

Destructive breakdown studies of irradiated LGADs at beam tests for the ATLAS HGTD

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ABSTRACT:

In the past years, it has been observed at several beam test campaigns that irradiated LGAD sensors break with a typical star shaped burn mark when operated at voltages much lower than those at which they were safely operated during laboratory tests. The study presented in this paper was designed to determine the safe operating voltage that these sensors can withstand. Many irradiated sensors from various producers were tested in two test beam facilities, DESY (Hamburg) and CERN-SPS (Geneva), as part of ATLAS High Granularity Timing Detector (HGTD) beam tests. The samples were placed in the beam and kept under bias over a long period of time in order to reach a high number of particles crossing each sensor. Both beam tests lead to a similar conclusion, that these destructive events begin to occur when the average electric field in the sensor becomes larger than $12 \text{ V}/\mu\text{m}$.

KEYWORDS: LGAD, Silicon sensors, Timing detectors, HL-LHC, ATLAS, HGTD

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1 Introduction

During the high-luminosity phase of the LHC (HL-LHC), the primary interactions created in proton-proton collisions are accompanied by a large number of zero and minimum bias interactions (pileup). In order to mitigate the adverse effects of pileup, the ATLAS experiment will install the High Granularity Timing Detector (HGTD) [1]. In particular, the high-precision track timing information from HGTD will allow for the proton-proton collisions to be distinguished in time. HGTD will use Low Gain Avalanche Detectors (LGADs) [2, 3]. LGADs provide low gain, typically to the order of several tens, by using a n^{++} - p^+ - p - p^{++} structure to create electric fields high enough for impact ionization to occur at the n^{++} - p^+ junction. The doping concentration and profile shape of the gain layer impacts the gain factor of the detector.

The harsh radiation environment at the HL-LHC, particularly in the forward region (corresponding to a pseudorapidity¹, η , range of $2.8 < \eta < 4.0$) where HGTD will operate, will lead to the deterioration of LGAD performances. The main concern is the so-called initial acceptor removal [4], which reduces the gain and requires an increase of bias voltage to compensate for the loss

¹The ATLAS experiment uses a right-handed coordinate system with its origin at the nominal interaction point (IP) in the center of the detector, and the z -axis along the beam line. The x -axis points from the IP to the center of the LHC ring, and the y -axis points upwards. Cylindrical coordinates (r, ϕ) are used in the transverse plane, ϕ being the azimuthal angle around the z -axis. Observables labelled “transverse” are projected onto the $x - y$ plane. The pseudorapidity is defined in terms of the polar angle θ as $\eta = -\ln \tan \theta/2$.

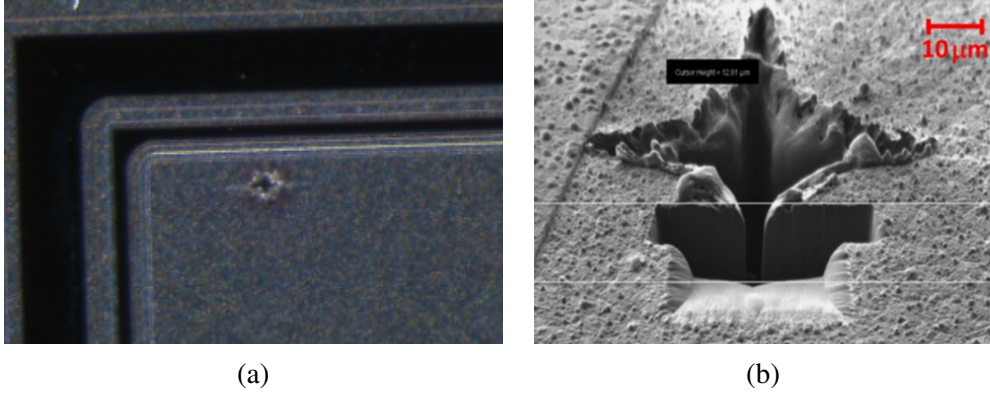


Figure 1: (a) Typical star shaped burn mark observed in beam test sensor mortalities due to SEB. Sensor pictured here is from run HPK-P2 wafer 31 irradiated to $2.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$, whose mortality occurred at the DESY beam test. (b) Microscopic photograph of a typical burn mark, observed in ATLAS proton beam tests at Fermilab in 2018 in a CNM LDA35 sensor (courtesy of CNM) [7].

of acceptors in the gain layer. By the end of their lifetime at HGTD the most exposed sensors will have received a 1 MeV neutron equivalent fluence of around $\Phi_{eq} = 2.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$. This would require operation of sensors at voltages exceeding 700 V at $-30 \text{ }^\circ\text{C}$ for a sensor active area thickness of $50 \text{ }\mu\text{m}$. It has been shown in the laboratory using strontium-90 electrons that in such conditions enough charge is collected and the targeted time resolution of 35 (70) ps at the start (end) of their lifetime. The minimal bias voltage under which each sensor reaches the 4 fC charge threshold was first measured in the laboratory using a strontium-90 source.

The HGTD beam test campaigns at CERN-SPS [5] (120 GeV pions) and DESY [6] (3 GeV electrons) aimed to reproduce the strontium-90 measurements. Many of the sensors underwent destructive breakdown at voltages that were $\sim 100 \text{ V}$ lower than those at which the sensors were successfully operated in laboratory tests. A typical star shape burn mark, see figure 1, appeared in the location of the particle hitting the sensors.

