

ACOL MAGNETS WITH REFERENCE TO LATTICE No. 84-05

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Introduction

In order to find a solution for the injected/ejected beam, to simplify the design and reduce the total cost, the following changes have been decided:

- Build 2 types of dipole: BHN (narrow) and BHW (wide).
- All semi-quadrupoles (QS) have been converted into narrow quadrupoles (QN) except those two involved in the injection region (QDS 53 and QFS 54). *These QN will be displaced in order to get the right bending angle.*

The consequence is a small increase of the aperture of the QN in order to accept the beam in the previous QS regions. The aperture of the wide quadrupoles (QW) remains the same.

All sextupole magnets *have* been removed for chromaticity corrections. Consequences are:

- i) Build sextupole components *into* in the profile of all QW's.
- ii) ~~However~~, all PU electrodes *could be* ~~can remain~~ in focusing quadrupoles, ~~if necessary~~.
- iii) The narrow QFN 6 (and symmetric) becomes a wide QFW 6 because a sextupole component is needed at this location to get symmetric orbit throughout the $\Delta p/p = \pm 3\%$ and minimize the orbit distortions in the regions $\alpha_p = 0$.

Figure 1 shows the present ACOL layout.

Lattice

Annex 1 gives the optic parameters retained for the present lattice (84-05) and completed by B. Autin.

Geometry

axis X X Table 1 gives the geometry of the machine from the AGS program. The distance between ACOL axis and AA axis at injection region is 1.7855 (m).

Dipoles

X end- Table 2 gives the characteristics for both types (BHN and BHW). No sextupole component will be built either in the pole or at the ends. Only shimming will be done at the end for small corrections. No prototypes will be built for these 2 families.

X Figure 2 shows the pole profile of a narrow dipole and Fig. 3 shows the pole profile of a wide one.

X A spare coil for each type of dipoles will be built.

The field precision $\Delta B/B$ should be $\pm 2 \times 10^{-4}$ in the good field region. However, the spread $\Delta B/B$ over the 24 dipoles should be less than 10^{-4} .

X At the ^{momentum} energy $p = 3.5752$ GeV/c, the rigidity value is $B\rho = 11.9255835$ Tm.

Table 2 - Dipole Parameters

		BHN	BHW
Number		8	16
Field	(T)	1.502	1.583
Effective length	(m)	1.9513	1.8513
Field x Eff. length	(Tm)	2.93131	2.93131
Bending radius	(m)	7.93857	7.53173
Deflection angle	(rd)	0.2458	0.2458
Gap height	(mm)	±50	± 58
Good field width	(mm)	147 + 60	±180
Good field height	(mm)	±45	± 52
Sagitta	(mm)	±30	± 28.4

*** ACOL RING LATTICE - VERSION 84.05 ***

WEDGE MAGNETS OF THE EXITS OF THE ELEMENTS
 X-COORDINATES OF THE FIRST ELEMENT IS AT X = 0 Y = 0
 THE ENTRANCE OF THE FIRST ELEMENT IS AT X = 0 Y = 0
 PHI IS THE ANGLE BETWEEN THE ORBIT AND THE X-AXIS
 PHI = 0 AT THE BEGINNING

