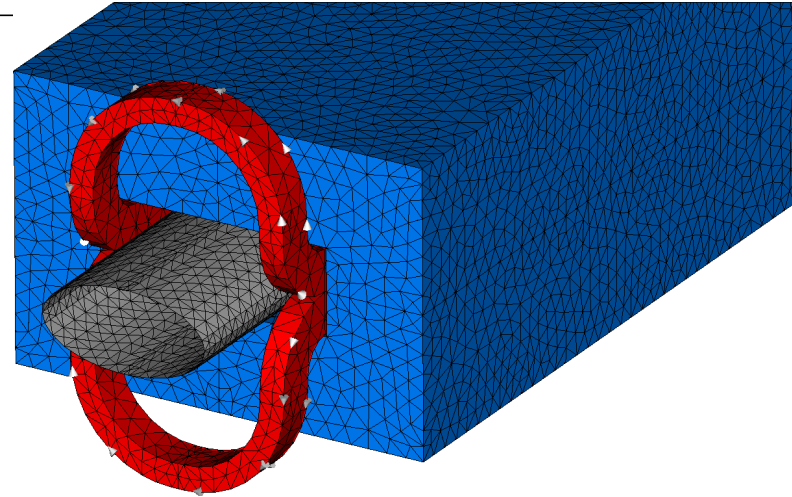
- length (meter)
vs. lamination thickness (mm)
- shimming, holes

beam tube

- < 1mm thick

end-winding parts

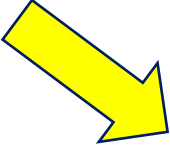
- determine the eddy currents
in the end plates



Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)


$$\bar{\bar{\nu}}(\vec{B}) = R^T \begin{bmatrix} \nu_{\text{rol}} & & \\ & \nu_{\text{trans}} & \\ & & \nu_{\text{trans}} \end{bmatrix} R$$

ν_{rol} reluctivity in the rolling direction

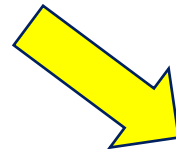
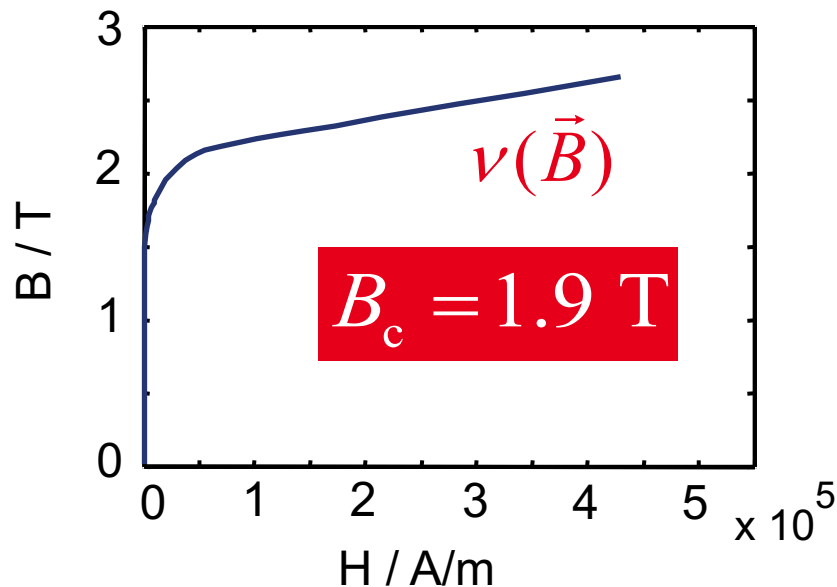
ν_{trans} reluctivity in the transversal direction

R local rotation matrix

Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)

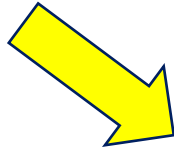


Newton method

Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)



Jiles-Atherton model

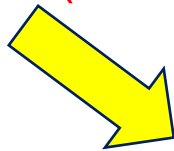
Preisach model

estimation of losses by Steinmetz-Bertotti

Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- **composite (lamination)**

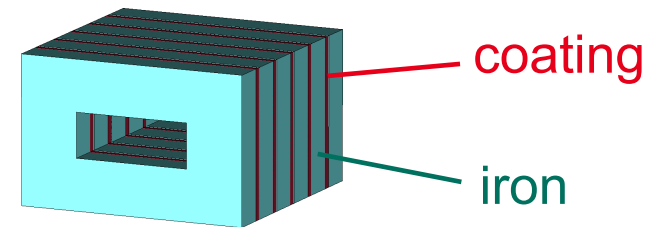


(simple) homogenisation
along lamination direction

perpendicular to laminates

stacking factor

$$\gamma_{st} \approx 0.95 \leq \sim 1$$



$$\frac{1}{\nu_{xy}} = \frac{\gamma_{st}}{\nu_{Fe}} + \frac{1 - \gamma_{st}}{\nu_0}$$

$$\nu_z = \gamma_{st} \nu_{Fe} + (1 - \gamma_{st}) \nu_0$$

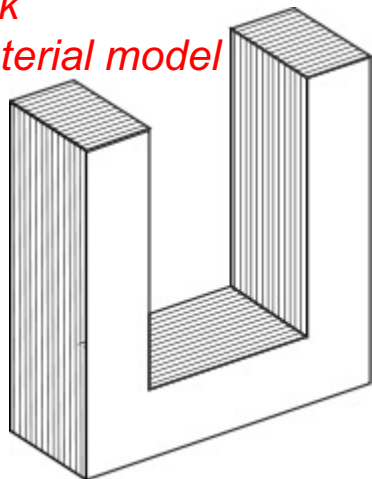
Challenge 2: Materials

yoke iron:

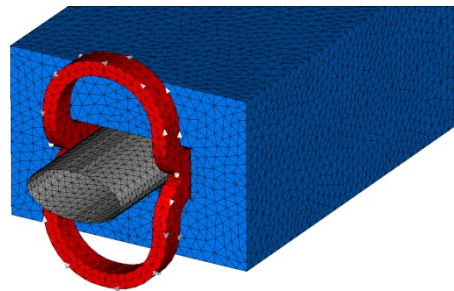
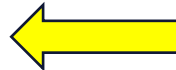
- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- **composite (lamination)**

multiscale simulation

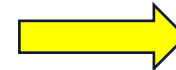
bulk material model



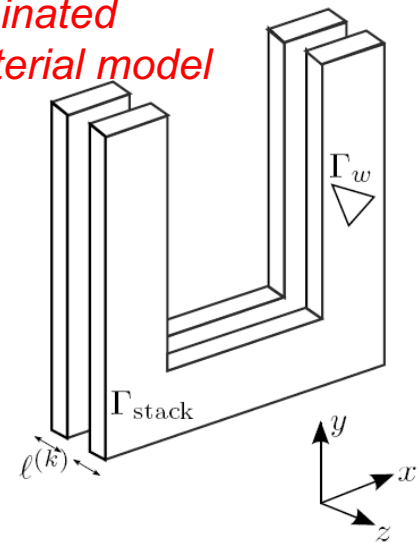
magnetic field



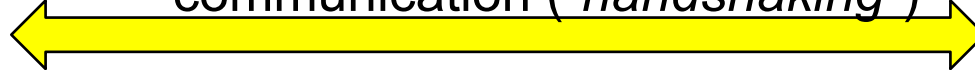
eddy currents



laminated material model



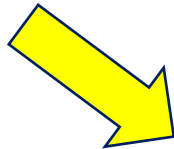
communication ("handshaking")



Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- composite (lamination)
- **variability**