An intensive investigation done within the ATLAS, CMS and RD50 Collaborations [8, 9] led to the conclusion that a single beam particle hitting the detector is responsible for the sensor destruction. Both ATLAS and CMS recorded the signal from such events and associated the location of the crater with the hit position reconstructed by the beam telescope. An example is shown in figure 2. Studies with high-power 50 fs laser pulses were performed [10] and also confirmed the destructive events at high bias voltages.

The mechanism of the destruction is called single event burnout (SEB) [11] and will be schematically described in the next section. However, it was not clear what the parameters determining its occurrence were. In order to answer that question a large set of sensors from various producers with different thicknesses of the active material, D, irradiation levels, annealing stages and gain layer designs, were tested in two different beam test campaigns at DESY and SPS, in 2021. This paper describes the result of these studies.

ATLAS HGTD

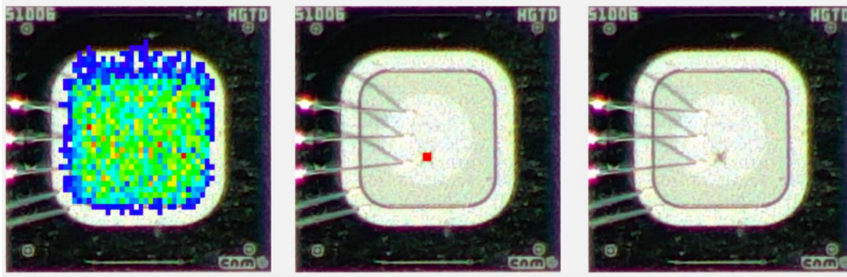


Figure 2: The right plot shows a typical single event burnout mark from a 2019 DESY beam test with 5 GeV electrons. The reconstructed track in the destructive event pointed to the location of the burn mark (middle and right plot). The distribution of all the reconstructed tracks across the detector before destruction is shown in the left plot.

2 Single event burnout

The most probable cause of the sensor mortalities observed is the mechanism known as SEB. Laboratory tests use a beta beam from a strontium-90 source which have significantly less energy than the test beams. The maximum energy of a strontium-90 electron is 2.3 MeV which sets the maximum deposited charge in the LGAD sensor. On the other hand, the deposited charge from a high-momentum particle beam in the active zone of the LGAD detector can be much larger. According to GEANT4 [12] simulations up to 100 MeV can be deposited by a single charged hadron [9, 13]. This leads to the generation of a large density of carriers. The screening effect created by such a large carrier density then prevents carriers from being swept away, leading to a change in the local resistivity such that the sensor becomes conductive [11]. The field collapses in the region of high free carrier density, leading to an increased voltage drop in the region where density is lower. The increase of the field there leads to avalanche breakdown (field exceeds the critical field). The charge stored on the sensor electrodes as well as on the high voltage (HV) filtering capacitor (typically 10 nF) is discharged through the sensor. The energy available in such a discharge is enough to melt the silicon, creating a crater and damaging the sensor. The breakdown is eventually quenched, but the sensor is permanently damaged. This mechanism is illustrated in figure 3.

3 Test beam set-up

The SEB events were initially observed in sensors being operated in test beam lines where occasionally the signals from the fatal events were recorded. In order to maximise the number of sensors that can be tested at a given beam test campaign, a printed circuit board (PCB) was designed that could host two sensors of different sizes. Figure 4 shows the circuit diagram of the boards, and the five connections to the boards. The current was measured as a voltage drop on the bias resistor. The resistor is either 30 k Ω or 100 k Ω based on the size of the sensors; smaller resistance for larger-sized sensors. A 2 nF capacitor was used to simulate the full sensor capacitance, while the circuitry in figure 4a prevented the voltage drop from exceeding the maximum tolerable at the analog-to-digital

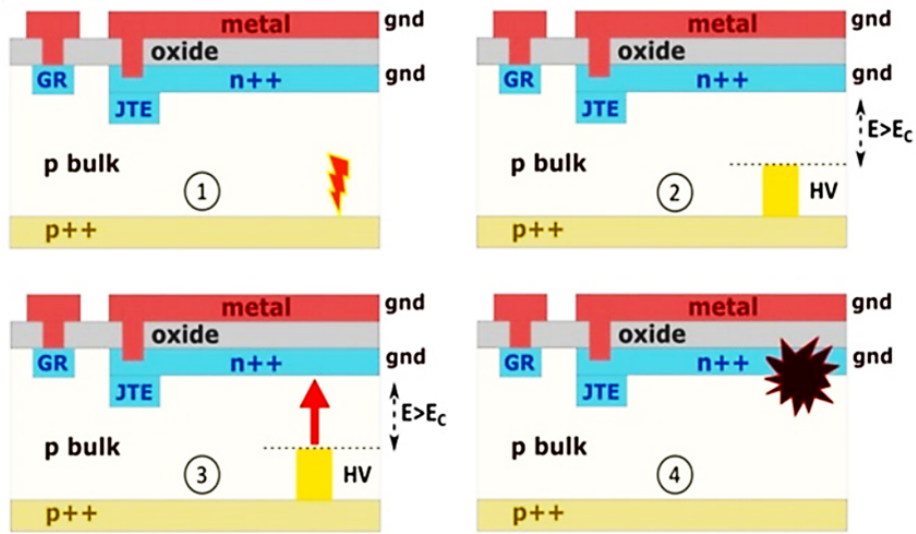


Figure 3: Scheme of the SEB mechanism in an LGAD [11]. (1) A large amount of energy is deposited in the sensor. (2) Large carrier density leads to collapse of the field. (3) The HV is brought closer to the pad leading to very high field strength. (4) Avalanche breakdown leads to destruction of the sensor.

