

AA INJECTION AND EJECTION BEAM LINES

T. Sherwood

Contents

1. Text
2. Appendix I. Non standard TRANSPORT elements and correspondence between BEATCH and TRANSPORT beam parameters
3. Data lists
4. Beam envelope graphs
5. Momentum vector graphs
6. List of magnet elements parameters and operating requirements

Introduction

This note gives a summary of the beam optics calculated for the AA beam lines. A non-standard version of TRANSPORT has been used, but users of the standard CERN version should be able to follow the appended data lists. Appendix I explains the relevant differences as well as giving some correspondences between TRANSPORT and BEATCH data conventions. Data files are stored on the permanent data file base for the CDC-MFB computer under the names AADn, ID = PS 321 TRS.

Names of beam line magnets follow the system described in PS/AA/Mem.79-41 (Blechsmidt, Sherwood, 28.3.79) and differ from those used in previous (informal) notes.

Lists of beam elements are given showing beam size and required currents against apertures and maximum nominal current available. The geometrical layout is given in PS/ML/BS/nc, (Mayoud, Szeless, 25.5.79).

When reading the geometry and beam optic lists, the following points should be noted:

1. Distances are given along the beam axis, whether sloping or horizontal.
2. Magnetic lengths are usually used, but in any case, the centre of the element and the integral of the field or gradient are always well defined.
3. The length of a bending magnet is defined as the arc length of the central trajectory (TRANSPORT convention). For a rectangular magnet block, of length L , oriented symmetrically to the incoming and outgoing beams and which gives a deflection angle θ , we have the related lengths:

a) arc-length, s , where

$$s = L\theta / (2 \sin \frac{\theta}{2})$$

and L' , the distance from entry (or exit) to the intersection point of the entering and exiting beams where

$$L' = (L/2) \sec \frac{\theta}{2}$$

Usually s , $2L'$ and L are only slightly different.

4. Tilt angles are defined in the geometry memo. In TRANSPORT a tilted magnet is treated by rotating the beam reference axis about the beam longitudinal direction so as to align it with the magnet element system. The angle is introduced via a TRANSPORT type 20 element. When the incoming beam X axis is horizontal, tilt and rotation angles are identical. Since beam envelopes are given in the beam reference system, the presence of tilted magnets introduces the discontinuities seen in the graphs. A vertical bending magnet is treated as a tilted magnet with tilt angle 90° .

Beam Envelopes

The injection line is treated in two parts:

- a) From the PS to the antiproton production target
and
- b) From the target to the end of the injection/ejection straight section.

The ejection line is taken from the start of the ejection straight section to a point just beyond the crossing with TT2.

The interpretation of the accompanying beam envelope and momentum vector graphs differ in these three sections.

Injection line PS to target

A small beam waist is required at the target for 26 GeV/c incident protons. The lower limit to beam size (apart from power density in the target itself) is given by the emittance and momentum spread of the PS beam as well as the apertures in the final vertical bending magnet and pulsed quadrupoles. The momentum vector ($\alpha_p, \alpha_{p'}$) should be zero at the target in both transverse planes, ($\alpha_{p'}$ does not affect beam size at the target but does use aperture in the upstream magnets). Such solutions were not found, in particular the condition ($\alpha_{p'}$) v was not possible and allowance had to be made for this.

The aperture required to pass this fraction of the beam is then

$$A = 2 \left[w^2 + \left(\frac{\Delta p}{p} \alpha_p \right)^2 \right]^{\frac{1}{2}} + 2 \frac{dp}{p} \alpha_p$$

where w is the half-width of one component. Values of A_H, A_V are given in the table comparing required aperture with that available. No special allowance has been made for steering errors or poor magnetic field quality regions. In the calculations the starting point has been taken as magnet QD102. The beam parameters at this point were obtained from a BEATCH run for normal operation of TT2 when the beam is going to the ISR.

Injection line - Target to AA ring

The antiproton beam is matched to the AA ring using the lattice parameters given in the 7th edition of the parameter list (Jan. 1979) using an acceptance of 100π mm.mR., a momentum spread of $\pm 0.75\%$. The septum magnets and the small effect of the kicker on the momentum vector are included.

It is assumed that the antiproton beam is a waist of radius 22 mm at the exit of the magnetic horn. The beam envelope is for $\frac{dp}{p} = 0$ and the required apertures are given by:

$$A = 2(w + \frac{dp}{p} \alpha_p)$$

Even to get $(\alpha_p, \alpha_p')_H = 0$ requires changing two quadrupoles, QF 107, in the TT2 line to run at currents a little higher than for normal ISR operation.

Solutions are given for the following beam sizes at the centre of the target:

- 1) horizontal 1.4 mm, vertical 1.5 mm
- 2) " 2.0 mm, " 2.0 mm
- 3) " 3.0 mm, " 3.0 mm

Two solutions are given for case 3). Beam envelopes are for zero momentum spread.

PS beam assumptions

The characteristics of the PS beam have been given in PS/DL/Note.78-7 (P. Lefèvre). If the beam is combined into five bunches at 26 GeV/c, we can consider it as a double beam, each component matched to the PS lattice but separated by a distance:

$$\delta x = \alpha_p \frac{dp}{p}$$

Each component is expected to have an emittance of 2π mm.mR and a momentum spread $\frac{\Delta p}{p} = \pm 10^{-3}$ (contains 95% of the beam) but separated in momentum by $\frac{dp}{p} = \pm 2 \cdot 10^{-3}$.

The envelopes calculated are for a component emittance 2.46 mm mR giving nearer to 97½% of the beam (assuming a Gaussian model).

Ejection Line - AA ring to junction with TTL2

The hande-over point is at the end of EJ 2575(D8 is the TTL2 name). This is the second quadrupole magnet after the ejection line crosses TT2. At this point the matching conditions requested are:

$$\begin{aligned}(\alpha_p)_H &= 0 & , & & (\alpha_{p'})_H &= 0 \\(\alpha_p)_V &= -0.508, & & & (\alpha_{p'})_V &= -0.0135 \\L_H &= 10 \text{ mn} & , & & L_V &= 75 \text{ m} \\S_H &= 0 & , & & S_V &= 0\end{aligned}$$

The ejected beam is matched to the AA lattice with an initial horizontal momentum vector (-0.0745 m, 0.0039 rad) due to the ejection kicker. The emittances used are 1.4π mn mR for the horizontal and $1.\pi$ mm mR for the vertical Beam envelopes are for $\frac{dp}{p} = 0$. Required apertures are given by:

$$A = 2 \left[(w^2 + \left(\frac{dp}{p} = \alpha_p\right)^2) \right]^{\frac{1}{2}}.$$

using a value of $\frac{dp}{p} = 3 \times 10^{-4}$

The effect of momentum spread on aperture requirement is small for the above values.

APPENDIX I

Non-Standard TRANSPORT

The beam optic calculations were made using a non-standard version of TRANSPORT. The attached data lists are for this version. They differ from that required for the CERN version of TRANSPORT (CERN 73-16) in format and the presence of both non-standard element types and modified standard types. These differences are noted below. The purpose of these notes is to enable a person familiar with the standard version of TRANSPORT to be able to construct a standard data list.

