

PS/OP/Info 89-1
02.02.89

**NEW RF-GYMNASTICS FOR THE ANTI-PROTONS
PRODUCTION BEAM**

Presented by R.Garoby (02.02.89)

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"QUASI-ADIABATIC" BEAM MERGING AND BATCH COMPRESSION.

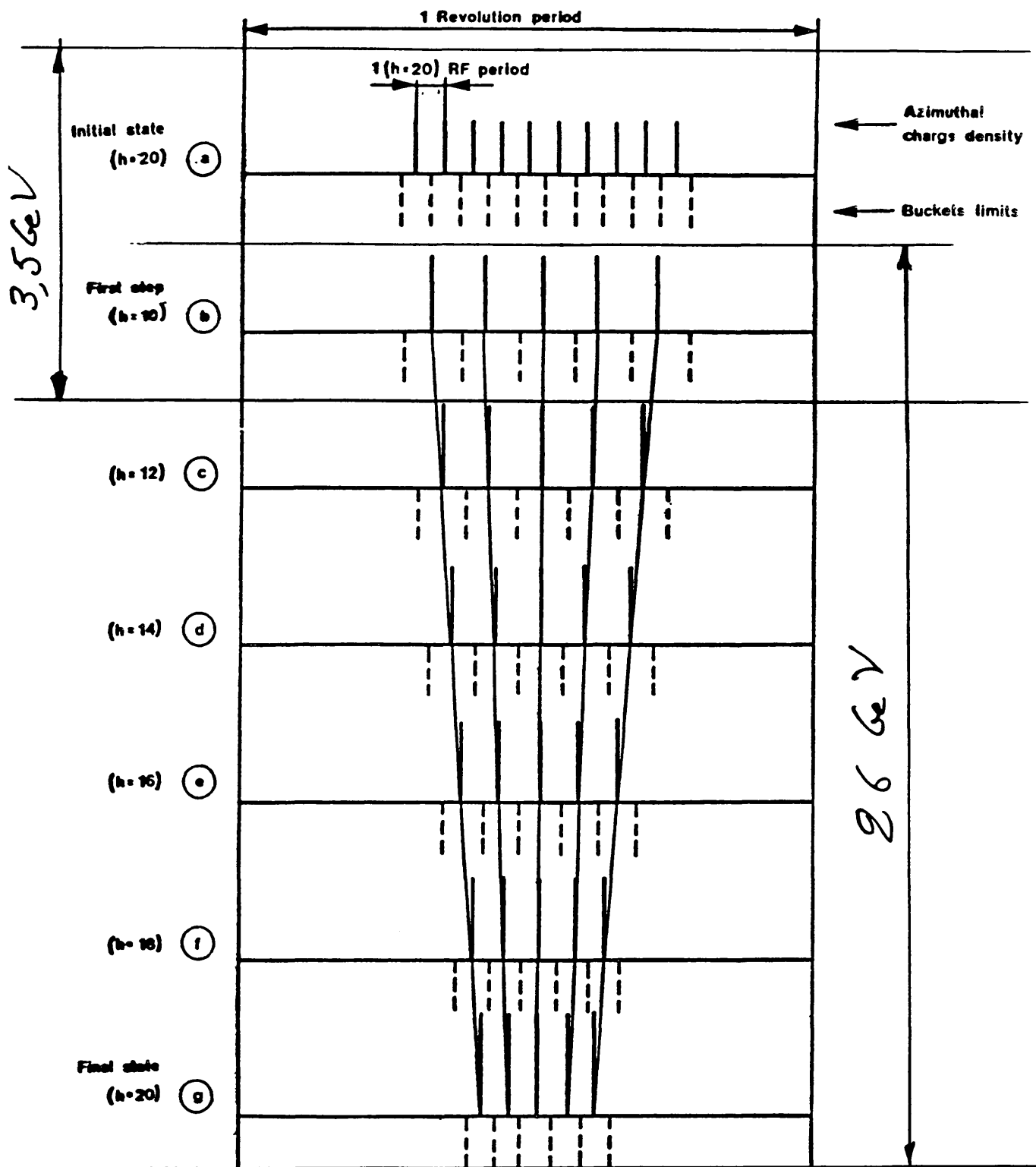
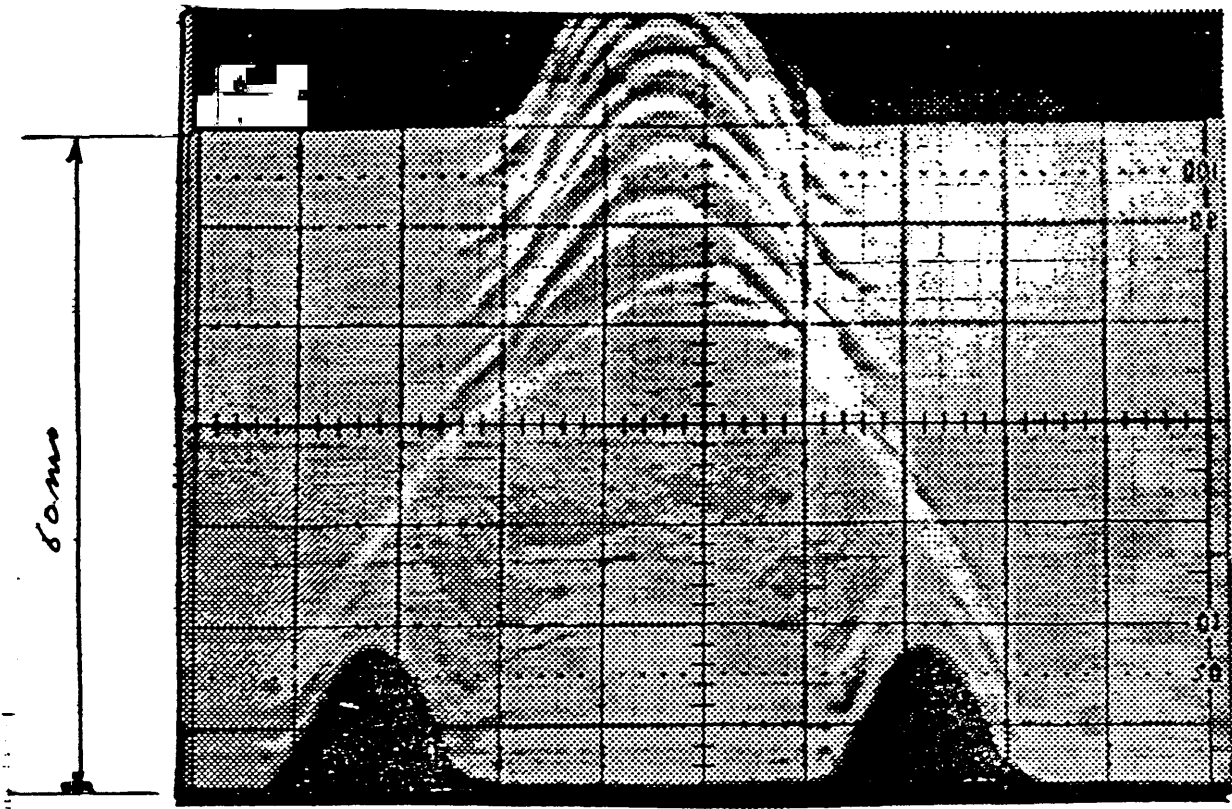
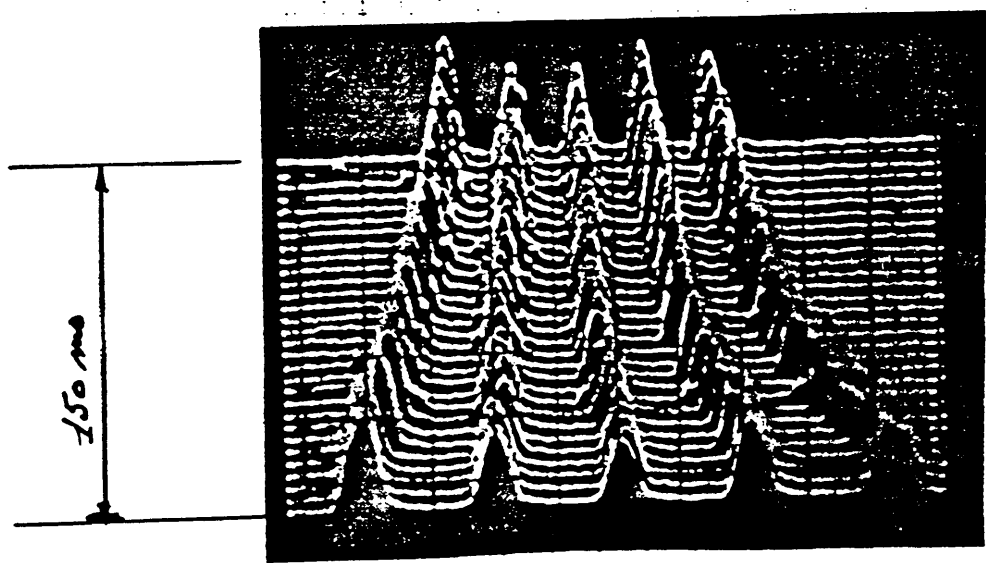