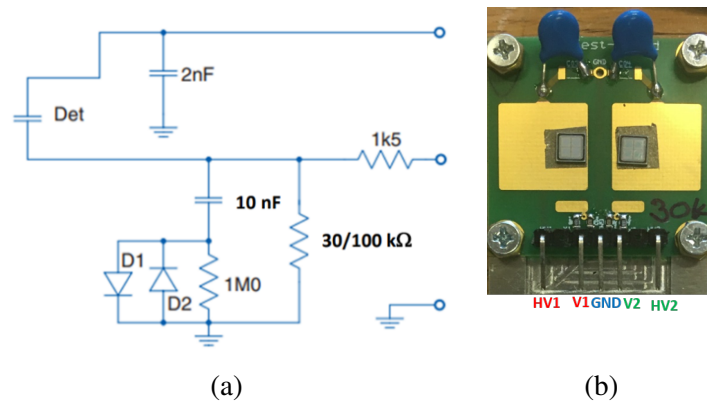


Figure 4: (a) Circuit diagram of a single channel of the PCB. (b) Photograph of the PCB, showing the five connections for: bias applied to the left sensor (HV1), the voltage output of the left sensor (V1), ground (GND), the voltage output of the right sensor (V2), and the bias applied to the right sensor (HV2).

converter (ADC) input. Up to eight PCBs, i.e. 16 sensors, were aligned to one another with the use of mechanical rails, as shown in figure 5.

A CAEN N472 HV power supply, which has four HV channels, was used to apply the bias to the sensors. To allow for more than one sensor to be biased by one HV channel the HV was first taken to an external box where it is split to allow up to seven connections per HV channel. Flat cables carried the HV to each of the PCBs. A major benefit of this design is that when a sensor broke it simply needed to be disconnected from this box and all the other sensors connected to the

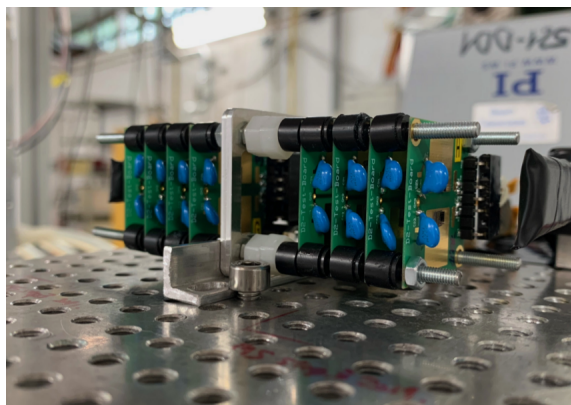


Figure 5: The eight PCBs are placed one in front of the other on a frame, and placed directly in the beam. A scintillator and PMT placed in front of the train of boards record the beam rate. Another scintillator and PMT are placed behind the train. The coincidence of both was used to align the sensors in the beam.

same HV channel could continue to be operated.

A NI-USB 6001 DAQ system was used to measure the voltage drop on the sensors, as well as the HV channels, temperature and humidity. This setup was used at both beam tests. At DESY dry ice was used to cool down the sensors. Since the temperature increases as the dry ice evaporates, detailed temperature measurement was kept throughout testing, which required a dedicated HV channel. 3 HV channels were used for sensor testing. The HV was applied only while the temperature was between -40°C to -25°C . At the SPS the cooling box used a chiller to keep the temperature stable at -30°C , which is the planned operating temperature of the HGTD in the ATLAS detector, and so the choice was made to measure 4 HV channels and just monitor the temperature by using an external sensor placed inside the cooling box.

In both beam tests, a 1 cm^2 scintillator read out by a photo multiplier tube (PMT) placed in front of the train of sensors recorded the beam rate, which allowed for the number of particles crossing through each sensor to be calculated. This scintillator was used together with a second scintillator placed behind the train of sensors to align the sensors in the beam by moving the platform to observe where the coincidence rate was maximum.

4 Sensors

4.1 LGAD samples

The ATLAS sensors will consist of 15×15 LGAD arrays of $1.3\times 1.3\text{ mm}^2$ pads. For the tests performed here other pad structures are used such as single-pads and 2×2 and 5×5 arrays. A complete list of the sensors sent to the beam tests and their properties is given in appendix A. A set of sensors from different runs and wafers, produced by HPK², IHEP-IME³, CNM⁴, FBK⁵,

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NDL⁶ and USTC-IME⁷, were chosen to test a wide variety of LGAD properties. The sensors also vary in size, active material thickness and in the radiation level they were subjected to, all given in the tables 1 and 2. Irradiation fluence is given as the 1 MeV neutron equivalent [14]. All of the sensors were irradiated with reactor neutrons at the Jozef Stefan Institute's TRIGA II research reactor [15]. Most of the sensors were then annealed for 80 min at 60 °C, unless otherwise stated. Of the sensors tested, USTC-IME-1.1 wafer 11 sensors, all FBK sensors and all IHEP-IMEv2 sensors are carbon-enriched [16] while the rest are not.