stochastics, sensitivity

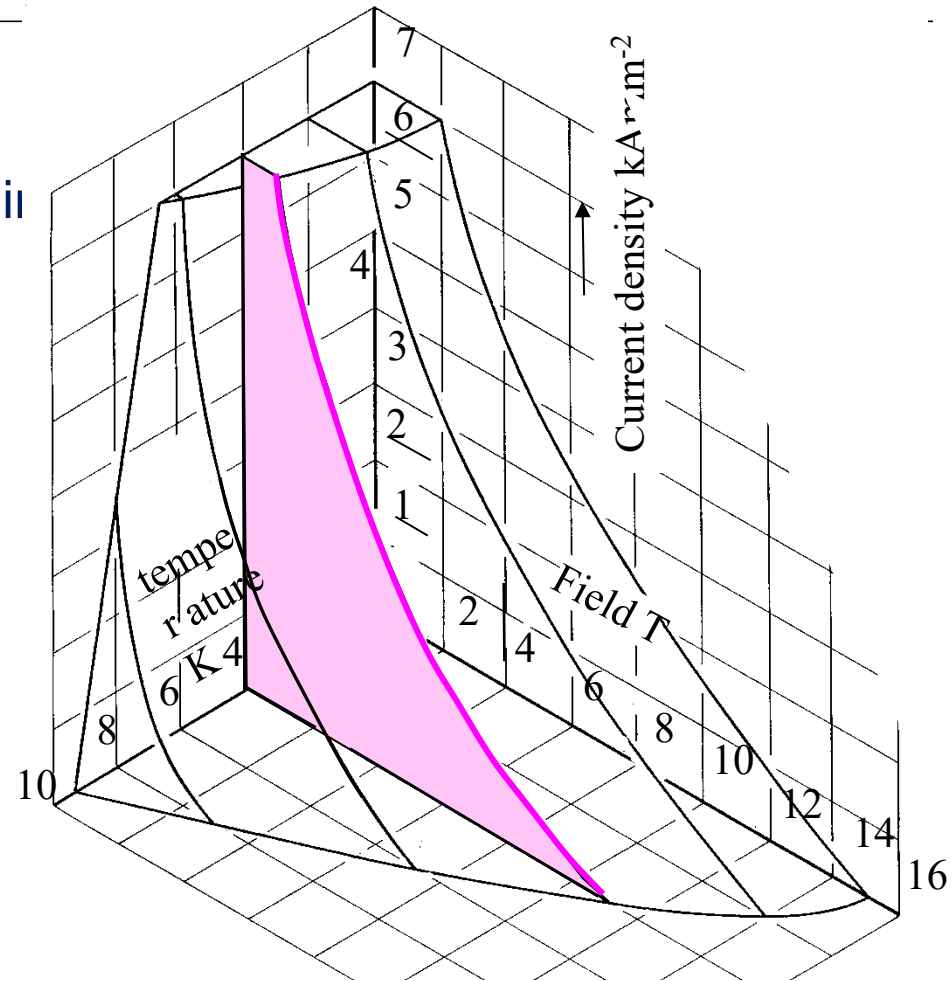
Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- composite (lamination)
- variability

superconductor:

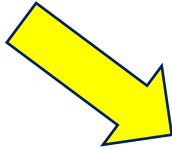
- critical current
- temperature
- magnetic field



Challenge 3: Transient phenomena

lamination

- hysteresis + remanence



Jiles-Atherton model

Preisach model

estimation of the remanence

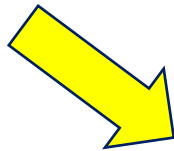
(based on data from material vendor)

Challenge 3: Transient phenomena

lamination

- hysteresis + remanence
- eddy currents

$$\nabla \times \left(\nu \nabla \times \vec{A} \right) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

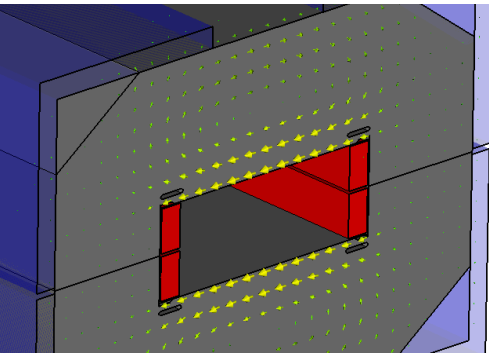


eddy current term

+ (simple) homogenisation $\sigma_{xy} = \gamma_{st} \sigma_{Fe}$

$$\sigma_z = 0$$

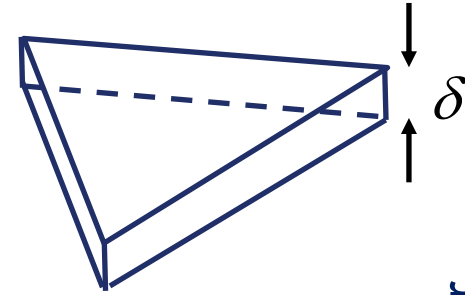
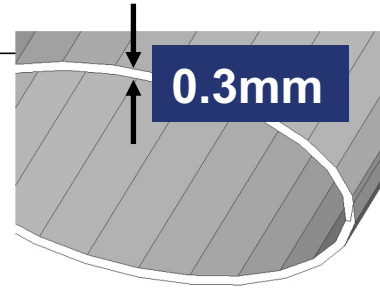
or + multi-scale model (hand-shaking)



Challenge 3: Transient phenomena

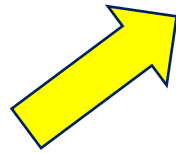
lamination

- hysteresis + remanence
- eddy currents



beam tube

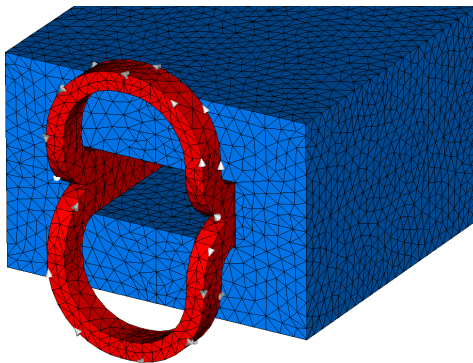
- eddy currents



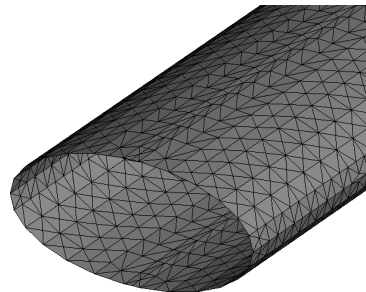
shell elements

additional matrix contributions \mathbf{K}_δ and \mathbf{M}_δ
assembling into system matrix by \mathbf{Q}

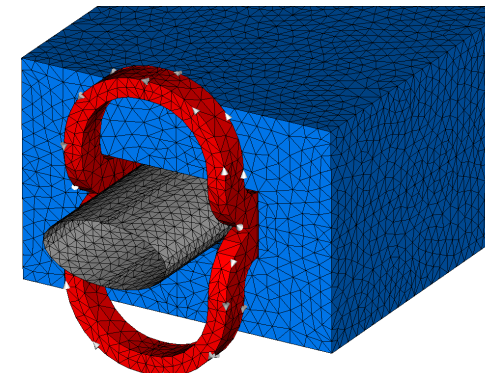
$$\mathbf{K}_V + \sigma \mathbf{M}_\sigma + \mathbf{Q}^T (\mathbf{K}_\delta + \alpha \mathbf{M}_\delta) \mathbf{Q} = \mathbf{K}_{\text{full}} + \alpha \mathbf{M}_{\text{full}}$$



+



=



Challenge 3: Transient phenomena

lamination

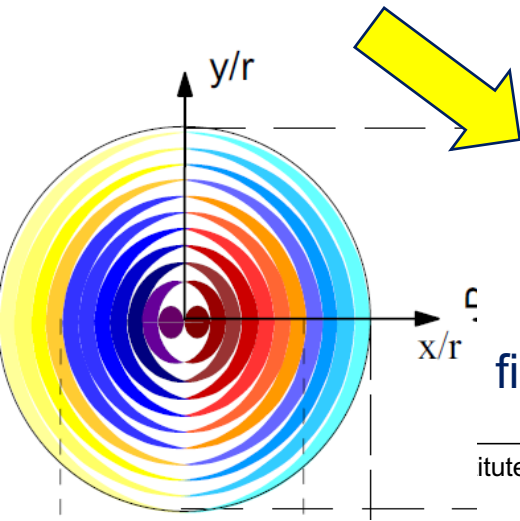
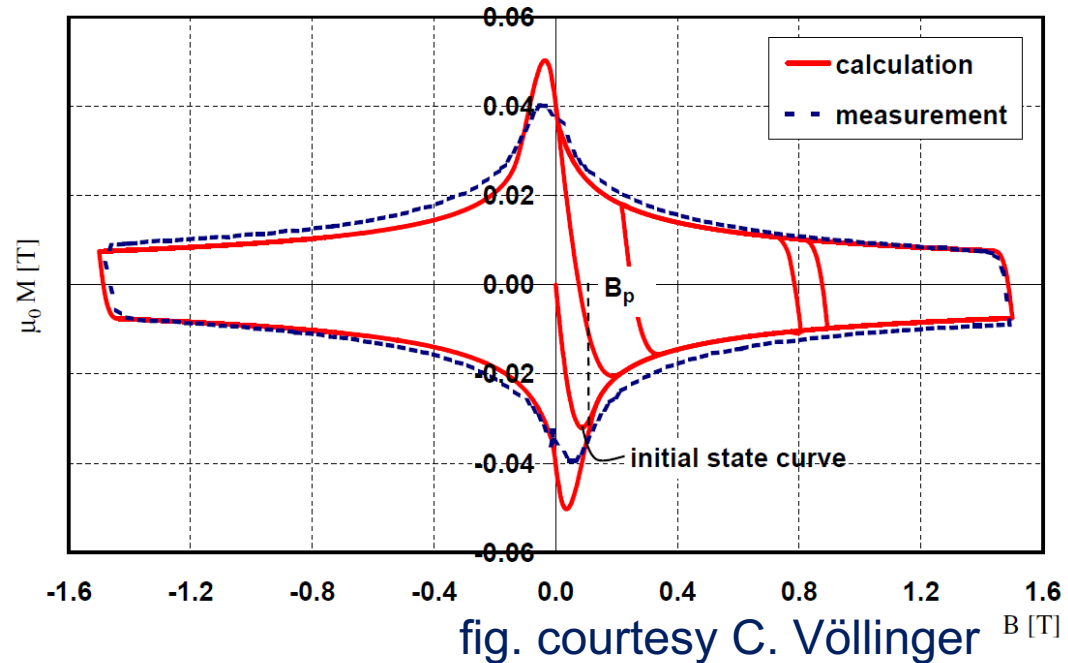
- hysteresis + remanence
- eddy currents

