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BEAM POSITION DEPENDENCE OF A WALL-CURRENT MONITOR

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Abstract

It was pointed out accently that there exists an appreciable beam position described in the wall statent mentor widely used a selectron accelerator. Detailed states of this dependence of performance is next orners varying the puls, width and the region of the appreciation in the results a experiments show that when the prace width becomes shorter more appreciable becomes the dependence, and it approaches to that if a subtraction the resthod of images. A unified analysis ander vay.

Introduction

A wall intent more of control the more is were an enabley of order for particles as extentions of a succeeding measure the beam crarect and as ways form and more united for short pulse the tention as a like ware of

Bowers, it was provided as a consecutive there is agrificant beam printing areas, and was then made to make own the charactristics and performance of this monitor of the results of the study is that the output argued as not proportional to the input signal in magnitude, but precisely proportional makes. These results are rejected elsewhere.

This paper describes a midy about the beam passive dependence of this detector. The information repetition to clarify the property of this dependence.

Experimental method

The operational principle of the consists with kown, across the register of a second before by a softage difference is produced by a soft outcome is a

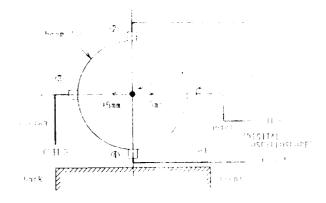


Fig.1 Schematic drawing of the monitor cross section

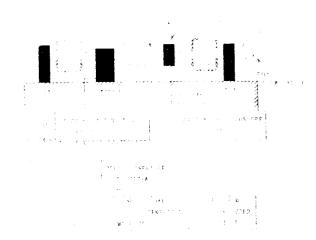
through it, and the current flow is esused by the beam. A schematic drawing of the monitor cross-section is shown in Fig.1, the monitor has four output ports to make clear the current distribution around the register.

The layout of the experimental apparatus is shown as Fig. 2. The beam duct has an insulator in its middle a unit which the monitor is installed. The beam is insulated by a current passing through a wire set in the counter of the beam duct. The current is supplied by a large pulse from a pulse generator 149.8131A.)

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the bean position dependence of the monitor. One is the experiment in which the width is saired of the input signal, the other is that the frequency is varied for the sinusoidal waveform used as an input signal. Although the beam does not have a sinusoidal waveform, the trequency dependence of the cause to produce the position dependence may probably be shown more directly by using the sinusoidal input

The attenuation of the signal in the cable and the voltage gain of the oscilloscope depend on the pulse width or the frequency of the signal, and both are measured and corrected for each measurement.

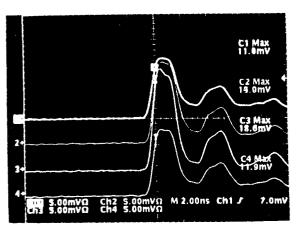


Fig.3 Waveforms of the monitor outputs from ch.1 to 4 for 1 ns input

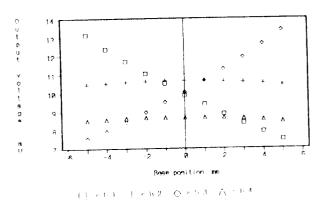


Fig.4 Output voltage vs. beam position for ch.1 to 4

Results and disscussions

Typical output waveforms are shown in Fig.3. The pulse width is 1 nsec, and the beam position is +5 mm. The channel number of each signal from the top to the bottom is 1 to 4, respectively, and corresponds to the output port indicated in Fig.1. An appreciable reflection of the signal is observed, however its influence may be mostly avoided in reading the magnitude by selecting an appropriate time point.

A result of the measurements is shown in Fig 4, in which the output signals from four channels are plotted as a function of the beam position. The pulse width is 1 nsec in all measurements. As is shown in the figure, four curves give different behaviours which are characteristic for the output positions relative to

the beam position deviation from the center.

Figure 5 shows a summery of the measurements for channel 1, where the output vs. the beam position is shown and the parameter is the pulse width varied from 750 ps to 50 ns.

When the pulse width is 50 nsec long, the output secarcely depends on the beam position. However, when the width becomes shorter, more apreciable becomes the dependence, and when it comes near or less than a few nanoseconds, the outputs seem to approach gradually to a solid curve shown in the Fig.5. This curve is obtained by the method of images, and given by [5]

$$r^{2} - \delta^{2}$$

$$r^{2} + \delta^{2} - 2r \delta \cos(\theta - \phi)$$
(1)

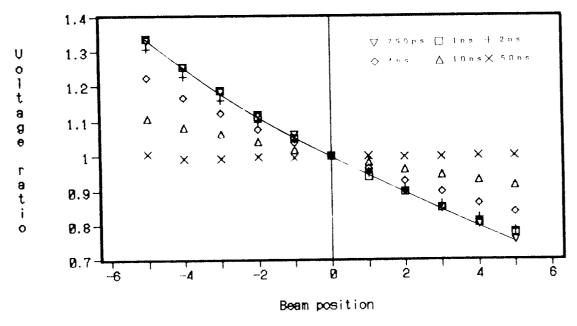


Fig.5 Output voltage vs beam position; the parameter is the pulse width

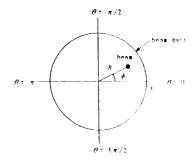


Fig.6 Beam position in the beam duct

where the quantities used are those given in Fig 6. In the calculation the value of r is required, and is assumed to be 35.25 mm which is about the average value of the solid register.

The result for channel 3 of the monitor output is very similar to the channel 1 described above. As shown in Fig.1, the channel 2 and 3 are much less sensitive to the beam position displacement as is also expected from Eq.(1).

Figure 7 represents the output waveforms for the channel 1 to 4 when the sinusoidal input is supplied The frequency is 300 MHz and the beam position + 5 mm. The results of the measurements for channel 1 is shown in Fig.8 where the frequency of the input is varied. The parameter is the frequency varied from 10 MHz to 300 MHz, and at 10 MHz the output does not seem to depend on the beam position. However, the frequency becomes higher more appreciably depends the output on the beam position. This is very similar to the previous experiment where the pulse width is varied. The solid curve is the one calculated by Eq.(1). At 300 MHz the experimental data show more appreciable beam position dependence than the calculated. Detailed examination of these data is under The reason to cause such beam position dependence is suggested to be due to the rxistance of an

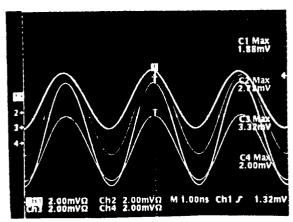


Fig 7 Waveforms of the monitor outputs from ch.1 to 4 for 300 MHz input

impedance along the beam duct in azimuthal direction [1], [2], and this impedance is shown most likely to be an inductance [3]. However, unified quantitative analysis of this monitor is required on various characteristics, and now in progress

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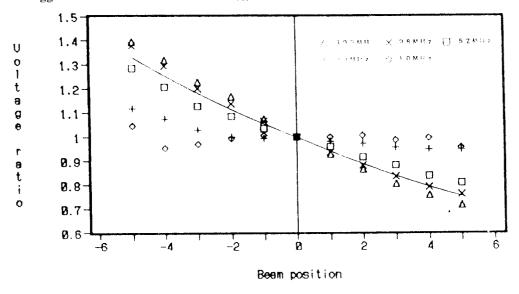


Fig.8 Output signals vs beam position; the parameter is the frequency