1. Format. The data is given in a fixed format (1X, A10, 7F 10.5). The first word is any label (or blank). The rest of the words on each line conform to the data requirement for the element type (word 2).
2. No indicator word is used.
3. Beam momentum (4th word) is entered via the type 16. element, not with a type 1 element.
4. The initial beam description is entered by the combination of the special type 24 emittance element and the modified type 1 element. The type 24 element gives three independent emittances for the horizontal, vertical and longitudinal planes in that order. The following type 1 element gives (in TRANSPORT notation)

$$\sigma_{11}^{\frac{1}{2}}, r_{12}, \sigma_{33}^{\frac{1}{2}}, r_{34}, \sigma_{55}^{\frac{1}{2}}, r_{56}$$

5. The special type 22 element is used to obtain plots of beam envelopes.

Relations between some BEATCH and TRANSPORT parameters

1. Quadrupole strengths. TRANSPORT expect two parameters (words 4 and 5) viz. field and a radius.

The fields are given in KG and an arbitrary radius of 1 cm is used. Consequently word 4 can be interpreted as gradient, G, in KG/am. BEATCH requires the parameter K(m⁻²). G and K are related by

$$K = - \frac{G}{\{B\rho\}}$$

where G is in T/m , B_ρ is in T.m

In TRANSPORT G is positive for a horizontally focussing magnet.

2. Bending magnet lengths. BEATCH uses the straight length of a straight magnet while TRANSPORT uses the arc length of the reference trajectory.

3. BEATCH uses the parameters L, S. TRANSPORT uses the sigma matrix

Horizontal beam size , $\sigma_{11}^{\frac{1}{2}} = \left[(\epsilon/L_H) (S_H^2 + L_H^2) \right]^{\frac{1}{2}}$
" divergence , $\sigma_{22}^{\frac{1}{2}} = (\epsilon/L_H)^{\frac{1}{2}}$

Distance to beam waist is r_{12} ; $(\sigma_{11}/\sigma_{22})^{\frac{1}{2}} = S_H$

giving $r_{12} = S_H / (L^2 + S^2)^{\frac{1}{2}}$

ϵ is the emittance (ellipse area / π)

E R R A T U M

Please note that all magnetic elements
in the ejection line should have names
of the form xyz 25 nn NOT xyz 24 nn
as in the data lists and diagrams.

D10HNFIL START 20102. APH=0 AFTER 9T11. SMALL SPOT ON TARGET 22/05/79 17.47.

SETMOM	16.000000	16.000000	26.000000			
WIT	24.000000	24.000000	24.000000	0.000100	0.000000	
BEAT	1.000000	594620	-1.725385	.772111	.809361	100.000000 0.000000
PLOT	22.000000	400000	0.000000	200.000000	0.000000	1.000000
INTR2	6.000000	0.000000	2.000000			
ALPHA IN	14.000000	1.000000				
ALPHA IN	14.000000	2.000000				
ALPHA IN	14.000000	0.000000	0.000000	0.000000	1.56470	
ALPHA IN	14.000000	0.000000	0.000000	0.000000	-1.71600	
D0	0.000000	0.000000				
D4	0.000000	1.200000	-1.986960	1.000000		
ZROT	20.000000	90.000000				
EDG10	20.000000	2.050500				
VR101	20.000000	2.200000	6.953090	0.000000		
EDG10	20.000000	2.050500				
ZROT	20.000000	90.000000				
DS	20.000000	2.310000				
QF103	20.000000	1.200000	.872132	1.000000		
QF06	20.000000	2.371000				
EDG11	20.000000	1.378000				
HB102	20.000000	1.850000	6.188080	0.000000		
EDG11	20.000000	1.378000				
Q7	20.000000	8.094900				
Q104	20.000000	1.200000	-1.687576	1.000000		
Q103	20.000000	8.515000				
QF105	20.000000	1.200000	.779320	1.000000		
Q9	20.000000	1.700000				
EDG12	20.000000	1.244000				
HB103	20.000000	1.400000	-5.286640	0.000000		
EDG12	20.000000	1.244000				
Q10	20.000000	1.553000				
ZROT	20.000000	90.000000				
EDG13	20.000000	2.050500				
VR102	20.000000	2.200000	6.953090	0.000000		
EDG13	20.000000	2.050500				
ZROT	20.000000	90.000000				
Q11	20.000000	1.960000				
Q106	20.000000	1.200000	-1.745900	1.000000		
Q12	20.000000	7.960000				
QF107	20.000000	1.200000	.784521	1.000000		
Q13	20.000000	13.080000				
Q208	20.000000	7.820000	-1.019570	1.000000		
Q14	20.000000	7.940000				
QF209	20.000000	8.600000	1.006040	1.000000		
Q15	20.000000	8.430000				
Q210	20.000000	8.600000	-1.021560	1.000000		
Q16	20.000000	8.430000				
QF211	20.000000	8.600000	1.006040	1.000000		
Q17	20.000000	8.430000				
Q212	20.000000	8.600000	-1.021560	1.000000		
Q18	20.000000	8.430000				
QF213	20.000000	8.600000	1.006040	1.000000		
Q19	20.000000	8.420000				
Q214	20.000000	8.820000	-1.019570	1.000000		
Q20	20.000000	8.420000				
QF215	20.000000	8.600000	1.006040	1.000000		
Q21	20.000000	14.590000				
TL11	20.000000	-14.085600				
Q0000	20.000000	1.150000				
BT100	20.000000	2.500000	13.952518	0.000000		
EDG5000	20.000000	-1.150000				
Q22	20.000000	1.750000				
EDG001	20.000000	1.150000				
BT101	20.000000	2.500000	13.952518	0.000000		
EDG001	20.000000	1.150000				
TLB11	20.000000	14.041900				
Q23	20.000000	3.229000				
Q1M05	20.000000	1.010000	-1.114766	1.000000		
Q24	20.000000	1.019000				
TLT2	20.000000	-14.041900				
EDG010	20.000000	1.037000				
BT110	20.000000	1.960100	16.024625	0.000000		
EDG010	20.000000	1.037000				
Q25	20.000000	1.033000				
EDG011	20.000000	1.037000				
BT111	20.000000	1.960100	16.024625	0.000000		
EDG011	20.000000	1.037000				
Q26	20.000000	13.927800				
Q1M01	10.000000	-21.000000	6.000000	0.000000	.001000	
Q1M01	10.000000	-22.000000	6.000000	0.000000	.001000	
Q27	20.000000	11.170840				
Q1M15	20.000000	6.800000	1.226398	1.000000		
Q27	20.000000	6.906100				
Q1M30	20.000000	21.800000	-1.616533	1.000000		
Q28	20.000000	21.200000				
Q1M35	20.000000	9.000000	-.030079	1.000000		
Q29	20.000000	9.925400				
ZROT	20.000000	90.000000				
EDG01	20.000000	1.062000				
BT140	20.000000	1.960100	16.402290	0.000000		
EDG01	20.000000	1.062000				
ZROT	20.000000	90.000000				
Q30	20.000000	3.060000				
Q1M50	20.000000	1.040000	3.122869	1.000000		
Q31	20.000000	1.547500				
Q1M52	20.000000	1.060000	-5.158794	1.000000		
Q32	20.000000	1.250000				
Q1M55	20.000000	1.450000	4.165266	1.000000		
Q33	20.000000	1.150000				
Q1M56	20.000000	1.450000	4.165266	1.000000		
Q34	20.000000	1.750000				
Q1M01	10.000000	1.000000	1.000000	.070000	.001000	
Q1M03	10.000000	3.000000	3.000000	.077000	.000100	
Q1M02	10.000000	2.000000	1.000000	0.000000	.001000	
Q1M04	10.000000	4.000000	3.000000	0.000000	.001000	
Q1M013	10.000000	-23.000000	6.000000	0.000000	.001000	