beam tube

- eddy currents

superconductor

- persistent currents



Bean model → magnetisation (Christine Völlinger)
implemented in ROXIE

fig. courtesy C. Völlinger

Challenge 3: Transient phenomena

lamination

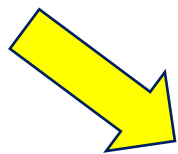
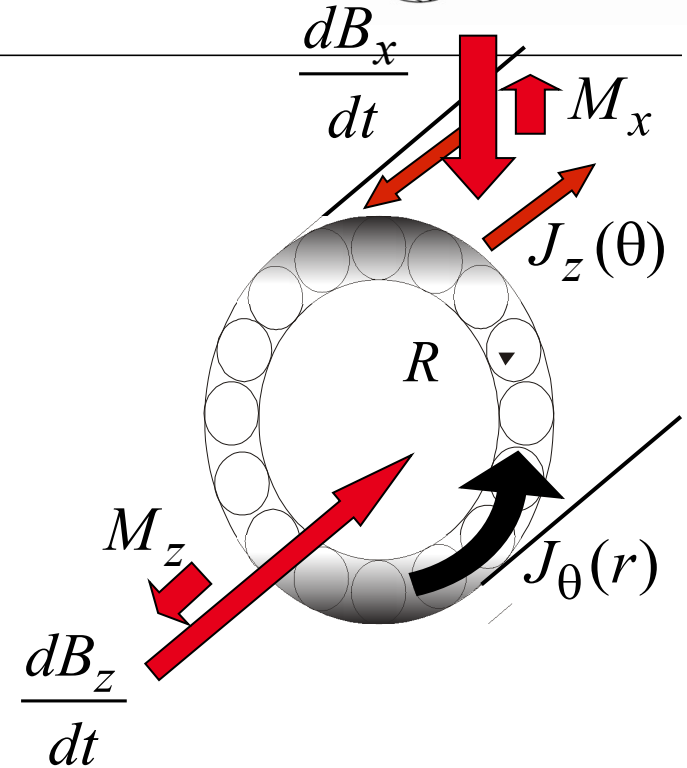
- hysteresis + remanence
- eddy currents

beam tube

- eddy currents

superconductor

- persistent currents
- coupling currents
- cable eddy currents



$$\nabla \times (\nu \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} + \nabla \times \left(\nu_0 \bar{\tau}_{cb} \nabla \times \frac{\partial \vec{A}}{\partial t} \right) = \vec{J}_s$$

additional magnetisation

Challenge 4: High accuracy requirements

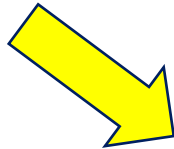


losses

- dimensioning of the cooling system
- hot spots
- quench

aperture field

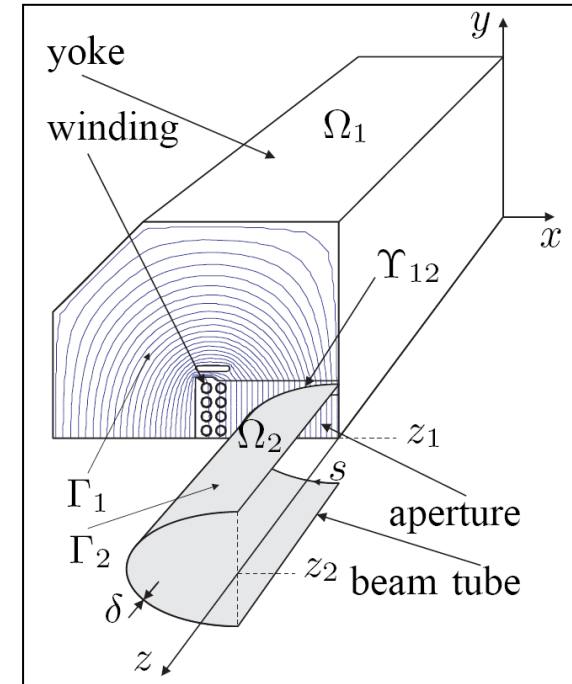
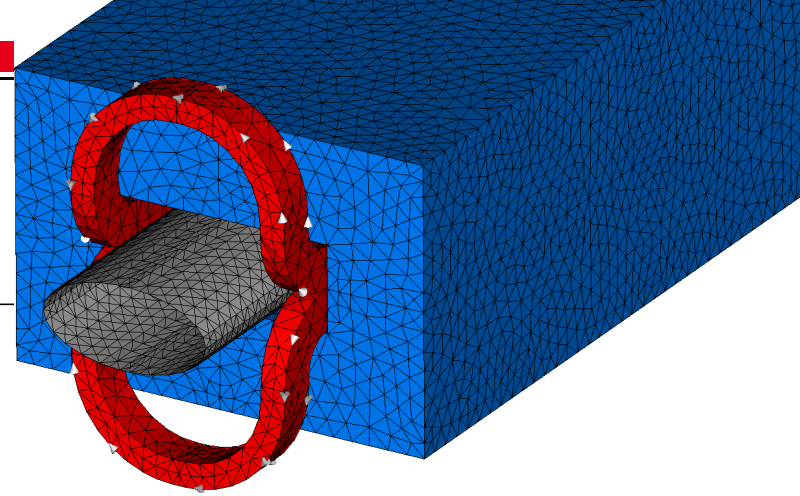
- multipoles during injection, ramping and extraction
- + influence of eddy currents



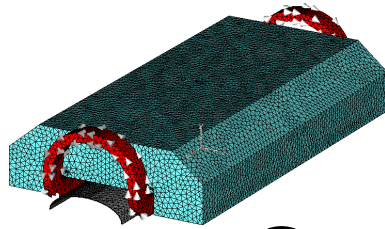
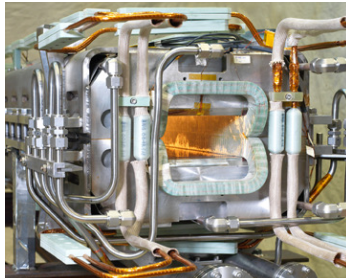
huge models
parallelisation, multi-core computers

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- stochastic models
- conclusions



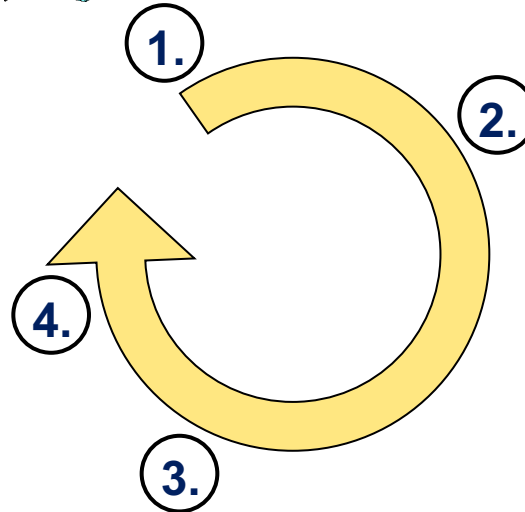
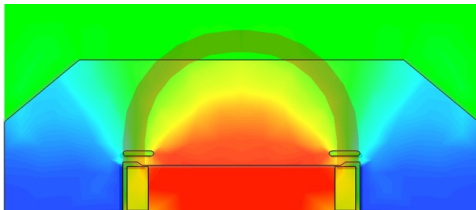
Dedicated Simulation Tool



CST Studio Suite®

- CAD modelling
- meshing

- visualisation



Matlab

- postprocessing
- visualisation

FEMSTER,
LLNL

TRILINOS,
Sandia Labs

own software

- FE assembly
(higher order FEs)
- transient solver
- nonlinear materials
- system solver