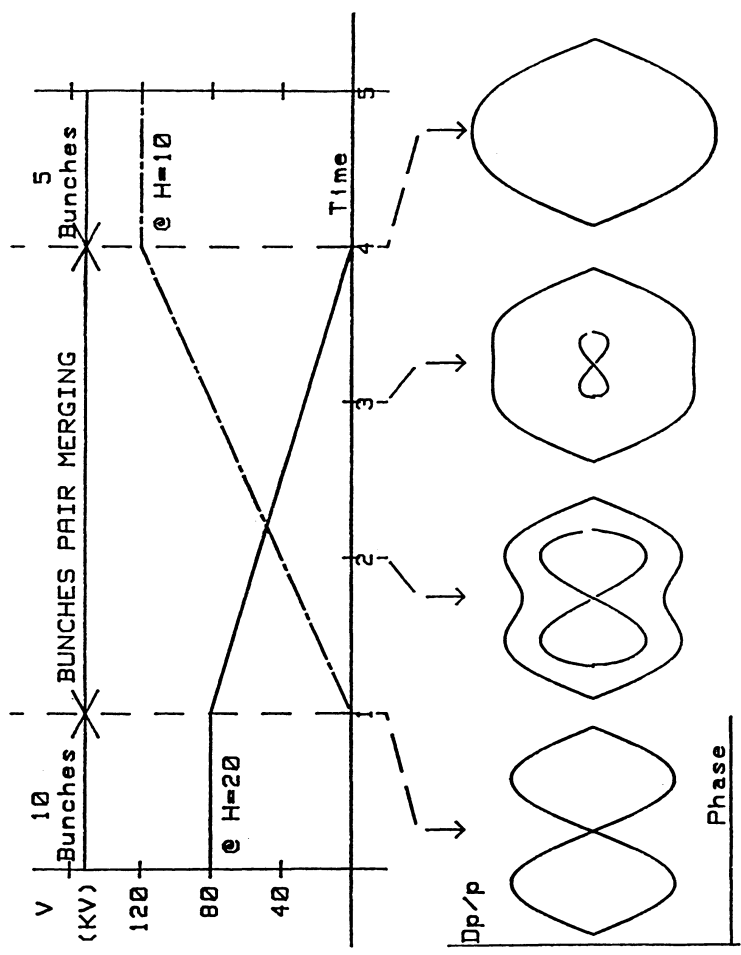
Fig.1: Coarse description of the azimuthal charge density during the process



"B.P.M." (Bunches pair merging)



"Batch Compression"



SELECTED CONTROL PARAMETERS FOR THE
26 GeV "BATCH COMPRESSION" PROCESS.