LIST 1 Data list AAD10. Injection line from TT2 to target.
Beam diameter on target 1.5 mm

```

D11MMFILE START 3D102. APH=0 AFTER BTI11. 2MM SPOT ON TARGET 22/05/79 17.47.
SETMOM 10.000000 16.000000 26.000000
EMIT 24.000000 24.000000 .240000 .000100 0.000000
BEAM 1.000000 .594520 -.728385 .772111 .809301100.000000 0.000000
PLOT 22.000000 0.400000 0.000000 200.000000 0.000000 1.000000
INTR 6.000000 0.000000 2.000000
ALPHA1H 14.000000 0.000000
ALPHA1V 1.000000 0.000000 0.000000 0.000000 1.56470
ALPHA2V 0.000000 2.000000
ALPHA3V 1.000000 0.000000 0.000000 0.000000 -1.71660
D0 0.000000 0.000000
D0102 0.000000 1.200000 -.986960 1.000000
D04 0.000000 1.700000
ZR0T1 20.000000 -90.000000
EDG10 0.000000 0.505000
VB101 0.000000 2.200030 6.953090 0.000000
EDG10 0.000000 0.505000
ZR0T1 20.000000 90.000000
D05 0.000000 2.316000
OF103 0.000000 1.200000 .872132 1.000000
EDG11 0.000000 2.371000
HB102 0.000000 1.050000 6.188080 0.000000
JG11 0.000000 0.378000
D07 0.000000 0.004900
D0104 0.000000 1.200000 -.687576 1.000000
D08 0.000000 0.515000
OF105 0.000000 1.200000 .786143 1.000000
D09 0.000000 1.700000
EDG12 0.000000 -.244000
HB103 0.000000 1.400000 -5.286640 0.000000
EDG12 0.000000 -.244000
D10 0.000000 1.553000
D10T2 2.000000 90.000000
EDG13 0.000000 0.505000
VB102 0.000000 2.200030 6.953090 0.000000
EDG13 0.000000 0.505000
ZR0T2 2.000000 -90.000000
D11 0.000000 1.966000
D0106 0.000000 1.200000 -.745900 1.000000
D12 0.000000 7.960000
F107 0.000000 1.200000 .784202 1.000000
D13 0.000000 13.050000
D0208 0.000000 13.020000 -1.019570 1.000000
D14 0.000000 7.940000
F209 0.000000 8.000000 1.006040 1.000000
D15 0.000000 8.430000
D16 0.000000 8.430000 -1.021560 1.000000
D17 0.000000 8.000000 1.006040 1.000000
D18 0.000000 8.430000 -1.021560 1.000000
D19 0.000000 8.000000 1.006040 1.000000
D20 0.000000 8.420000 -1.019570 1.000000
D21 0.000000 8.420000 1.006040 1.000000
D22 0.000000 8.000000
TL11 2.000000 -14.085660
EDG000 0.000000 1.150000
BTI100 0.000000 2.500200 13.952518 0.000000
EDG000 0.000000 1.150000
D22 0.000000 1.750000
EDG001 0.000000 1.150000
BTI101 0.000000 2.500200 13.952518 0.000000
EDG001 0.000000 1.150000
TLBT1 20.000000 14.041900
D23 0.000000 3.229000
QIN05 0.000000 1.800000 -1.101001 -1.000000
D24 0.000000 1.019000
TLT2 20.000000 -14.041900
EDG010 0.000000 1.037000
BTI110 0.000000 1.966100 16.024625 0.000000
EDG010 0.000000 1.037000
D25 0.000000 1.033000
EDG011 0.000000 1.037000
BTI111 0.000000 1.966100 16.024625 0.000000
EDG011 0.000000 1.037000
TLT01 2.000000 13.921800
CJND10 10.000000 21.000000 6.000000 0.000000 .001000
CJND11 10.000000 22.000000 6.000000 0.000000 .001000
D26 0.000000 11.176840
OIN15 0.000000 1.800000 1.215346 1.000000
D27 0.000000 6.900100
OIN30 0.000000 8.000000 -1.531706 1.000000
D28 0.000000 21.200000
OIN35 0.000000 8.000000 .699012 1.000000
D29 0.000000 9.02840
ZR0T 20.000000 90.000000
EDG001 0.000000 1.062000
VBV140 0.000000 1.966100 16.402290 0.000000
EDG001 0.000000 1.062000
ZR0TR 20.000000 -90.000000
D30 0.000000 3.068
OIN50 0.000000 1.000000 2.096061 1.000000
OIN51 0.000000 1.547500
OIN52 0.000000 1.060000 -4.800000 1.000000
OIN53 0.000000 1.250000
OIN55 0.000000 1.250000 4.880198 1.000000
OIN56 0.000000 1.500000 4.880198 1.000000
OIN57 0.000000 1.700000
CJND1 10.000000 1.000000 1.000000 .100000 .001000
CJND3 10.000000 3.000000 3.000000 .100000 .001000
CJND2 10.000000 2.000000 1.000000 0.000000 .001000
CJND4 10.000000 4.000000 3.000000 0.000000 .001000
CJND13 10.000000 23.000000 6.000000 0.000000 .001000
SENTINEL

```

LIST 2 Data list AAD11. Injection line from TT2 to target.
Beam diameter 2 mm on target.