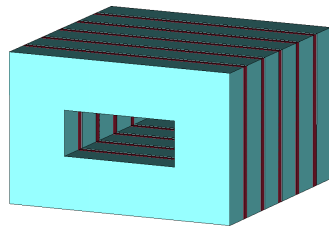
parallelisation

+ Stephan Koch, Jens Trommler

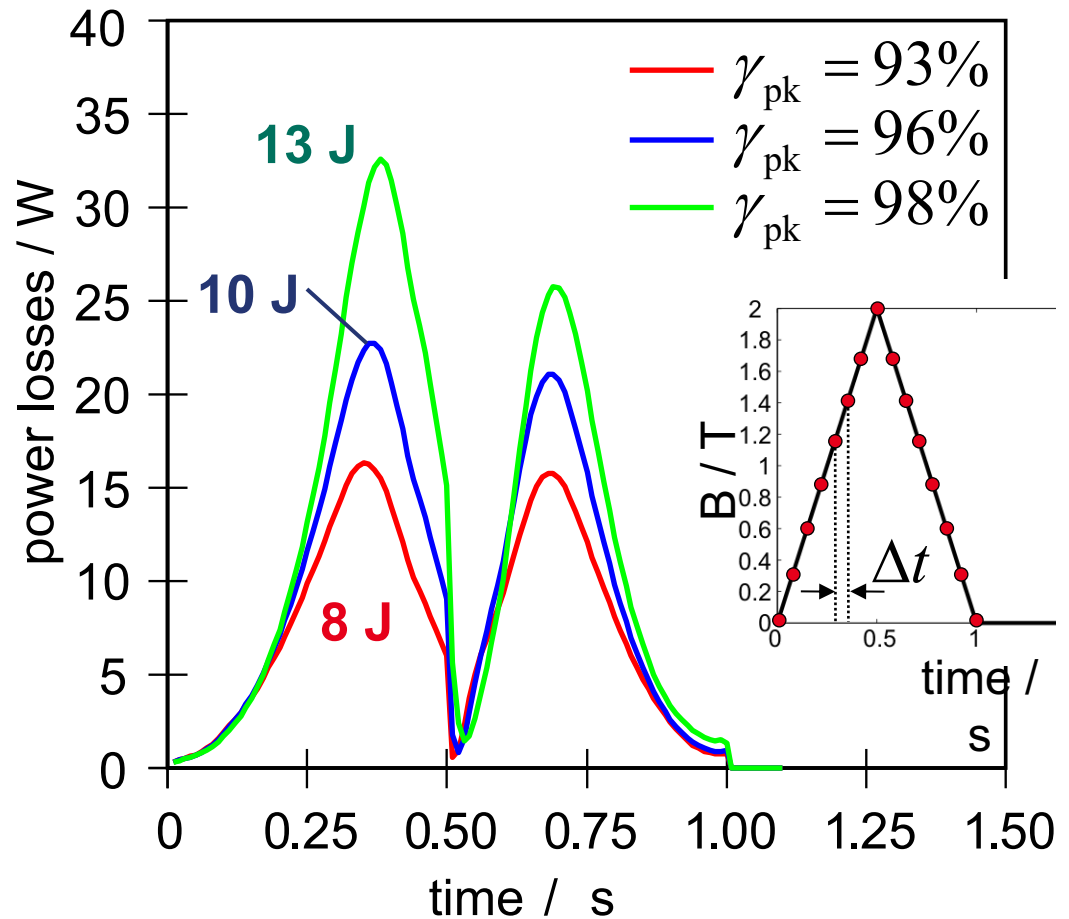
Results: Eddy-Current Losses

eddy-current losses
over one cycle

for different
stacking factors γ_{pk}



loss energy: $W = \int_0^T P dt$



+ Stephan Koch, Jens Trommler

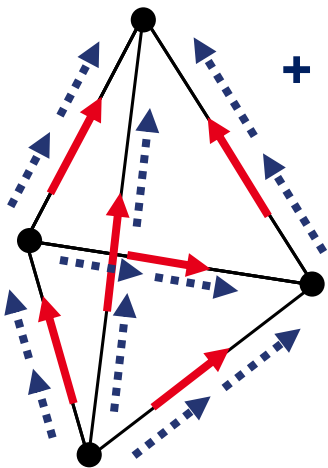
Results: Loss Energy

- discretization:
 - increase number of elements
 - increase order of approximation

$$\vec{A} \approx \vec{A}_{\text{FE}} = \sum_j a_j \vec{w}_j^{\text{tv}}$$

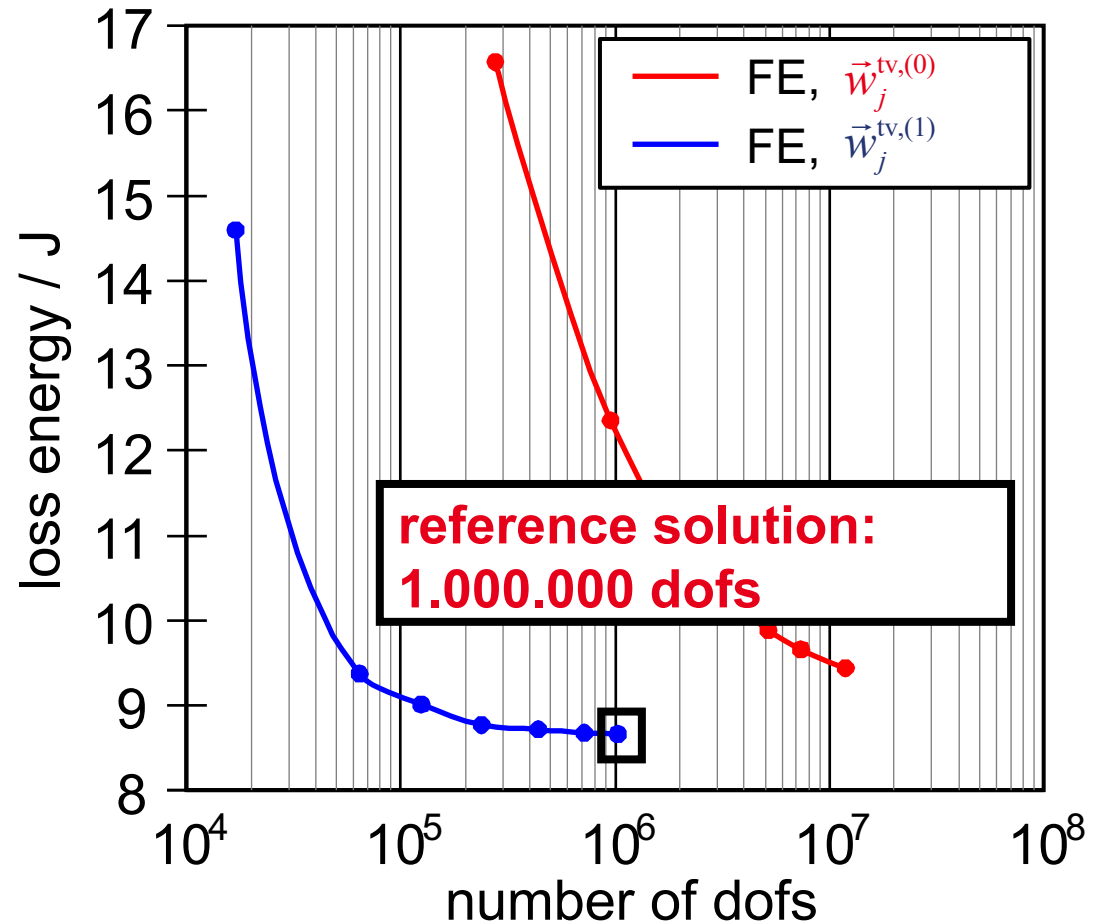
degrees of freedom:

