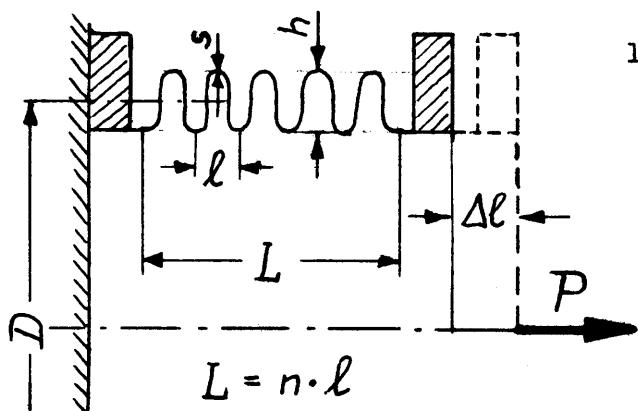


### HOW TO CALCULATE BELLOWS

As first order approximations, the following formulas are recommended. They do not make a difference between hydroformed and welded types. A refined version of this note will appear later.



#### 1) Extension

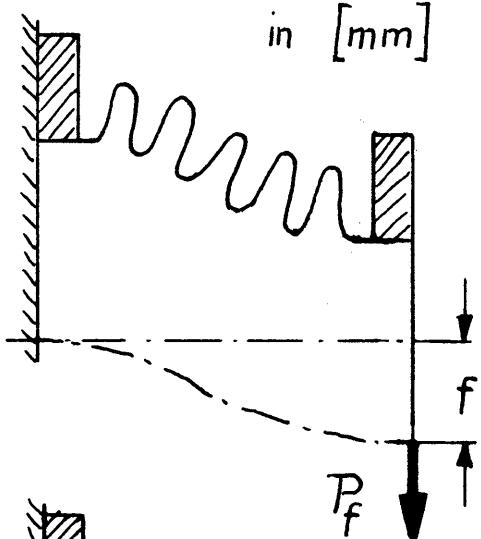
$$\Delta l = \frac{2 \cdot n \cdot h \cdot (\ell + h)}{3 \cdot E \cdot s} \sigma \quad [\text{mm}]$$

$$P = \frac{\pi \cdot D \cdot s^3 \cdot E}{2 \cdot n \cdot h \cdot (\ell + h)} \Delta l \quad [\text{kg}]$$

$$\sigma = \frac{3h}{\pi \cdot D \cdot s^2} P \quad [\text{kg/mm}^2]$$

all dimensions

in [mm]



#### 2) Displacement

$$f = \frac{L^2 \cdot h \cdot (1+h/\ell)}{9 \cdot E \cdot s \cdot D} \sigma \quad [\text{mm}]$$

$$P_f = \frac{3 \cdot \pi \cdot s^3 \cdot D^3 \cdot E}{2 \cdot L^3 \cdot h^2 \cdot (1+h/\ell)} f \quad [\text{kg}]$$

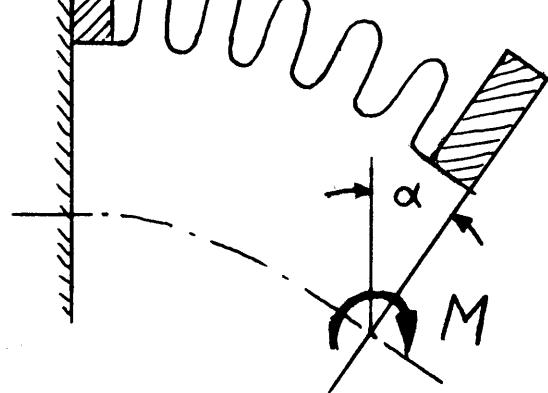
$$\sigma = \frac{6 \cdot h \cdot L}{\pi \cdot D^2 \cdot s^2} P_f \quad [\text{kg/mm}^2]$$

#### 3) Bending

$$\alpha = \frac{4 \cdot n \cdot h \cdot (\ell + h)}{3 \cdot E \cdot s \cdot D} \sigma \quad [\text{rad}]$$

$$M = \frac{\pi \cdot s^3 \cdot D^3 \cdot E}{16 \cdot n \cdot h^2 \cdot (\ell + h)} \alpha \quad [\text{mm} \cdot \text{kg}]$$

$$\sigma = \frac{12 \cdot h}{\pi \cdot s^2 \cdot D^2} M \quad [\text{kg/mm}^2]$$



4) Vacuum contributions

$$\Delta P = \frac{\pi D^2}{4} \cdot p \quad [kg] \quad \text{with } p = 0,01 \text{ kg/mm}^2$$

$$\Delta P_f = \frac{\pi D^2 \cdot f}{4 \cdot L} \cdot p \quad [kg]$$

$$\Delta M = \frac{\pi D^2 \cdot L \cdot (1 - \cos \alpha)}{4 \alpha} \cdot p \quad [mm \cdot kg]$$

$$\Delta \sigma = \frac{3}{8} \left(\frac{h}{s}\right)^2 p \quad [kg/mm^2]$$

hence avoid bellows with  $h/s > 100$   
for vacuum applications

5) Strain values

For stainless **steel** (304) is  $E = 20\,000 \text{ kg/mm}^2$ .  
Recommended maximum values for  $\sigma$  are :

- ± 12  $\text{kg/mm}^2$  for dynamic loads with less than 2 c/s.
- ± 24  $\text{kg/mm}^2$  up to a maximum of 1000 strokes.
- ± 36  $\text{kg/mm}^2$  for no more than 10 movements.

No plastic deformation is noticeable until one passes  $40 \text{ kg/mm}^2$ .

6) Comparison

Calorstat (Paris) uses for its hydroformed bellows 2 to 3 times bigger  $\sigma$ -values and gives for welded bellows a spring force which is 3 to 4 times bigger than calculated here.

Boa (Luzern) recommends for hydroformed bellows slightly lower  $\sigma$ -values.

Comments are welcomed

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Distribution :

ML-design and vacuum section

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## RECOMMENDED CERN-BELLOWS FOR VACUUM APPLICATIONS

26.11.69 R

int/ext. diameter * wall-thickness mm	n	Values for L = 100 mm and $\sigma = 24 \text{ kg/mm}^2$						$\Delta M$ mm.kg
		$\Delta\ell$ mm	P kg	$\Delta P$ kg	f mm	$P_f$ kg	$\Delta P_f$ kg	
7/20 x 0,08	65	34	0,33	1,43	42	0,023	0,6	288° 1,1 19,6
20/40 x 0,1	40	40	0,75	7,1	22	0,113	1,56	153° 5,6 500
30/50 x 0,1	40	40	1,0	12,6	16,7	0,2	2,1	114° 10 890
75/95 x 0,1	40	40	2,13	57	7,8	0,91	4,4	54° 45 2 500
90/115 x 0,12	40	50	2,97	82	8,1	1,52	6,6	56° 76 3 700
100/150 x 0,25	20	48	7,86	122	6,4	4,9	7,8	44° 246 4 500
160/180 x 0,1	30	32	4,28	226	3,1	3,6	7,0	22° 182 4 400
200/230 x 0,15	40	56	8,1	363	4,3	8,7	15,6	30° 435 9 400
230/270 x 0,2	20	40	12,6	490	2,7	15,8	13,2	18° 790 7 800
280/330 x 0,25	20	48	19,2	730	2,6	29,3	19	18° 1 460 11 600