A few sensors were studied for more specific reasons. The HPK-P1 sensors of type-3.1 and 3.2 were annealed for an extremely long time, and for this reason were chosen in order to test if annealing time would have any impact on the occurrence of mortality. The performance of these type-3.1 and 3.2 sensors were tested at HGTD beam tests in 2018 and 2019 [17]. HPK-P1 sensors of type-1.1 and 1.2 were chosen to give a clearer picture if mortality was impacted by the sensor active material thickness, as they are thinner than the more recently produced LGADs at 35 μm versus the more typical $\sim 50 \mu\text{m}$. Lastly, irradiated Positive Intrinsic Negative (PIN) diodes were chosen in order to determine if gain had an impact on the mortality.

4.2 Testing process

In total, 32 samples were sent to DESY and were measured in two batches of 16 sensors across two weeks. Those that survived the DESY test beam were sent to the SPS test beam. In total, 42 sensors were sent to SPS and measured in four batches altogether, again across two weeks. In each case, the sensors were grouped up in such a way that sensors requiring similar biases to achieve the 4 fC requirement for the HGTD [1] were connected on the same HV channel. The bias of each HV channel was then increased until it was high enough to reach 4 fC for the best performing sensor. The sensors were left for a significant amount of time in the beam, so as to acquire a high number of particles crossing the sensor. At DESY, where the particle rate was approximately 2 kHz/cm² through the entire beam test period, the sensors were left in the beam for 6 to 8 hours so as to reach a total of about a million particles crossing each sensor pad in this time. At the SPS, the rate was less stable but overall significantly higher, reaching up to more than 6 kHz/cm² at times, so most sensors received many millions of particles per pad. Once at least 10⁶ events had been reached, the bias was increased by about 20 V. This was repeated until either the sensor broke or a bias well above the one required to achieve the 4 fC charge requirement was reached. Sensor breakdown was identified through a current divergence.

5 Results and discussion

An example of the plots produced from the recorded data is shown in figure 6. Figure 6a shows the current of a HPK-P2 W25 2×2 sensor as a function of time measured during the DESY beam test. It can be clearly seen that the current gradually rises over time and this is due to the temperature increase as the dry ice evaporates, as previously described. There is also a large spike in the current at 90 hours which indicates that the sensor broke. Figure 6b shows the current of a IHEP-IMEv2 W4-II 1×3 sensor as a function of time measured during the SPS beam test. The current stays steady

⁶Novel Device Laboratory, China.

⁷University of Science and Technology of China and Institute of Microelectronics, China.

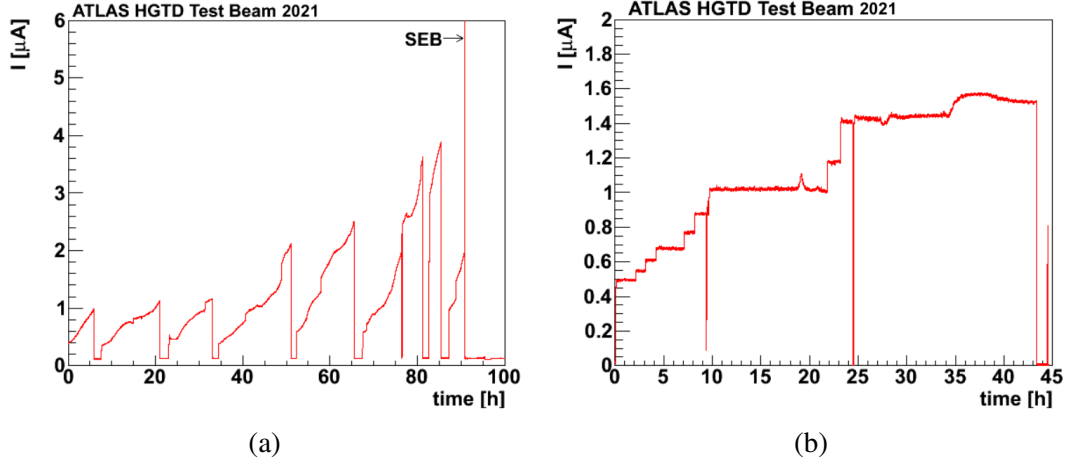


Figure 6: Example of the plots produced from the data obtained at the beam tests. (a) The current of a HPK-P2 W25 SE3-IP4 2x2 sensor irradiated to $1.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$ measured at DESY. It broke at 90 hours. (b) The current of a IHEP-IMEv2 W4-II 1x3 sensor irradiated to $1.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$ measured at SPS.

over time in comparison to the sensor measured at DESY due to the stable temperature. In both plots, each pause in the current is due to the HV being switched off for reasons such as replacing the dry ice (at DESY only) or removing a broken sensor from the same HV channel. Each large jump in current is caused by the bias being stepped up as part of the testing plan.