+ 2 per face



$$\vec{w}_j^{\text{tv},(0)} \quad n_{\text{dof}} = 6$$

$$\vec{w}_j^{\text{tv},(1)} \quad n_{\text{dof}} = 20$$

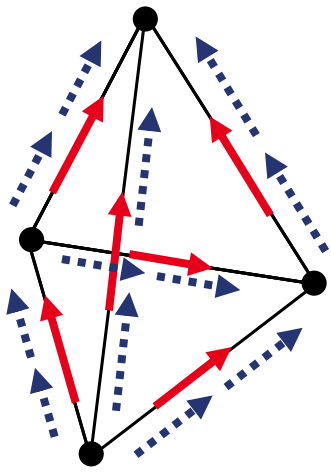


+ S. Koch, J. Trommler

Convergence: Loss Energy

- relative error with respect to reference solution

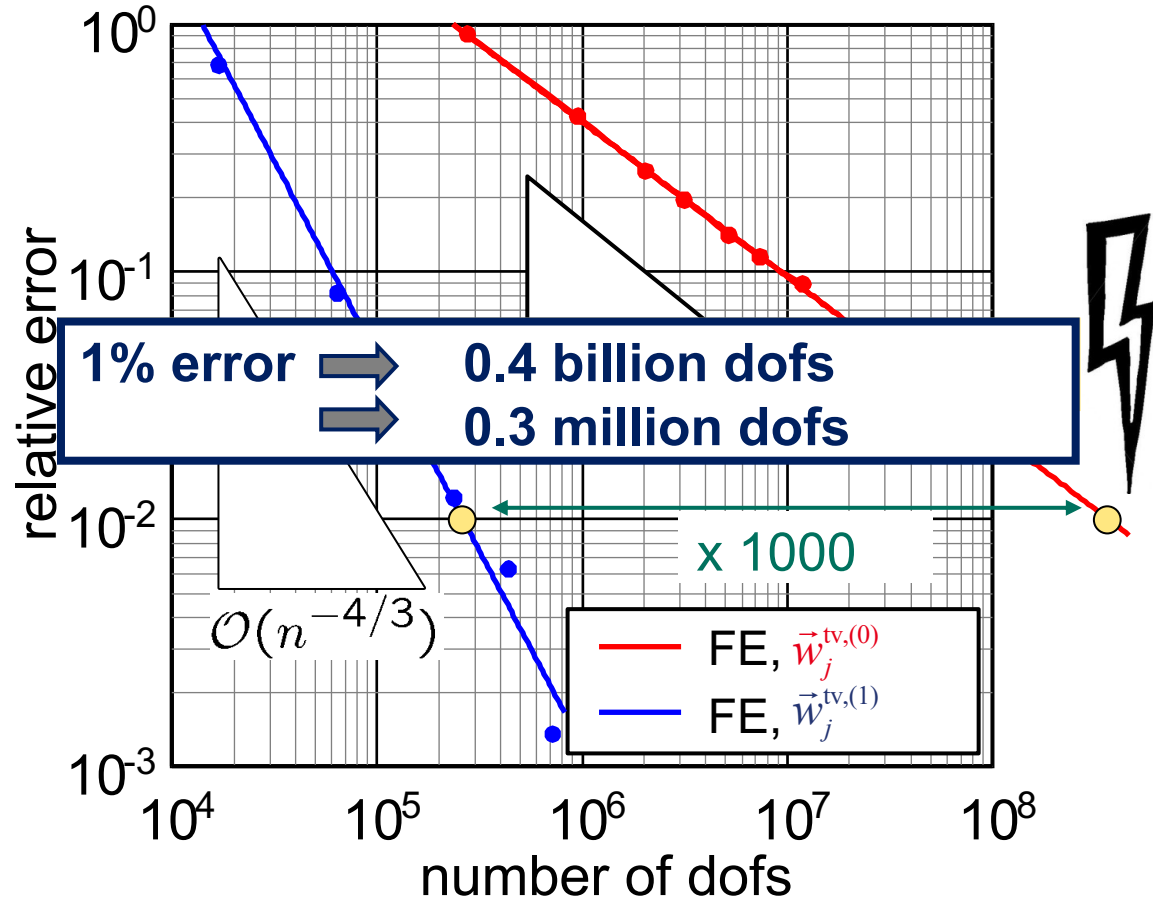
degrees of freedom:



+ 2 per face

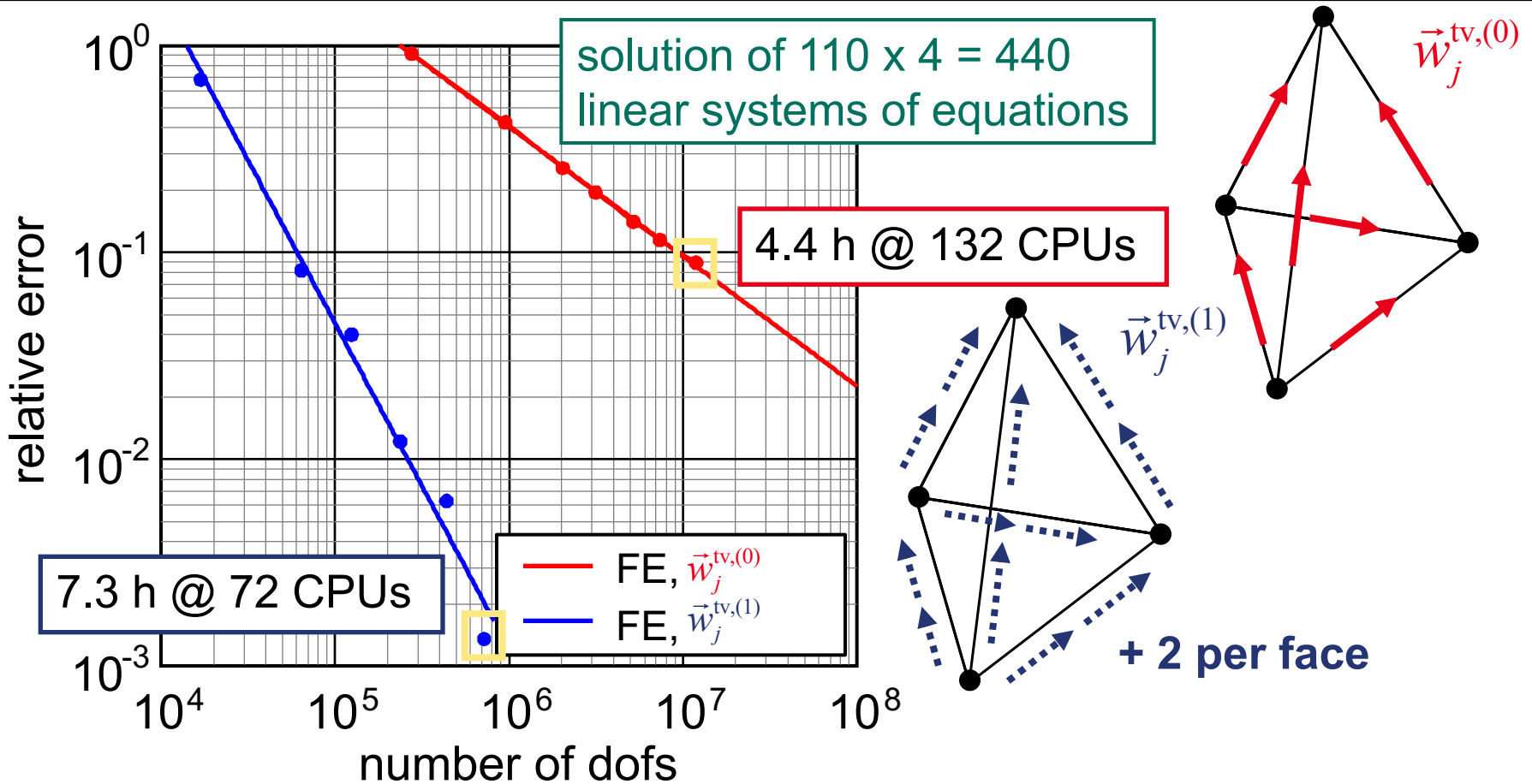
$$\vec{w}_j^{tv,(0)}$$

$$\vec{w}_j^{tv,(1)}$$



+ S. Koch, J. Trommler

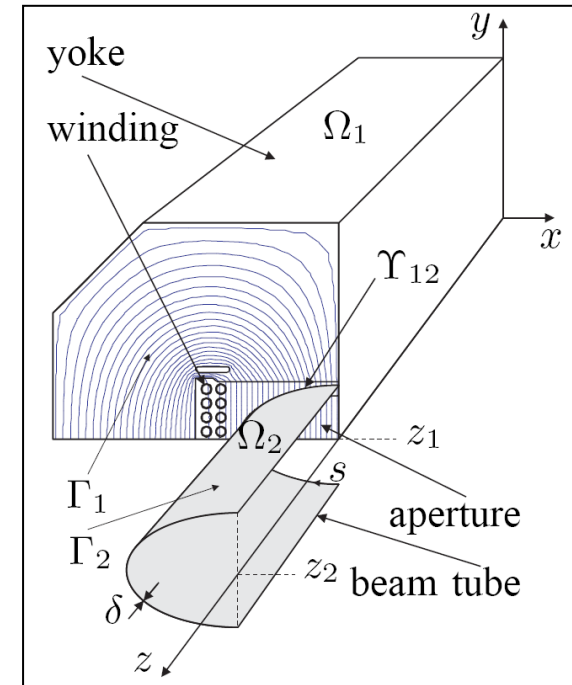
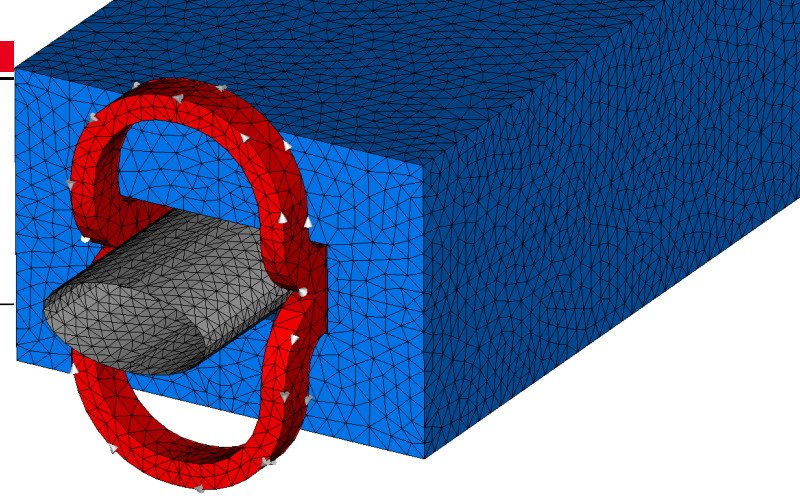
Comparison: Shape Functions