NO	NAME	LENGTH	ANGLE	K(V)	X	Y	PHI
1	QDN1	3500	0.00000	58000000	3500000	0.000000	0.000000
2	SS	2.6000	0.00000	0.0000000	2.9500000	0.000000	0.000000
3	QFN2	7000	0.00000	-58000000	3.6500000	0.000000	0.000000
4	SS	2.6000	0.00000	0.0000000	6.2500000	0.000000	0.000000
5	QDN3	7000	0.00000	58000000	9.4500000	0.000000	0.000000
6	SS	2.5000	0.00000	0.0000000	0.149895	0.010499	0.030000
7	QF*4	7000	30.00000	-55000000	12.648770	0.085488	0.030000
8	SS	2.5000	18.00000	0.0000000	13.772739	1.131781	0.048000
9	QD*5	4250	0.00000	5152200	15.690776	1.33173	0.048000
10	BHN1	9513	245.80000	0.0000000	16.073636	4.464194	0.293800
11	SS	1.4000	0.00000	0.0000000	16.791498	5.80031	0.293800
12	QFW6	7500	0.00000	-4457000	17.910841	7.97224	0.293800
13	SS	1.8513	245.80000	0.0000000	18.222116	9.27541	0.539600
14	BHW2	4513	0.00000	0.0000000	19.090338	6.74960	0.539600
15	SS	1.4500	0.00000	0.0000000	19.296900	1.99061	0.539600
16	QDW7	7500	0.00000	4905500	21.527480	2.24202	0.539600
17	SS	1.8500	0.00000	0.0000000	22.170915	3.62737	0.539600
18	QFW8	7500	0.00000	-5428100	22.569775	6.25858	0.539600
19	SS	1.4500	0.00000	0.0000000	24.012973	8.94431	0.785400
20	BHW3	8513	245.80000	0.0000000	24.331173	9.94431	0.785400
21	SS	1.4500	0.00000	0.0000000	24.861502	8.42961	0.785400
22	QDW9	7500	0.00000	3863100	25.179699	1.61160	0.785400
23	SS	1.8513	245.80000	0.0000000	26.315546	6.17163	0.031200
24	BHW4	4513	0.00000	0.0000000	26.546751	8.03225	0.031200
25	SS	1.4500	0.00000	0.0000000	26.932093	6.46662	0.031200
26	FW10	7500	0.00000	-5428100	27.882604	8.23380	0.031200
27	SS	1.8500	0.00000	0.0000000	28.279946	9.87724	0.031200
28	DW11	4500	0.00000	4905500	28.499152	10.87306	0.031200
29	SS	1.4500	0.00000	0.0000000	29.246565	11.93426	0.277000
30	BHW5	8513	245.80000	0.0000000	29.394071	13.38265	0.277000
31	SS	1.4500	0.00000	-4457000	29.709906	14.10051	0.277000
32	FW12	4000	0.00000	0.0000000	30.040920	14.48337	0.277000
33	SS	1.9513	245.80000	0.0000000	30.40920	16.40141	0.522800
34	BHN6	4250	0.00000	0.0000000	30.061311	16.82592	0.522800
35	SS	1.4250	18.00000	5152200	30.088601	17.52538	0.540800
36	D*13	7000	0.00000	0.0000000	30.163581	20.72415	0.540800
37	SS	2.5000	30.00000	-5500000	30.174077	22.41533	0.570800
38	F*14	7000	0.00000	5500000	30.174077	23.57415	0.570800
39	SS	2.5000	0.00000	0.0000000	30.174068	23.57415	0.570800
40	SS	2.3500	0.00000	58000000	30.174067	23.57415	0.570800
41	DN15	3500	0.00000	0.0000000	30.174067	23.57415	0.570800

THE COORDINATES OF THE MACHINE CENTRE ARE X = 3.300000, Y = 26.874055

MAXIMUM RADIUS = 30.128811

MINIMUM RADIUS = 26.876334

Table 1

Quadrupoles

Table 3 gives the characteristics for both types (QN and QW). Figure 4 shows the QN profile. Figures 5 show the QFW profile with sextupole components and beam sizes. Figures 6 show the QDW profile with sextupole components and beam sizes.

No prototype will be built for these 2 families. A spare quadrupole of each type will be built.

The two semi-quadrupoles at injection are under study.

Table 3 - Quadrupole Parameters

			QN	QW
Number			26	28
Strength	max.	(m ⁻²)	0.58	0.54281
Gradient	max.	(T/m)	6.92	6.47
Effective length		(m)	0.7	0.75
Gradient × eff. length		(T)	4.84	4.85
Inscribed circle radius		(m)	0.110	0.132
Good field width		(mm)	±130	±160
Good field height		(mm)	± 60	± 60

The gradient precision $\Delta G/G$ should be $\pm 2 \times 10^{-3}$ in the good field region.

Table 4 gives the distribution of quadrupoles in focusing and defocusing families, assuming same current in each family.

Table 5 gives the distribution after an optimization of the number of turns. The ^{consequences} ~~differences~~ are:

- i) inscribed circle radius for QW = 133.01 mm. *fine*
- ii) quadrupoles ^{incircled} ~~into circles~~ will have shunts for ~~final~~ *final* adjustments. *fine*
- iii) a separate power supply will feed current in the QFN₄ and QDN₅ in series.