The results of both beam tests are represented in figure 7. The graph shows the bias voltage required for the minimum required charge of 4 fC (when known from strontium-90 measurements in the laboratories), the lowest bias tested, and the highest bias tested. For the sensors that broke it also marks the bias at which it failed. Based on these results, the sensors that are able to reach the bias required for 4 fC are HPK-P2 W25 and USTC-IME irradiated to $1.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$, and IHEP-IMEv2 and FBK-UFSD3.2 irradiated to both $1.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$ and $2.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$. The USTC-IME-1.1 wafer 11, IHEP-IMEv2 and FBK sensors are carbon-enriched. None of the NDL nor CNM sensors reached the required bias.

In order to determine the conditions under which a sensor breaks in the beam, various active material thicknesses are compared against the last bias and the electric field, both shown in figure 8.

As can be seen, sensors with a larger active material thickness were able to withstand a higher bias, and when an average field in the sensors is calculated, $\langle E \rangle = V_{bias}/D$, they start to break once they reach $12 \text{ V}/\mu\text{m}$ regardless of the LGAD design. This explains why the sensor from FBK-UFSD3.2 wafer 7 (active thickness $55 \mu\text{m}$) irradiated to $2.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$ survived at biases well above 600 V while sensors from other FBK wafers (active thickness $45 \mu\text{m}$) irradiated to $2.5 \times 10^{15} \text{ n}_{eq}/\text{cm}^2$ did not. No fatality was observed at $E < 12 \text{ V}/\mu\text{m}$, although this observation is with a limited number of particles crossing the detector. However, to account for uncertainty and the fact that breakdown depends exponentially on the field, a safe zone of operation of $E < 11 \text{ V}/\mu\text{m}$ is proposed.

For the sensors that did not survive, the probability of mortality per particle crossing the sensor can be calculated. The number of particles crossing the 1 cm^2 scintillator was recorded, and this

value was scaled down to the number of particles that crossed a single-pad of each sensor. The probability was then calculated as the inverse of the number of particles that passed through the sensor pad before it broke. The precision with which the rate, and therefore the number of particles, is known is better than 50% due to the control of the beam profile and the efficiency of the particle scintillator counter. The probabilities are presented in figure 9 and are generally in the range of $10^{-5} - 10^{-6}$. As would be expected, the sensors that broke at a bias of 680 V have the highest probability of mortality. However, these sensors were not tested at biases below 680 V, so it is possible that they would have broken at a lower bias with a lower probability.