+ S. Koch, J. Trommler

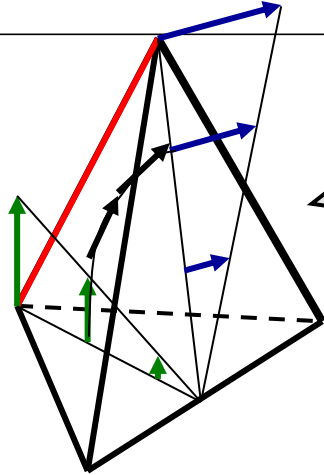
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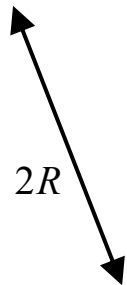


Hybrid discretisation

(edge)
finite
elements

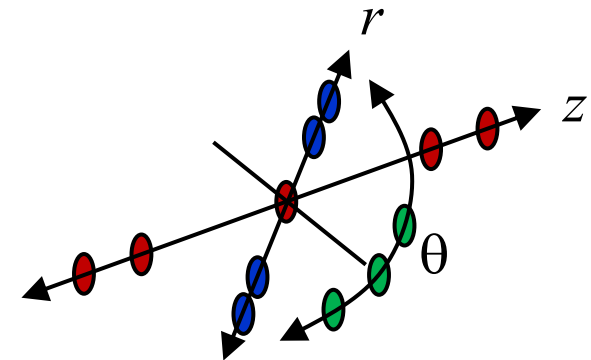
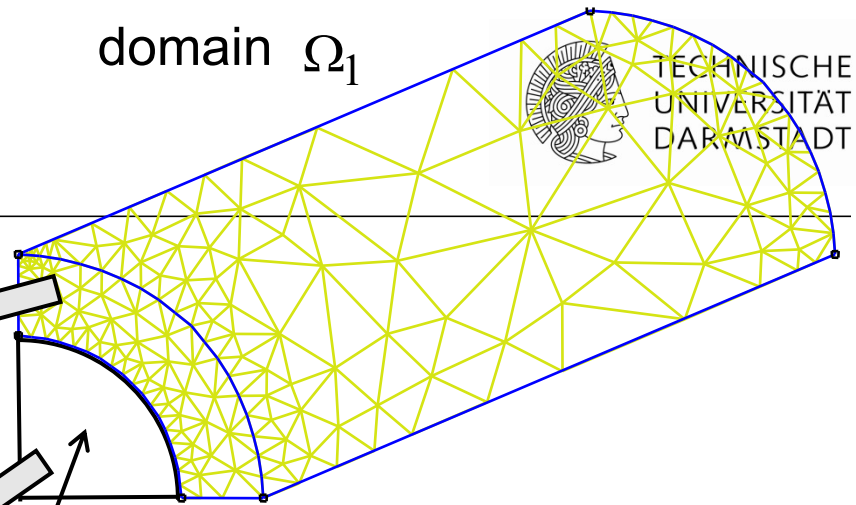


spectral
elements



domain Ω_1

domain Ω_2

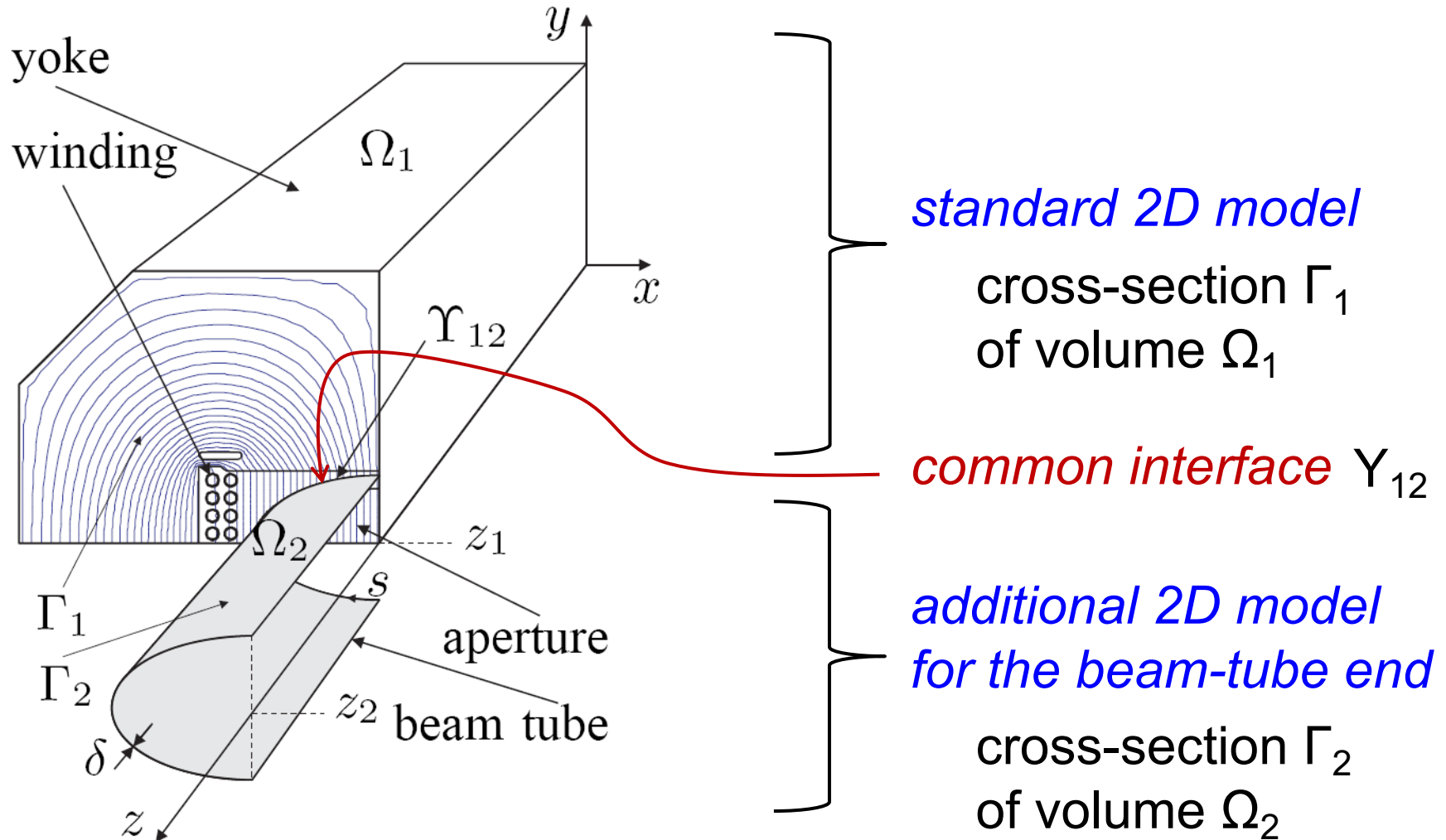


Legendre distribution in r
equidistant distribution in θ
Legendre distribution in z

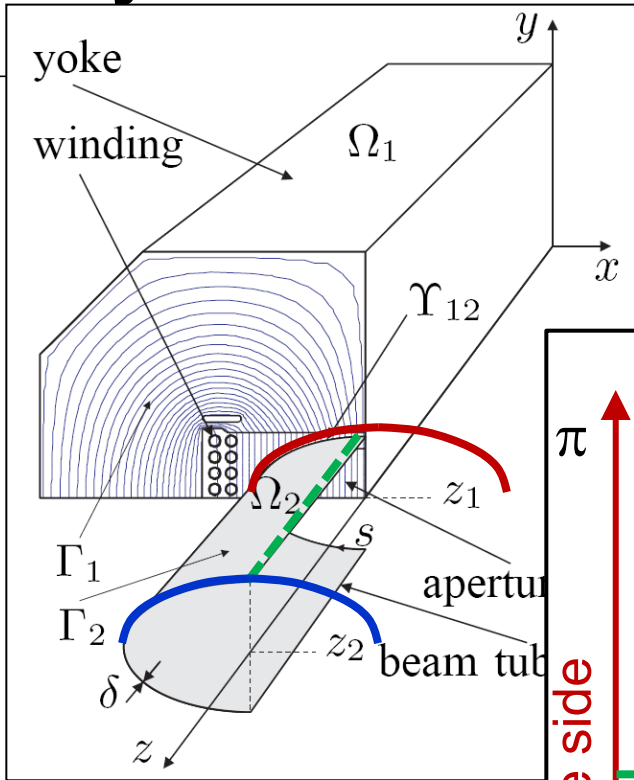
$$N_q(r, \theta, z) = N_{q_1, q_2, \lambda}(r, \theta, z) = P_{q_1}\left(\frac{r}{R}\right) e^{-j\lambda_q \theta} P_{q_2}\left(\frac{z}{Z}\right)$$