D3HNFIL START QD102. APH=0 AFTER BT111. 3MM SPDT ON TARGET 22/05/79 17.47.52.						
SETMOM	16.000000	16.000000	26.000000			
FEIT	24.000000	.245000	.245000	.000100	0.000000	
BEAM	1.000000	.594620	-.723385	.772111	.809301	1.000000 0.000000
PLOT	22.000000	.400000	0.000000	200.000000	0.000000	1.000000
INTR	6.000000	0.000000	2.000000			
ALPHA IN	14.000000	0.000000				
1.000000	0.000000	0.000000	0.000000	0.000000	1.56470	
ALPHA PIN	14.000000	2.000000				
0.000000	1.000000	0.000000	0.000000	0.000000	-1.71600	
QD	3.000000	0.000000				
QD102	5.000000	1.200000	-9.986960	1.000000		
QD4	3.000000	.700000				
ZROT1	2.000000	-90.000000				
QD10	2.000000	.050500				
QD101	2.400000	2.200030	6.953090	0.000000		
QD10	2.000000	.650500				
ZROT1	2.000000	90.000000				
QD5	3.000000	2.310000				
QD103	3.000000	1.200000	.872132	1.000000		
QD6	3.000000	2.371000				
EDGE11	2.000000	.378000				
HR102	2.000000	1.856000	6.188080	0.000000		
QD11	2.000000	.378000				
QD7	2.000000	0.694900				
QD104	3.000000	1.200000	-6.687576	1.000000		
QD8	3.000000	8.515000				
QD9	3.000000	1.200000	.848603	1.000000		
QD12	2.000000	.700000				
QD103	2.000000	1.400000	-5.286640	0.000000		
QD12	2.000000	1.244000				
QD10	2.000000	1.553000				
ZROT2	2.000000	90.000000				
QD13	2.000000	.050500				
QD102	2.400000	2.200030	6.953090	0.000000		
QD13	2.000000	.650500				
ZROT2	2.000000	-90.000000				
QD106	3.000000	1.900000				
QD11	3.000000	1.200000	-.745900	1.000000		
QD12	3.000000	7.960000				
QD107	3.000000	1.200000	.752495	1.000000		
QD13	3.000000	13.680000				
QD208	3.000000	7.820000	-1.619570	1.000000		
QD14	3.000000	7.940000				
QD209	3.000000	8.000000	1.006040	1.000000		
QD15	3.000000	8.430000				
QD210	3.000000	8.600000	-1.021560	1.000000		
QD16	3.000000	8.430000				
QD211	3.000000	8.600000	1.006040	1.000000		
QD17	3.000000	8.430000				
QD212	3.000000	8.600000	-1.021560	1.000000		
QD18	3.000000	8.430000				
QD213	3.000000	8.600000	1.006040	1.000000		
QD19	3.000000	8.430000				
QD214	3.000000	8.600000	-1.019570	1.000000		
QD20	3.000000	8.430000				
QD215	3.000000	8.600000	1.006040	1.000000		
QD22	3.000000	8.430000				
QD11	2.000000	-14.000000				
QD6000	2.000000	1.150000				
TI100	2.000000	2.500000	13.952518	0.000000		
QD5000	2.000000	1.150000				
QD101	2.000000	1.150000				
QD101	2.400000	2.500000	13.952518	0.000000		
QD101	2.000000	1.150000				
QD101	2.000000	1.150000				
QD105	2.000000	14.041900				
QD24	2.000000	3.229000	.051951	1.000000		
QD10	2.000000	1.019000				
QD10	2.000000	-14.041900				
QD10	2.000000	1.037000				
QD10	2.000000	1.900100	16.024625	0.000000		
QD10	2.000000	1.037000				
QD10	2.000000	1.633000				
QD10	2.000000	1.037000				
QD10	2.000000	1.960100	16.024625	0.000000		
QD10	2.000000	1.037000				
QD10	2.000000	13.427900				
QD10	10.000000	-21.000000	6.000000	0.000000	.001000	
QD10	10.000000	22.000000	0.000000	0.000000	.601000	
QD26	3.000000	11.170840				
QD15	3.000000	8.800000	.984085	1.000000		
QD27	3.000000	6.900160				
QD130	3.000000	8.800000	-.991106	1.000000		
QD28	3.000000	3.000000	3.000000	2.000000	.001000	
QD135	3.000000	21.200000				
QD29	3.000000	8.000000	1.284056	1.000000		
QD30	3.000000	9.02840				
QD35	10.200000	1.000000	1.000000	1.400000	.001000	
ZROT	20.000000	90.000000				
QD30	2.000000	1.062000				
QD140	2.000000	1.960100	16.402290	0.000000		
QD30	2.000000	1.062000				
ZROT	20.000000	-90.000000				
QD30	3.000000	3.068000				
QD150	3.000000	1.060000	0.000000	1.000000		
QD31	3.000000	.547500				
QD152	3.000000	1.060000	-2.97235	1.000000		
QD32	3.000000	1.250000				
QD155	3.000000	.450000	5.489062	1.000000		
QD33	3.000000	.150000				
QD156	3.000000	.450000	5.489062	1.000000		
QD34	3.000000	1.700000				
QD31	10.000000	1.000000	1.000000	.150000	.001000	
QD32	10.000000	3.000000	3.000000	.150000	.001000	
QD33	10.000000	1.000000	1.000000	0.000000	.001000	
QD34	10.000000	3.000000	3.000000	0.000000	.001000	
QD35	10.000000	1.000000	1.000000	0.000000	.001000	
QD36	10.000000	3.000000	3.000000	0.000000	.001000	
SENTINEL	10.000000	-23.000000	0.000000	0.000000	.001000	

LIST 4 Data list AAD3. Injection line from TT2 to target.
Beam diameter on target 3 mm. Solution 2.

```

DISOL1      AAD1 FINAL VERSION 25/4/79 TARGET TO AA RING      16/05/79  12.21.22.
P           16.000000 16.000000 3.575200
*EMITT*     24.000000 10.000000 10.000000 75.000000 0.000000
*BEAM*      1.000000 2.200000 0.000000 2.200000 0.000000 100.000000 0.000000
*SP CM*     22.000000 0.250000 0.000000 200.000000 0.000000 1.000000
*SLIT*      0.000000 0.000000 2.000000
D           3.000000 2.810000
60          5.010000 1.160000 -.457392 1.000000
65          3.000000 1.340000
66          5.010000 1.160000 .440517 1.000000
67          3.000000 0.459600
68          2.000000 2.250000
69          4.000000 1.140300 8.213910 0.000000
70          3.000000 2.250000
71          3.000000 7.849600
75          5.010000 1.160000 -.234131 1.000000
76          3.000000 0.840000
80          5.010000 1.160000 .151600 1.000000
81          3.000000 8.160000
85          5.010000 1.160000 .127873 1.000000
86          3.000000 3.920000
90          5.010000 1.160000 -.203178 1.000000
91          3.000000 3.420000
95          5.010000 1.160000 .148980 1.000000
96          3.000000 8.052200
97          2.000000 6.500000
98          4.000000 0.900000
99          2.000000 -3.549270
100         2.000000 3.575000
101         2.000000 3.549270
102         4.000000 0.750000 2.548112334.312000
103         3.000000 -2.614410
104         3.000000 0.575000
105         2.000000 2.614410
106         4.000000 0.900000 6.820000 0.000000
107         2.000000 0.330000
108         3.000000 3.920500
COND1      10.000000 1.000000 1.000000 4.318970 .001000
COND2      10.000000 2.000000 2.000000 4.050810 .001000
COND3      10.000000 3.000000 3.000000 2.816190 .001000
COND4      10.000000 4.000000 4.000000 3.713300 .001000
COND5      10.000000 -21.000000 6.000000 .109000 .001000
COND6      10.000000 -22.000000 6.000000 .063000 .001000
SENTINEL

```

LIST 5 Data list AAD1. Injection line. Target to AA ring

D7SOL1

AA EJECTION-FINAL

14/06/79 08.58.16.