Quadrupole distribution (1)

- 5 -

	QF				
	QFN		QFW		QFS54
	QFN ₂	QFN ₄	QFW ₆	QFW ₈	
l_{eff} (m)	0,70	0,70	0,75	0,75	0,70
K (m^{-2})	-0,58	-0,55	-0,4457	-0,54281	-0,55
$S = K \cdot l_{eff}$	-0,406	-0,385	-0,33427	-0,4071	-0,385
r (mm)	110	110	132	132	127
G (T/m)	6,92	6,56	5,31	6,47	6,56
B_{pole} (T)	0,76	0,721	0,701	0,854	0,83
n (turns)	19	18	(21,3)	(25,6)	24
N (number of magnets)	4	7	8	8	1

	QD				
	QDN		QDW		QDS53
	QDN ₁	QDN ₅	QDW ₇	QDW ₉	
l_{eff} (m)	0,7	0,7	0,75	0,75	0,7
K (m^{-2})	0,58	0,51522	0,49055	0,38631	0,51522
$S = K \cdot l_{eff}$	0,406	0,3606	0,3679	0,2897	0,3606
r (mm)	110	110	132	132	110,4
G (T/m)	6,92	6,14	5,85	4,60	6,14
B_{pole} (T)	0,76	0,67	0,77	0,60	0,67
n (turns)	19	(16,8)	(23,5)	(18,5)	17
N (number of magnets)	8	7	8	4	1

Table 4

Quadrupole distribution (2)

	QF				
	QFN		QFW		QFS54
	QFN ₂	QFN ₄	QFW ₆	QFW ₈	
l_{eff} (m)	0,70	0,70	0,75	0,75	0,7
K (m^{-2})	-0,58	-0,55	-0,4457	-0,54281	-0,55
$S = K \cdot l_{eff}$	-0,406	-0,385	-0,33427	-0,4071	-0,385
r (mm)	110	110	133,01	133,01	126,17
G (T/m)	6,92	6,56	5,31	6,47	6,56
B_{pole} (T)	0,76	0,721	0,701	0,854	0,83
n (turns)	19	19	22	26	25
N (number of magnets)	4	7	8	8	1
I (A)	1752,6	1662	1752,6	1752,6	1662

	QD				
	QDN		QDW		QDS53
	QDN ₁	QDN ₅	QDW ₇	QDW ₉	
l_{eff} (m)	0,7	0,7	0,75	0,75	0,7
K (m^{-2})	0,58	0,51522	0,49055	0,38631	0,51522
$S = K \cdot l_{eff}$	0,406	0,3606	0,3679	0,2897	0,3606
r (mm)	110	110	133,01	133,01	110,6
G (T/m)	6,92	6,14	5,85	4,60	6,14
B_{pole} (T)	0,76	0,67	0,77	0,60	0,67
n (turns)	19	18	24	19	18
N (number of magnets)	8	7	8	4	1
I (A)	1752,6	1662	1752,6	1752,6	1662