+ Markus Clemens

Beam-tube end model

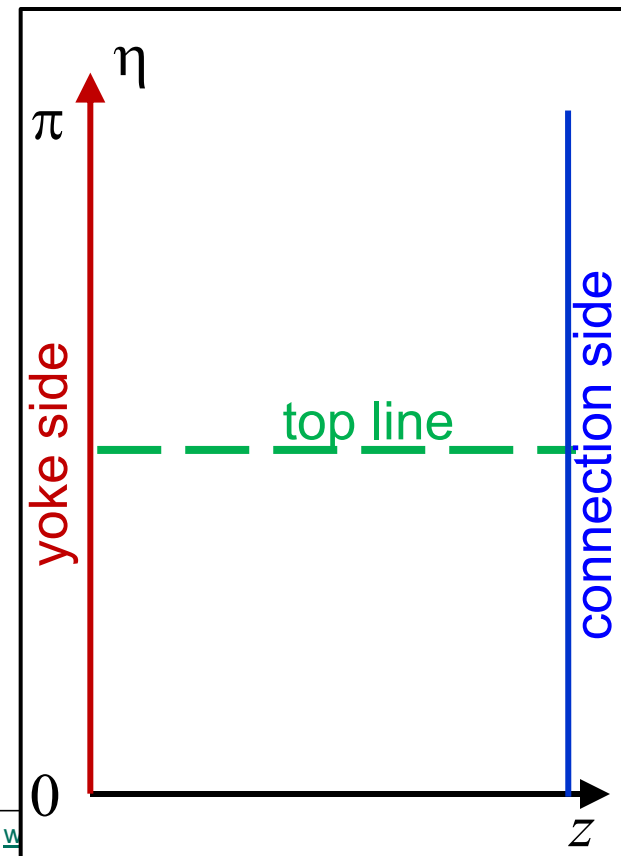
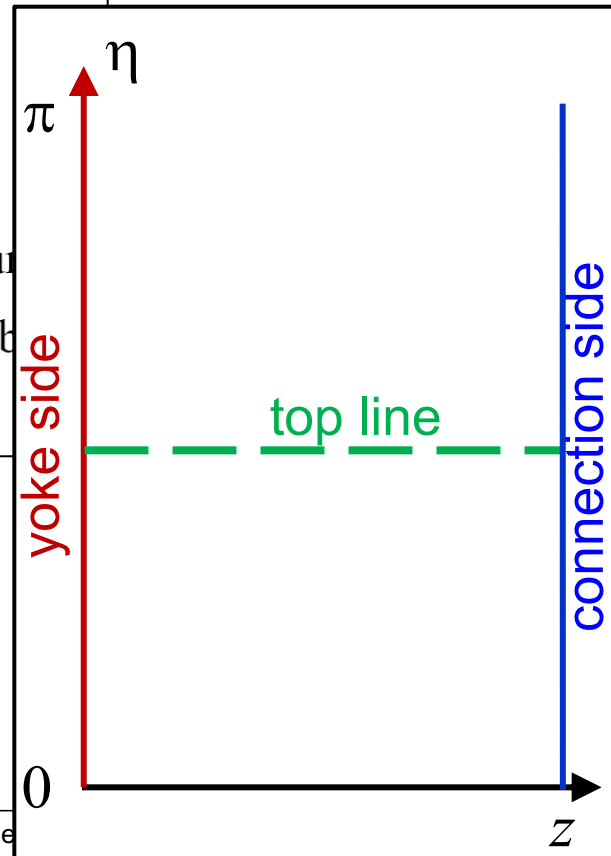


Eddy-current closing paths



connected
beam tube

disconnected
beam tube



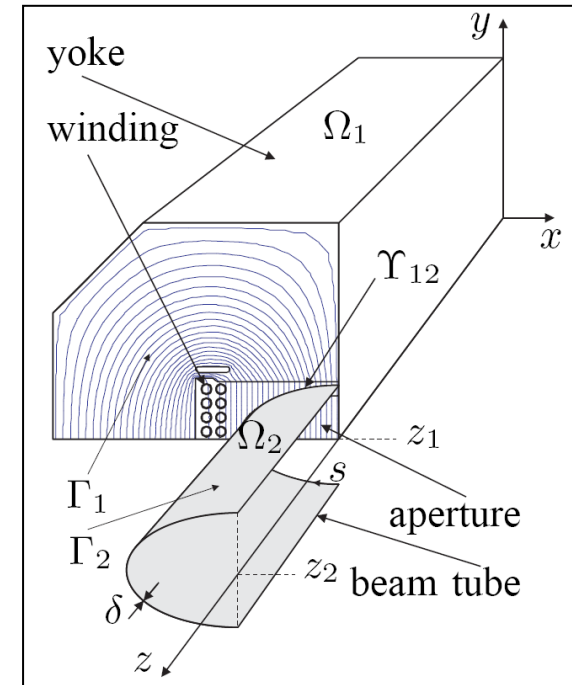
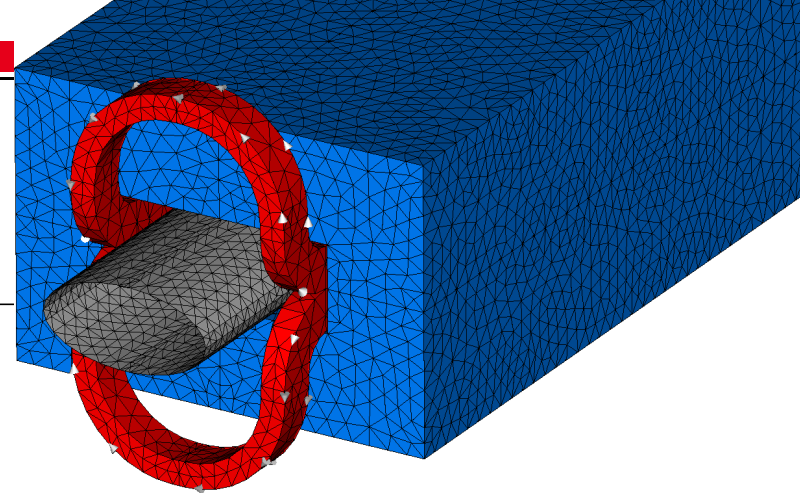
yoke side

top line

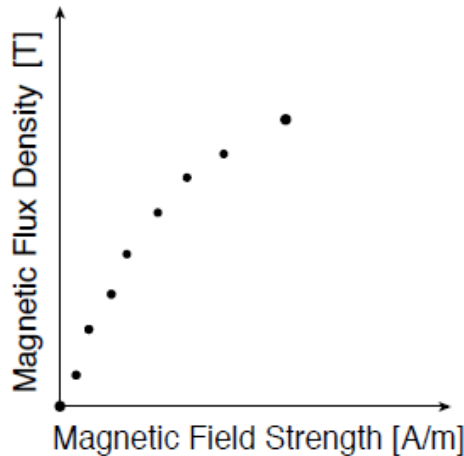
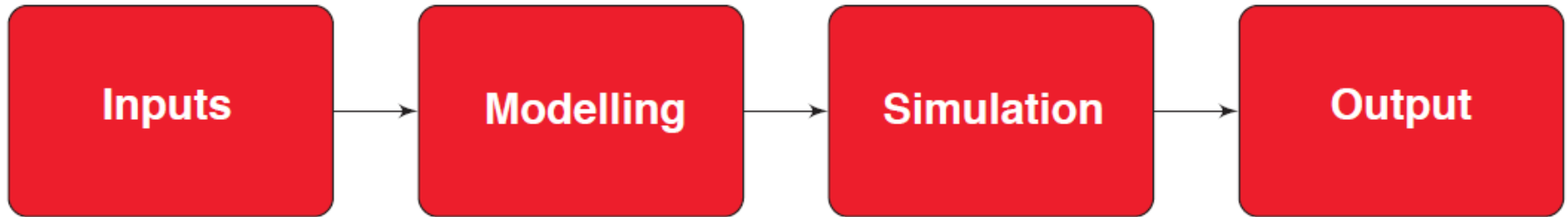
connection side

Overview

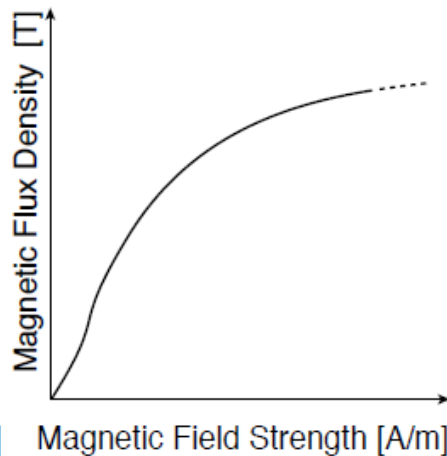
- magnet simulation (standard 3D FE solver)
- challenges
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hybrid models
- **stochastic models**
- **conclusions**