PERMIT	16.000000	16.000000	3.575200			
BEAM	24.000000	.140000	.100000	.000010	0.000000	
BL0T	1.000000	.511027	-.826547	.251819	-.294713	1.000000 0.000000
INTRP	22.000000	.500000	0.000000	0.000000	0.000000	1.000000
INTAP	6.000000	0.000000	2.000000			
INTAPP	14.000000	1.000000	0.000000	0.000000	0.000000	-.07450
DO	0.000000	0.000000	0.000000	0.000000	0.000000	.03890
DO1	1.000000	0.000000	0.000000			
DO2	3.000000	3.920500				
DO3	3.000000	-.215000				
DO4	4.000000	.900000	-6.824000	0.000000		
DO5	4.000000	-2.736000				
DO6	2.000000	.575000				
DO7	2.000000	2.736000				
DO8	4.000000	.750000	-2.259410	425.200000		
DO9	4.000000	-3.549000				
DO10	3.000000	.575000				
DO11	3.000000	3.549000				
DO12	4.000000	.900000	-6.824000	0.000000		
DO13	4.000000	-6.500000				
DO14	7.000000	7.160000				
DO15	1.000000	.500000	.831380	1.000000		
DO16	1.000000	1.700000				
DO17	1.000000	.500000	-.908389	1.000000		
DO18	2.000000	.612900				
DO19	2.000000	-17.559700				
DO20	2.000000	-6.859600				
DO21	4.000000	1.964700	-14.534070	0.000000		
DO22	2.000000	-6.859600				
DO23	2.000000	17.043200				
DO24	3.000000	3.092900				
DO25	3.000000	.500000	.951020	1.000000		
DO26	4.000000	4.090000				
DO27	3.000000	.500000	-.686993	1.000000		
DO28	1.000000	3.000000	3.000000	.800000	.100000	
DO29	5.000000	5.300000				
DO30	1.000000	.500000	.836143	1.000000		
DO31	1.000000	1.000000	1.000000	.750000	.100000	
DO32	3.000000	3.040000				
DO33	3.000000	.500000	-.986792	1.000000		
DO34	5.000000	5.920000				
DO35	3.000000	.500000	1.056610	1.000000		
DO36	3.000000	.635500				
DO37	2.000000	-15.316947				
DO38	2.000000	7.580000				
DO39	2.000000	1.964690	16.056152	0.000000		
DO40	2.000000	7.580000				
DO41	2.000000	15.683200				
DO42	3.000000	.782700				
DO43	3.000000	.500000	-1.050000	1.000000		
DO44	3.000000	1.713000				
DO45	3.000000	.500000	.660174	1.000000		
DO46	6.000000	6.752200				
DO47	3.000000	.500000	.361335	1.000000		
DO48	3.000000	3.856000				
DO49	5.000000	.500000	-.339440	1.000000		
DO50	1.000000	-21.000000	0.000000	0.000000	.001000	
DO51	1.000000	-22.000000	6.000000	0.000000	.001000	
DO52	1.000000	-23.000000	6.000000	-.507626	.001000	
DO53	1.000000	-24.000000	6.000000	-.134760	.001000	
DO54	1.000000	1.000000	1.000000	.374160	.001000	
DO55	1.000000	2.000000	1.000000	0.000000	.001000	
DO56	1.000000	3.000000	3.000000	.665000	.000100	
DO57	1.000000	4.000000	3.000000	0.000000	.001000	
DO58	3.000000	1.000000				
SENTINEL						

LIST 6 Data list AAD7. Ejection line.

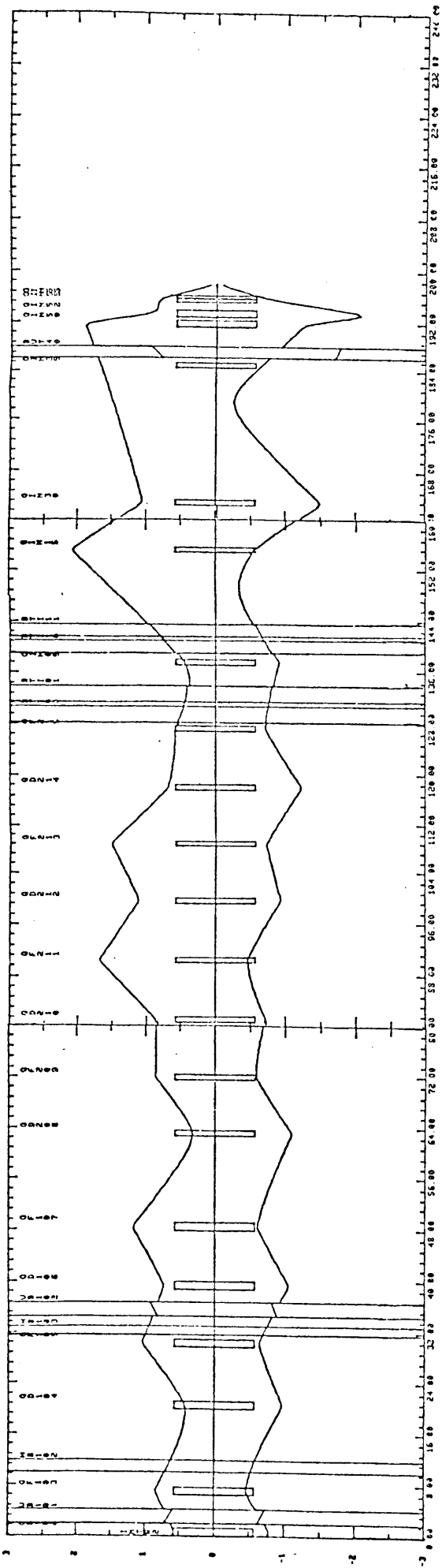


Fig. 1. Beam Envelopes from TT2 to target. Beam diameter on target 1.5 mm LIST 1. Data set AAD10

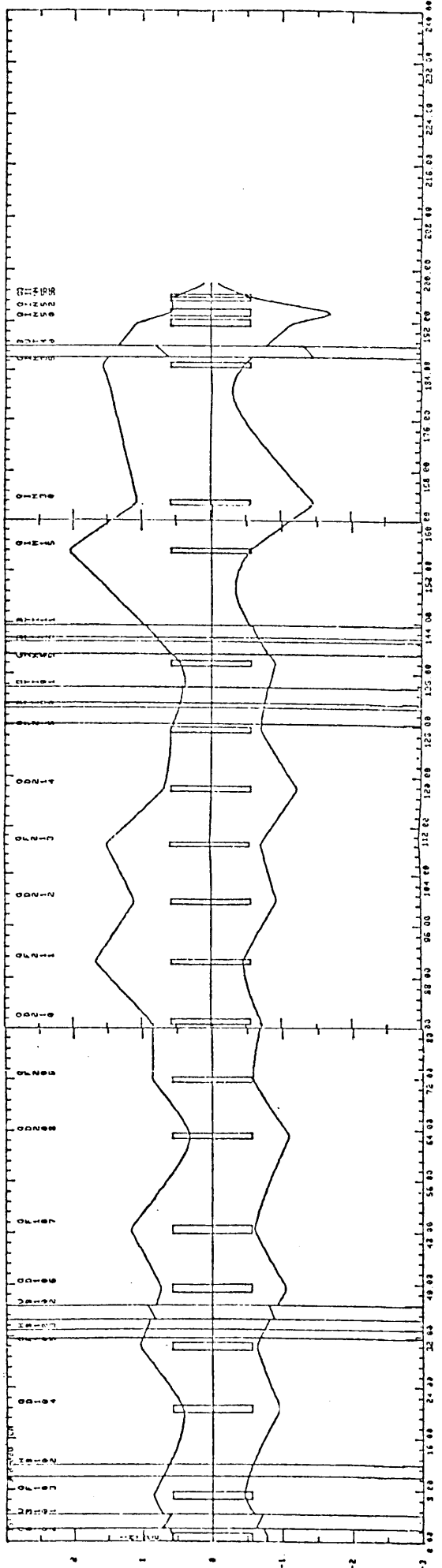


Fig. 2. Beam Envelopes from TT2 to target. Beam diameter on target 2.0 mm LIST 2. Data set AAD11