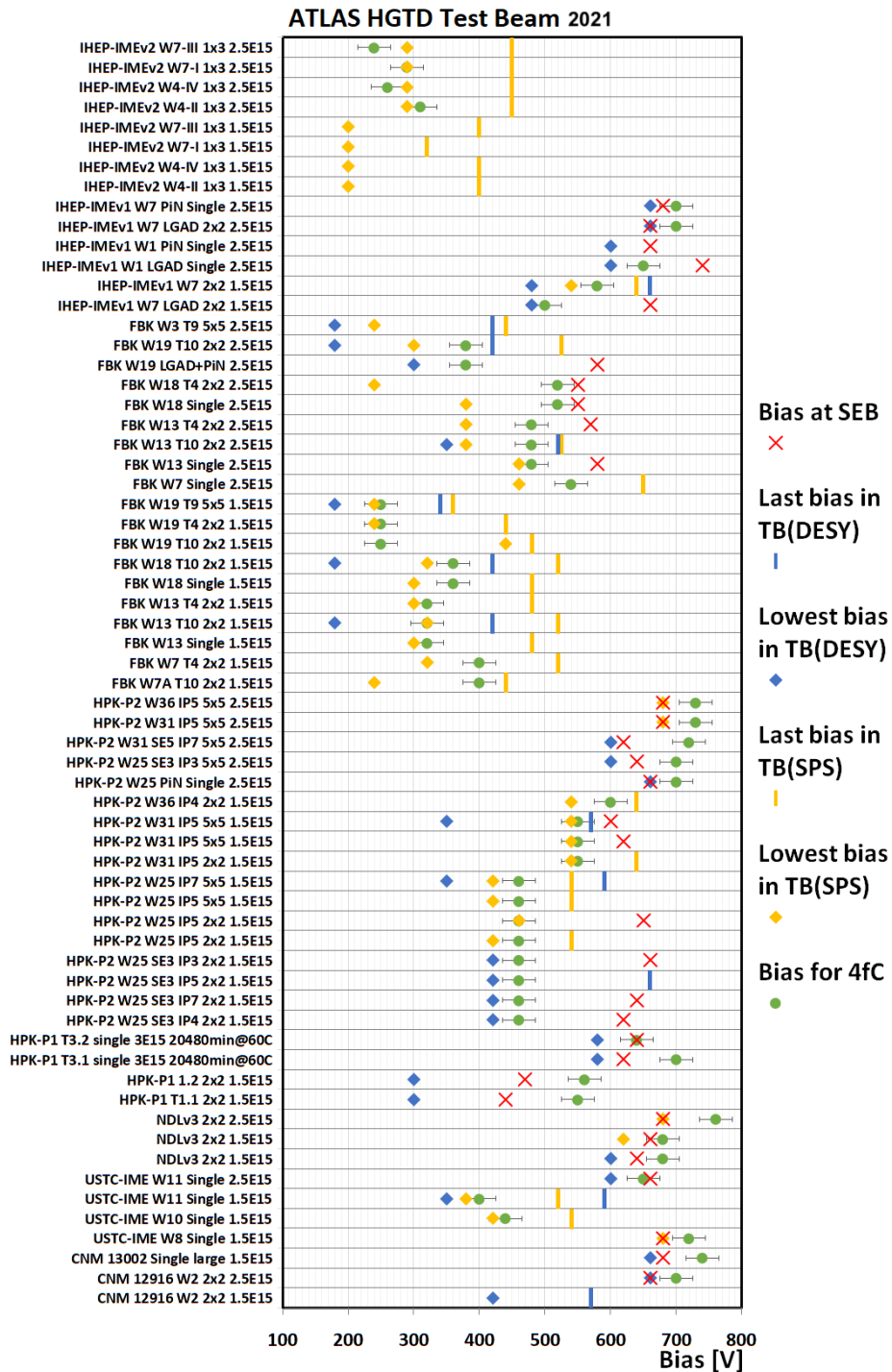


Figure 7: Results of both the DESY and SPS beam tests. Green points mark the bias required to reach 4fC and includes the error. The diamond marks are the lowest bias tested while the line marks are the highest bias tested. Yellow marks the measurement range performed at SPS, while blue marks the measurement range performed at DESY. Red crosses mark the bias at which a sensor broke in the beam. Sensors are grouped up by producer.

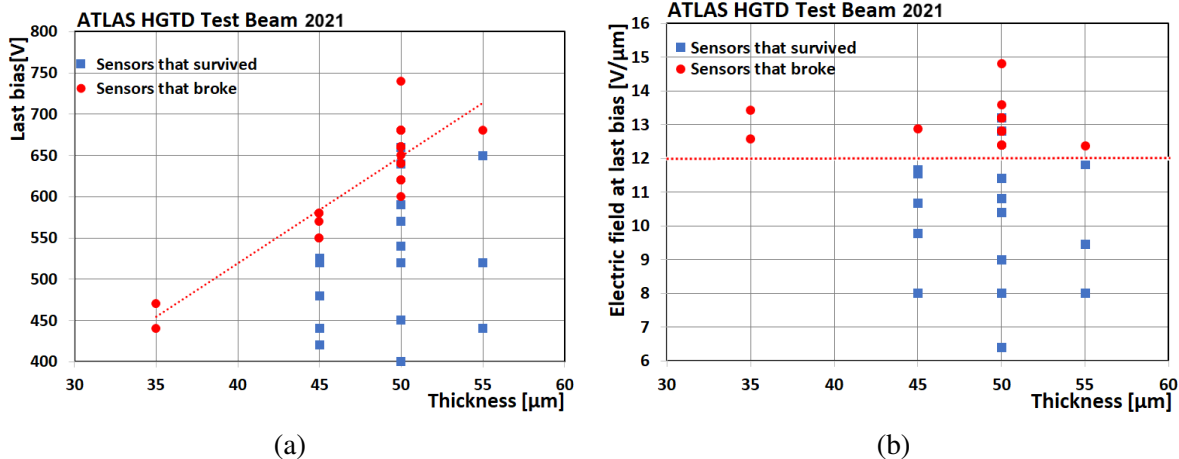


Figure 8: Comparison of (a) the thickness with the last tested bias for all sensors, and (b) the thickness with the electric field in the sensor. In both plots the red circles mark sensors that broke and the red dashed line indicates 12 V/ μm .