Sextupole Location in the QW in ACOL

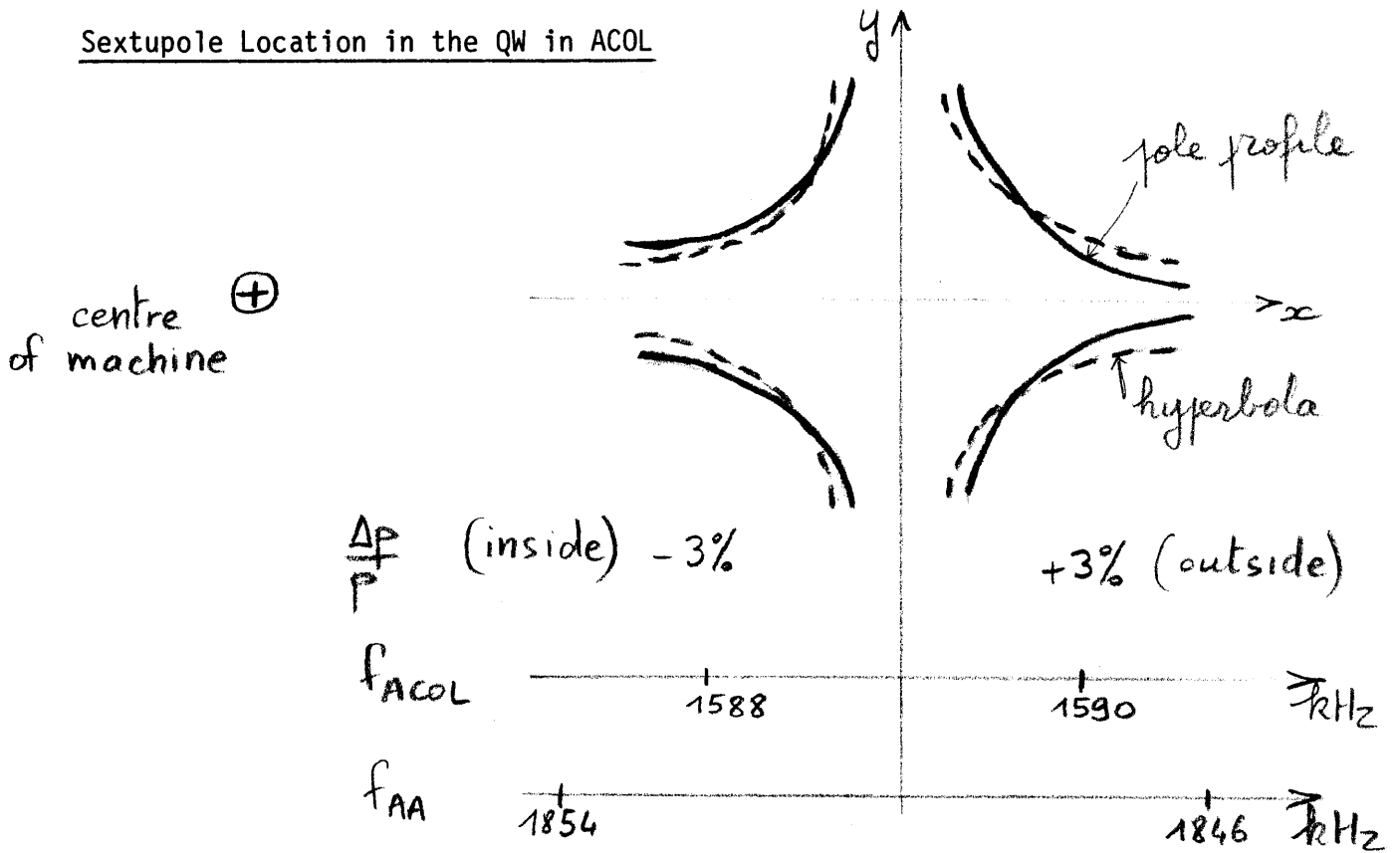


Figure 7

For each QW in ACOL the narrower gap is situated towards the outside of the machine.

Permeability

Figure 8 shows the permeability curve used by RAL and CERN.

Magnet Sizes

Table 6 below gives a rough approximation of magnet dimensions.

Table 6

		BHN	BHW	QN	QW
l_{eff}	(m)	1.9513	1.8513	0.700	0.750
l_{Fe}	(m)	1.812	1.69 1,765	0.60	0.64
Overall length	(m)	2.4 2,2	2.2 2,140	0.84	0.85
Overall width	(m)	1.0 1,4	1.9 2,050	1.10	1.4
Overall height	(m)	1.0 1,15	1.5 1,215	1.10	1.3

β Variations across Aperture

Figure 9 shows the β variations with momentum according to the results from ORBIT program (B. Autin). These variations are plotted in one dipole (BHN1) and in one quadrupole (QFW6). The maximum $\Delta\beta/\beta$ is 18%.

Figure 10 shows the η variations with momentum and Figure 11 gives the Q_H , Q_V variations with momentum.

Beam Monitoring

It is possible to put PU electrodes in each focusing quadrupole except in QFS 54. ~~A new study will be made by H. Koziol.~~

Vacuum Chambers

Figures 2 to 6 show possible vacuum chambers. An updated design will be done by F. Malthouse ~~and R. Bennett (RAL).~~

Power Supplies

For dipoles, a main power supply will be necessary along with a trim power supply. For quadrupoles, two main power supplies (~2000 A each) for QF and QD. Another main power supply (~2000 A) will feed current in all the QFN's and QDN's which are displaced in the machine.

~~According to the solution found for QDS 53 and QFS 54,~~ Two small trim power supplies (~50 A) may be necessary.

All ^{major} adjustments will be done by ^{adapting} ~~changing~~ the number of turns on requested quadrupole families. The final adjustments will be made by small shunts and/or shims.

In the long term, the necessity to put small sextupole magnets in the machine for resonance corrections will be studied. If they are needed, two more small power supplies would have to be built.

An updated proposal will be made by F. Völker.

Fig 1