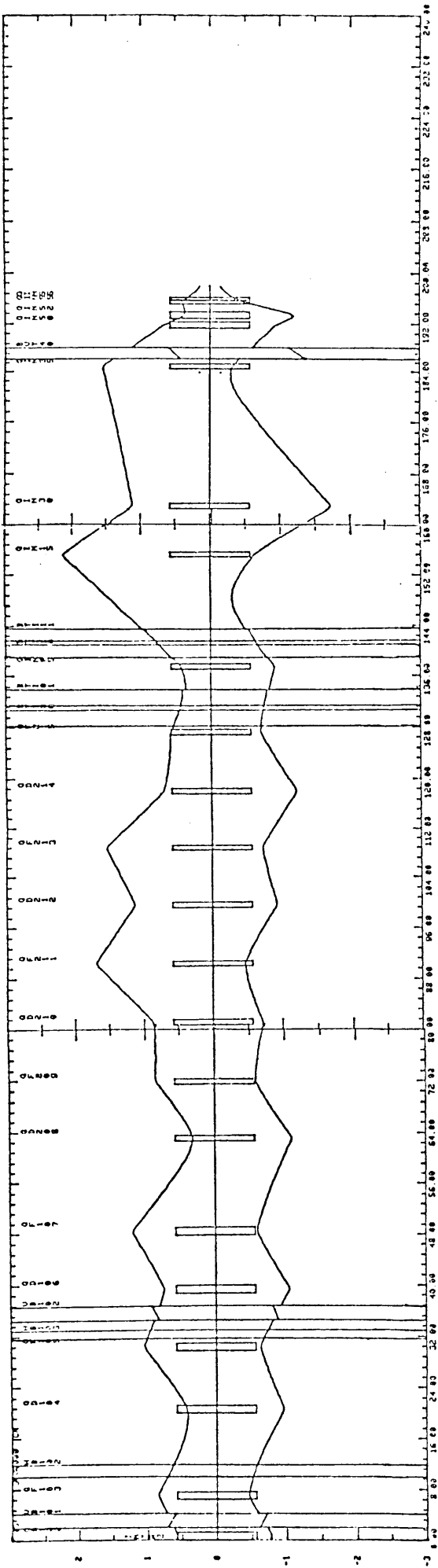


Fig. 3. Beam Envelopes from TT2 to target. Beam diameter on target 3.0 mm LIST 3. Data set ADD12 Solution 1

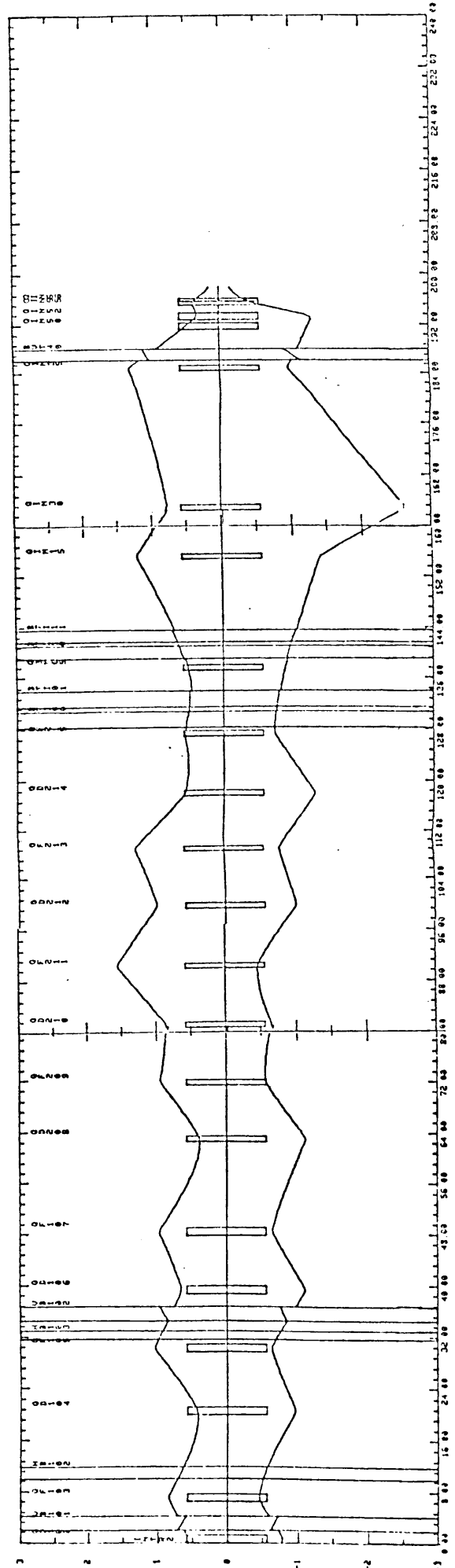


Fig. 4. Beam envelopes from TT2 to target. Beam diameter on target 3.0 mm LIST 4. Data set AAD3 Solution 2