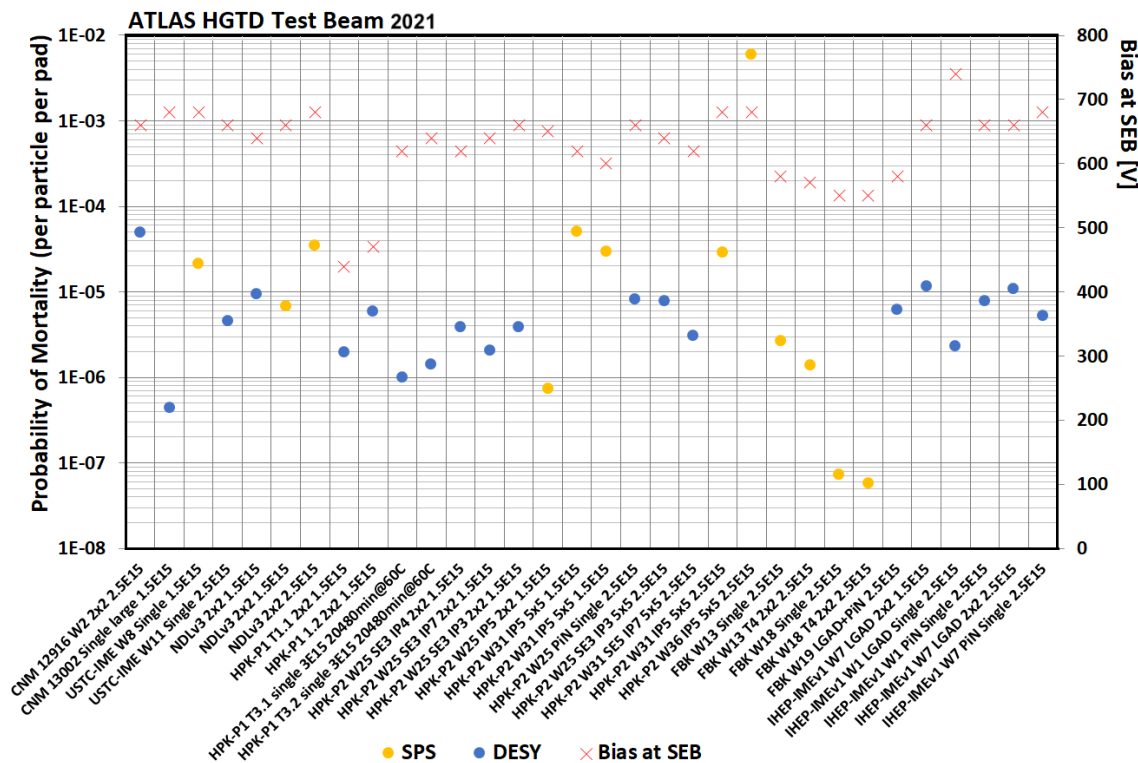


Figure 9: Probability of mortality for each particle crossing a single-pad of the sensor, calculated for the sensors that broke at DESY and SPS beams. The bias that the sensor was operated at when mortality occurred is denoted by a red cross.

6 Conclusion

In this study, many sensors from various producers and runs were sent to two test beam facilities to have their survivability tested in the particle beam. Some of the sensors broke at biases lower than those tested in the lab, demonstrating that the particle beam itself causes their mortality. It was determined that it was not the design of the LGAD that changed the chances of mortality, but the strength of the electric field. It is concluded that the safe zone of operation is at electric fields below $11 \text{ V}/\mu\text{m}$.

Acknowledgements

The authors gratefully acknowledge CERN and the SPS staff for successfully operating the North Experimental Area and for continuous supports to the users. The measurements leading to these results have been performed at the Test Beam Facility at DESY Hamburg (Germany), a member of the Helmholtz Association (HGF). This work was partially funded by MINECO, Spanish Government, under grant RTI2018-094906-B-C21. This project has received funding from the European Union's Horizon 2020 research and innovation programme under the Marie Skłodowska-Curie grant agreement No. 754510. This work was partially funded by: the Spanish Government, under grant FPA2015-69260-C3-2-R and SEV-2012-0234 (Severo Ochoa excellence programme); and by the H2020 project AIDA-2020, GA no. 654168. The authors acknowledge the financial support from the Slovenian Research Agency (ARRS J1-1699, ARRS P1-0135). The USP group acknowledges support from FAPESP grant 2020/04867-2 and CAPES.

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Appendices

A List of tested sensors

The sensors that were tested in both test beam facilities are listed in this table. The sensor name is made up of the producer, run, wafer, and in certain cases other information such as the type or inter-pad (IP) distance. Where the sensor is a PiN and not an LGAD, this is mentioned in parenthesis next to the sensor name. The size of the sensor refers to the number of pads. In the case of LGAD-PiN this means that there were two pads, with one being an LGAD and the other a PiN. The annealing for the majority of the sensors was done at 60 °C, unless stated otherwise in parenthesis next to the annealing time.

Table 1: List of tested sensors from CNM, USTC-IME, NDL and HPK vendors.

Sensor name	Pad structure	Active thickness [μm]	V_{gl} [V]	Fluence [neq/cm^2]	Annealing time [min] (@60 °C)	Tested at
CNM 12916 W2	2×2	50	13.2	1.5×10^{15}	80	DESY
CNM 12916 W2	2×2	50	6.6	2.5×10^{15}	80	DESY
CNM 13002	single large	55	unknown	1.5×10^{15}	80	DESY
USTC-IME-1.1 W8	single	50	15.6	1.5×10^{15}	80	SPS
USTC-IME-1.1 W10	single	50	19.1	1.5×10^{15}	80	SPS
USTC-IME-1.1 W11	single	50	29.2	1.5×10^{15}	80	DESY/ SPS
USTC-IME-1.1 W11	single	50	23.3	2.5×10^{15}	80	DESY
NDLv3 B14-D3	2×2	50	10.8	1.5×10^{15}	80	DESY
NDLv3 B14-D5	2×2	50	10.8	1.5×10^{15}	80	SPS
NDLv3 B14-B5	2×2	50	unmeasurable	2.5×10^{15}	80	SPS
HPK-P1 Type1.1 SE2-IP9	2×2	35	unknown	1.5×10^{15}	80	DESY
HPK-P1 Type1.2 SE3-IP5	2×2	35	unknown	1.5×10^{15}	80	DESY
HPK-P1 Type3.1 SE5	single	50	unknown	3×10^{15}	20480	DESY
HPK-P1 Type3.2 SE2	single	50	unknown	3×10^{15}	20480	DESY
HPK-P2 W25 SE3-IP4	2×2	50	29.5	1.5×10^{15}	80	DESY
HPK-P2 W25 SE3-IP7	2×2	50	29.5	1.5×10^{15}	80	DESY
HPK-P2 W25 SE3-IP5	2×2	50	29.5	1.5×10^{15}	80	DESY
HPK-P2 W25 SE3-IP3	2×2	50	29.5	1.5×10^{15}	80	DESY
HPK-P2 W25 SE3-IP5	2×2	50	29.5	1.5×10^{15}	80	SPS
HPK-P2 W25 SE3-IP5	2×2	50	29.5	1.5×10^{15}	80	SPS
HPK-P2 W25 SE3-IP5	5×5	50	29.5	1.5×10^{15}	80	SPS
HPK-P2 W25 SE3-IP7	5×5	50	29.5	1.5×10^{15}	80	DESY/ SPS
HPK-P2 W31 SE3-IP5	2×2	50	27.4	1.5×10^{15}	80	SPS
HPK-P2 W31 SE3-IP5	5×5	50	27.4	1.5×10^{15}	80	SPS
HPK-P2 W31 SE3-IP5	5×5	50	27.4	1.5×10^{15}	80	DESY/ SPS
HPK-P2 W36 SE3-IP4	2×2	50	24.8	1.5×10^{15}	80	SPS
HPK-P2 W25 (PIN)	single	50	N/A	2.5×10^{15}	80	DESY
HPK-P2 W25 SE3-IP3	5×5	50	18.9	2.5×10^{15}	80	DESY
HPK-P2 W31 SE5-IP7	5×5	50	18.9	2.5×10^{15}	80	DESY
HPK-P2 W31 SE3-IP5	5×5	50	18.9	2.5×10^{15}	80	SPS
HPK-P2 W36 SE3-IP5	5×5	50	15.2	2.5×10^{15}	80	SPS