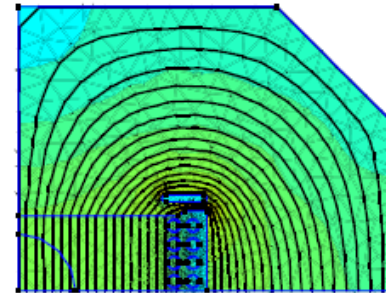
Uncertainty quantification



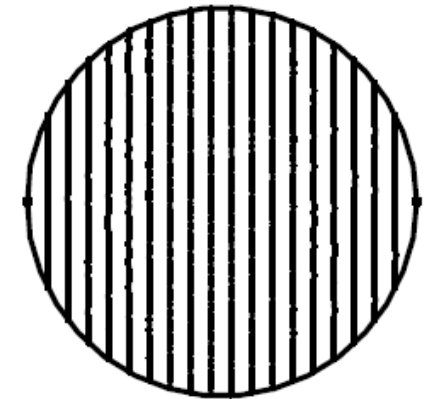
Measurement



Model of saturation



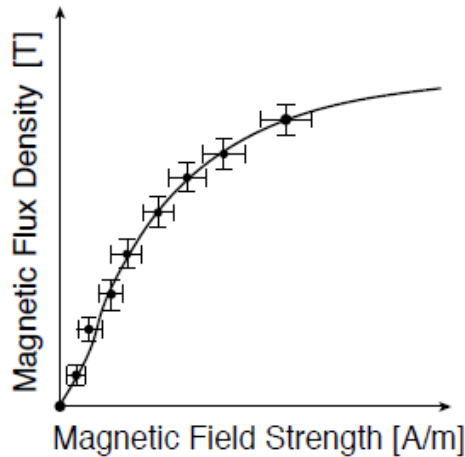
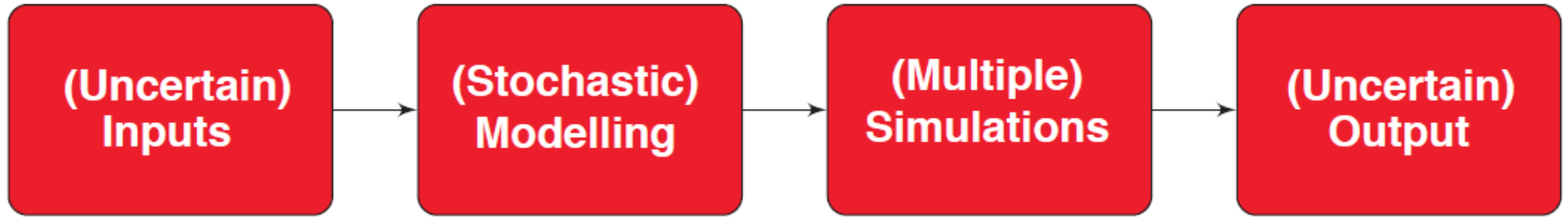
Accelerator Magnet



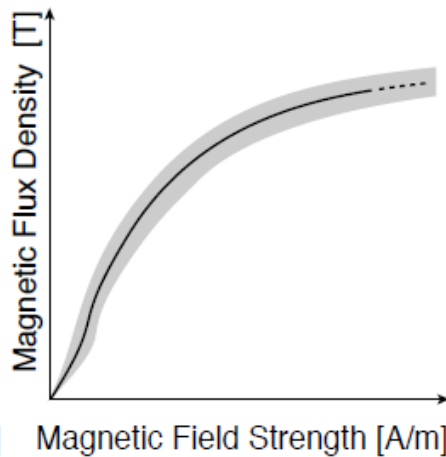
Multipoles b_j

+ Ulrich Römer, Sebastian Schöps

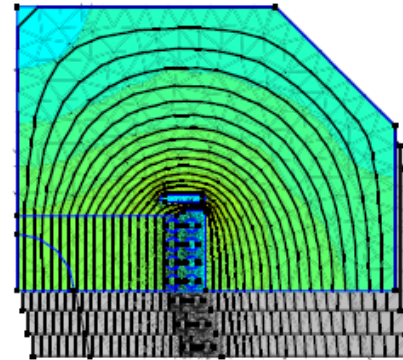
Overview



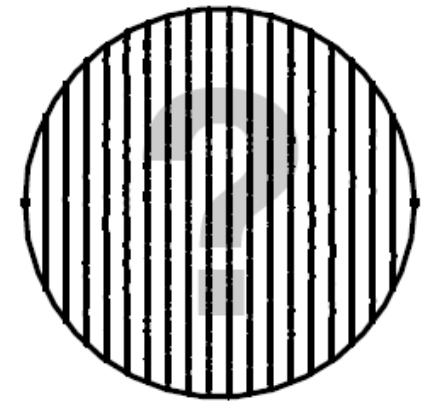
Measurement



Model of saturation



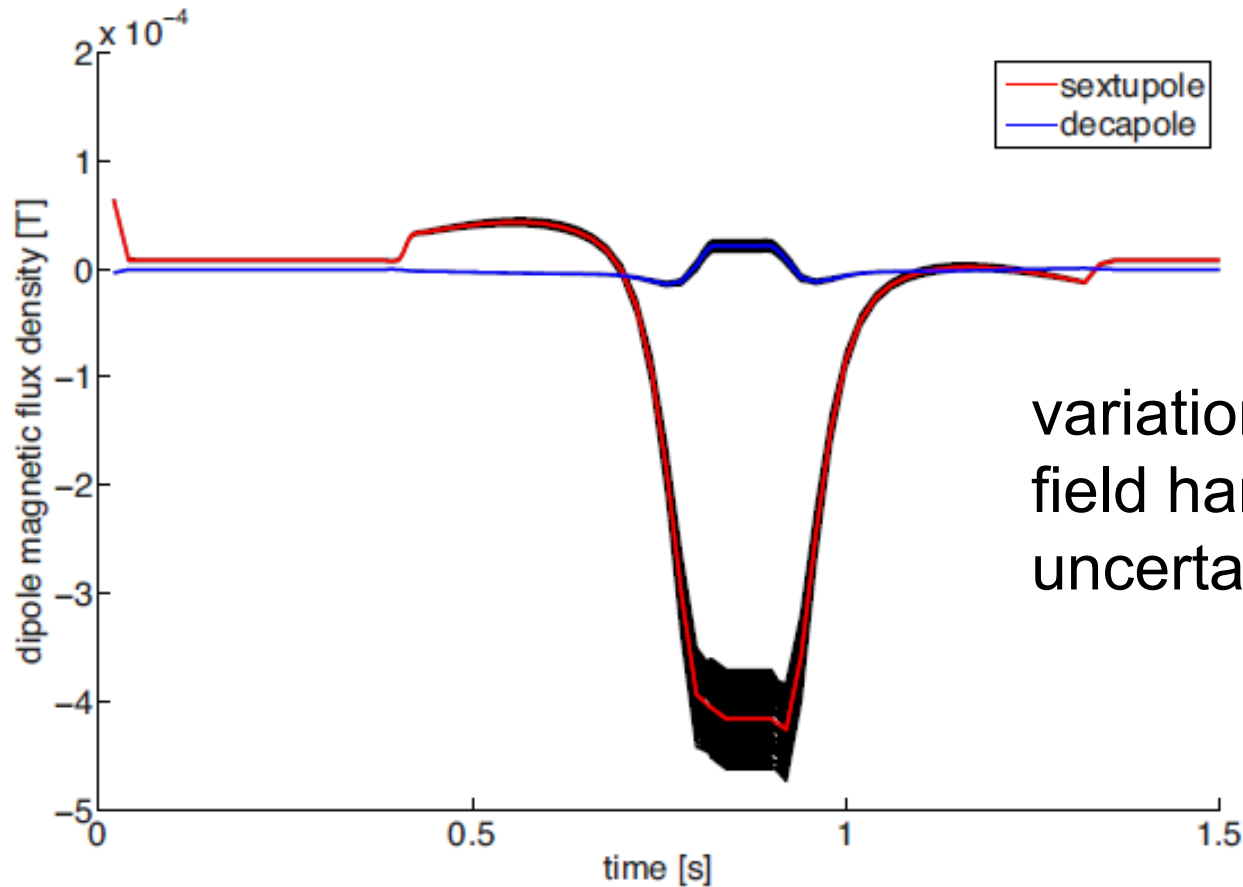
Accelerator Magnet



Multipoles b_i

+ Ulrich Römer, Sebastian Schöps

Uncertainty quantification



variation on the
field harmonics due to
uncertain BH-characteristic

+ Ulrich Römer, Sebastian Schöps

Conclusions

- nonlinear 3D transient magnetic simulation feasible with off-the-shell software
- challenges remain and are problem specific
 - geometrical details
 - materials
 - transient effects
 - high accuracy
- dedicated methods and software