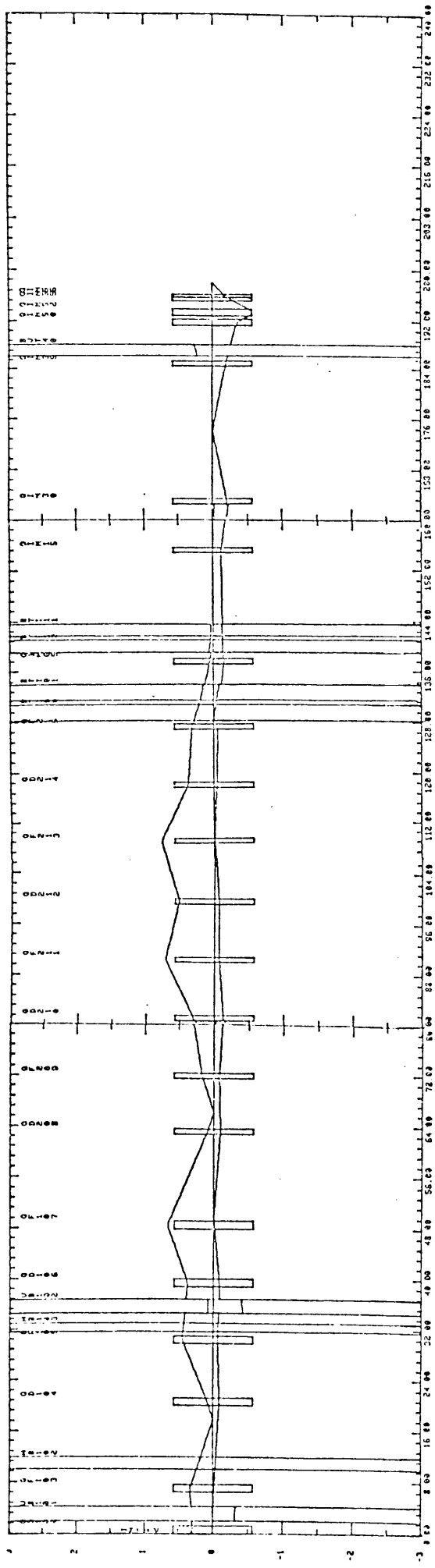


Fig. 7. Momentum Vectors $dp/p = 0.2\%$ See Fig. 1

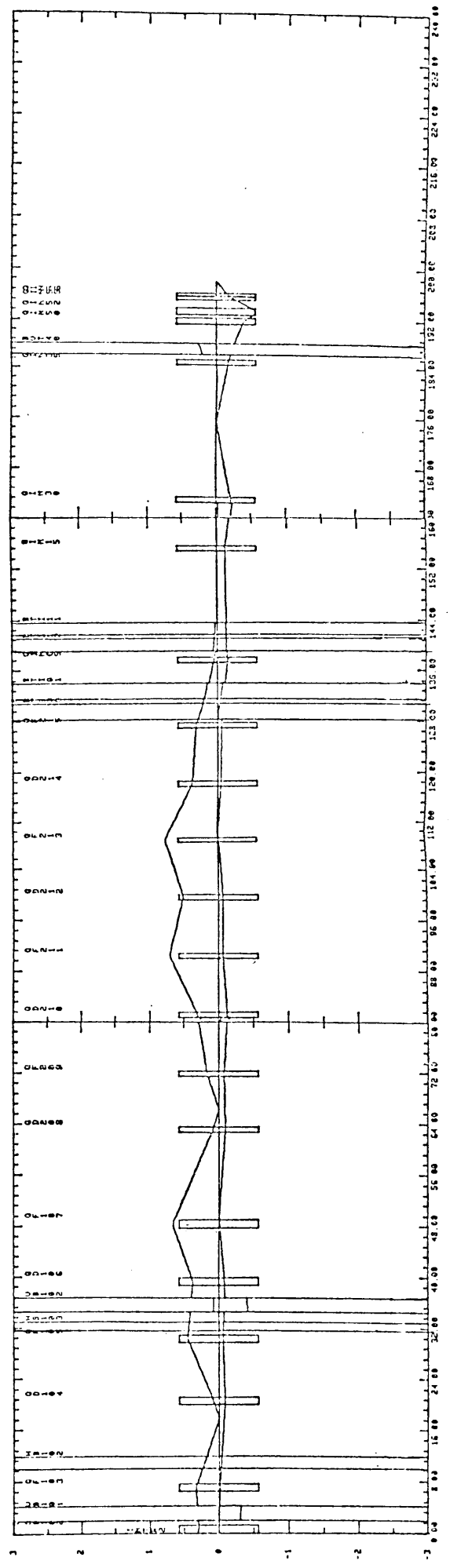


Fig. 8. Momentum Vectors $dp/p = 0.2\%$ See Fig. 2

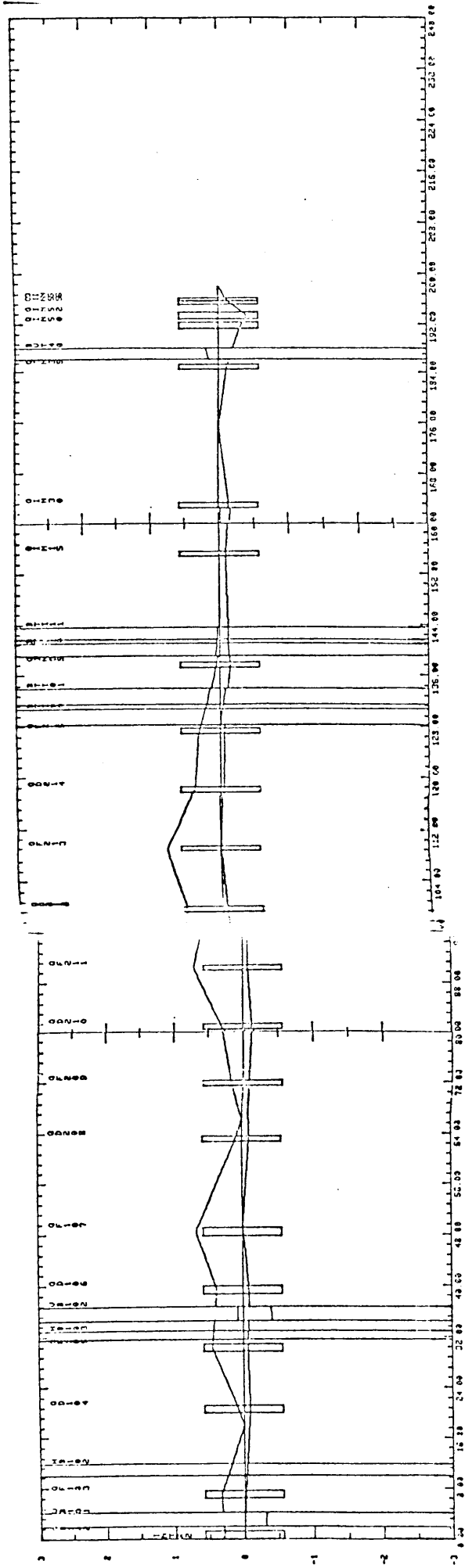


Fig. 9. Momentum Vectors $dp/p = 0.2\%$. See Fig. 3.

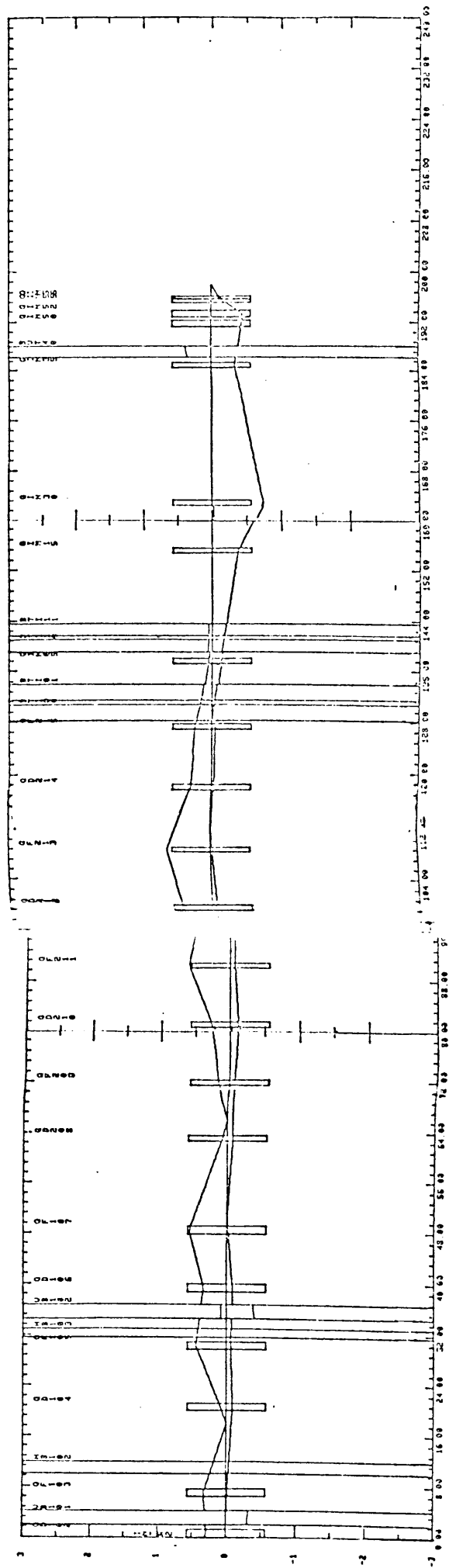


Fig. 10. Momentum Vectors $dp/p = 0.2\%$. See Fig. 4.