Table 2: List of tested sensors from FBK and IHEP-IME vendors.

Sensor name	Pad structure	Thickness [μm]	V_{gl} [V]	Fluence [$\text{n}_{eq}/\text{cm}^2$]	Annealing time [min] (@60 °C)	Tested at
FBK-UFSD3.2 W7A-Type 10	2×2	55	18.0	1.5×10^{15}	80	SPS
FBK-UFSD3.2 W7-Type 4	2×2	55	19.6	1.5×10^{15}	80	SPS
FBK-UFSD3.2 W13	LGAD-PiN	45	34.2	1.5×10^{15}	80	SPS
FBK-UFSD3.2 W13-Type 10	2×2	45	34.2	1.5×10^{15}	80	DESY/ SPS
FBK-UFSD3.2 W13-Type 4	2×2	45	34.2	1.5×10^{15}	130	SPS
FBK-UFSD3.2 W18	LGAD-PiN	45	33.1	1.5×10^{15}	80	SPS
FBK-UFSD3.2 W18-Type 10	2×2	45	33.1	1.5×10^{15}	80	DESY/ SPS
FBK-UFSD3.2 W19-Type 10	2×2	45	37.3	1.5×10^{15}	80	SPS
FBK-UFSD3.2 W19-Type 4	2×2	45	37.3	1.5×10^{15}	80	SPS
FBK-UFSD3.2 W19-Type 9	5×5	45	37.3	1.5×10^{15}	80	DESY/ SPS
FBK-UFSD3.2 W7	LGAD-PiN	55	17.6	2.5×10^{15}	80	SPS
FBK-UFSD3.2 W13	LGAD-PiN	45	29.1	2.5×10^{15}	80	SPS
FBK-UFSD3.2 W13-Type 10	2×2	45	29.1	2.5×10^{15}	80	DESY/ SPS
FBK-UFSD3.2 W13-Type 4	2×2	45	29.1	2.5×10^{15}	80	SPS
FBK-UFSD3.2 W18	LGAD-PiN	45	28.5	2.5×10^{15}	80	SPS
FBK-UFSD3.2 W18-Type 4	2×2	45	28.5	2.5×10^{15}	80	SPS
FBK-UFSD3.2 W19	LGAD-PiN	45	32.4	2.5×10^{15}	80	DESY
FBK-UFSD3.2 W19-Type 10	2×2	45	32.4	2.5×10^{15}	80	DESY/ SPS
FBK-UFSD3.2 W3-Type 9	5×5	45	unknown	2.5×10^{15}	80	DESY/ SPS
IHEP-IMEv1 W7	2×2	50	14.3	1.5×10^{15}	80	DESY
IHEP-IMEv1 W7	2×2	50	14.3	1.5×10^{15}	80	DESY/ SPS
IHEP-IMEv1 W1	single	50	10.8	2.5×10^{15}	80	DESY
IHEP-IMEv1 W1 (PIN)	single	50	N/A	2.5×10^{15}	80	DESY
IHEP-IMEv1 W7	2×2	50	11.1	2.5×10^{15}	80	DESY
IHEP-IMEv1 W7 (PIN)	single	50	N/A	2.5×10^{15}	80	DESY
IHEP-IMEv2 W4-II	1×3	50	18.3	1.5×10^{15}	80	SPS
IHEP-IMEv2 W4-IV	1×3	50	19.7	1.5×10^{15}	80	SPS
IHEP-IMEv2 W7-I	1×3	50	18.7	1.5×10^{15}	80	SPS
IHEP-IMEv2 W7-III	1×3	50	20.3	1.5×10^{15}	80	SPS
IHEP-IMEv2 W4-II	1×3	50	16.7	2.5×10^{15}	80 (@90°C)	SPS
IHEP-IMEv2 W4-IV	1×3	50	17.2	2.5×10^{15}	80 (@90°C)	SPS
IHEP-IMEv2 W7-I	1×3	50	16.3	2.5×10^{15}	80 (@90°C)	SPS
IHEP-IMEv2 W7-III	1×3	50	18.7	2.5×10^{15}	80 (@90°C)	SPS