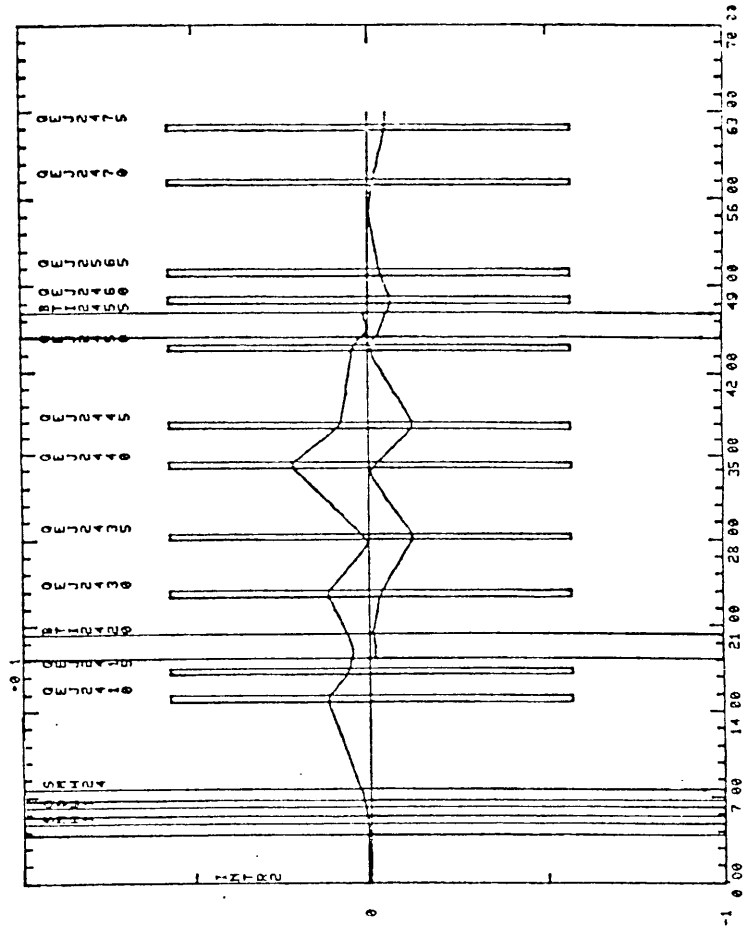


Fig. 11. Momentum Vectors $dp/p = 0.75\%$ See Fig. 5

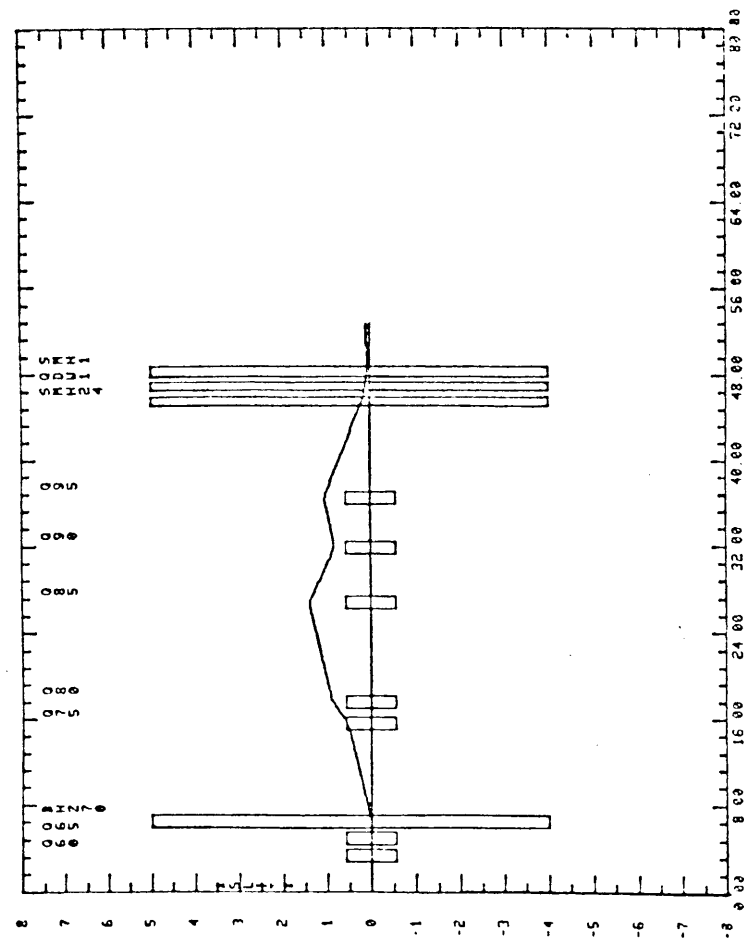


Fig. 12. Momentum Vectors $dp/p = 0.1\%$ See Fig. 6

Name	Type Origin	Pole tip Diameter (mm)	Vacuum tube ID	Plane	Required Aperture	Required Strengths σ in KG/cm ² , Km ²	Required Current	Available Current
QIN0060	Q100 PS	200	152	H V	72 52	-0.4574 0.3835	230.2	430
QIN0065	Q100 PS	200	152	H V	97 40	0.4405 -0.3694	221.7	430
QIN0075	Q100 PS	200	152	H V	70 137	-0.2341 0.1963	117.8	250
QIN0080	Q100 PS	200	152	H V	104 118	0.1516 -0.1271	76.3	150
QIN0085	Q100 PS	200	152	H V	142 98	0.1279 -0.1072	64.4	150
QIN0090	Q100 PS	200	152	H V	102 142	-0.2032 -0.1704	102.3	150
QIN0095	Q100 PS	200	152	H V	132 82	0.1490 -0.1249	75.0	150

Quadrupole Magnet - Operating Requirements - Injection Line Target to AA Ring

e n	Pole tip diameter (mm)	Vacuum tube I.D.	Plane	Required Aperture	Required Strength G in K/gm, K in m ²	* Required Current	Available Current
	80	75	H V	13 7	G K 0.8314 -0.6977	80.4	150
	80	75	H V	6 13	G K -0.9084 0.7617	87.9	150
	80	75	H V	8 3	G K 0.9570 -0.7974	92.0	150
	80	75	H V	4 12	G K -0.8870 0.7438	85.8	150
	80	75	H V	16 3	G K 0.8361 -0.7011	80.9	150
	80	75	H V	6 8	G K -0.9868 0.8274	95.4	150
	80	75	H V	8 4	G K 1.0567 -0.8860	102.2	150
	80	75	H V	4 11	G K -7.0500 0.8804	101.5	150
	80	75	H V	9 6	G K 0.6602 -0.5536	63.8	150
	80	75	H	13	G 0.3613	34.9	150