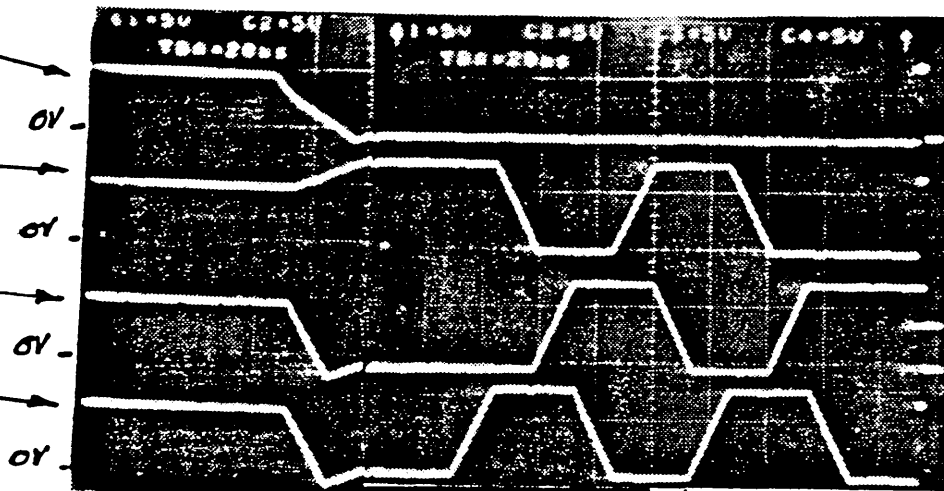
LIST OF CAVITIES

51, 76, 81, 91

36, 46

56, 66

86, 96



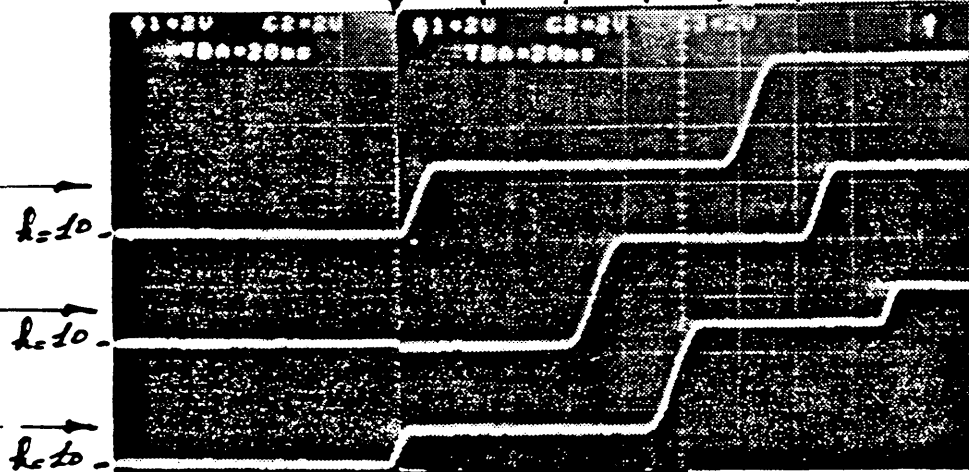
VOLTAGE
PROGRAMS

C1110	$h_c = 10$	$h_c = 12$	$h_c = 14$	$h_c = 16$	$h_c = 18$	HARMONIC "SEEN" BY THE BEAT
	\downarrow	\downarrow	\downarrow	\downarrow	\downarrow	
	12	14	16	18	20	

56, 66, 76, 81, 91

36, 46

86, 96

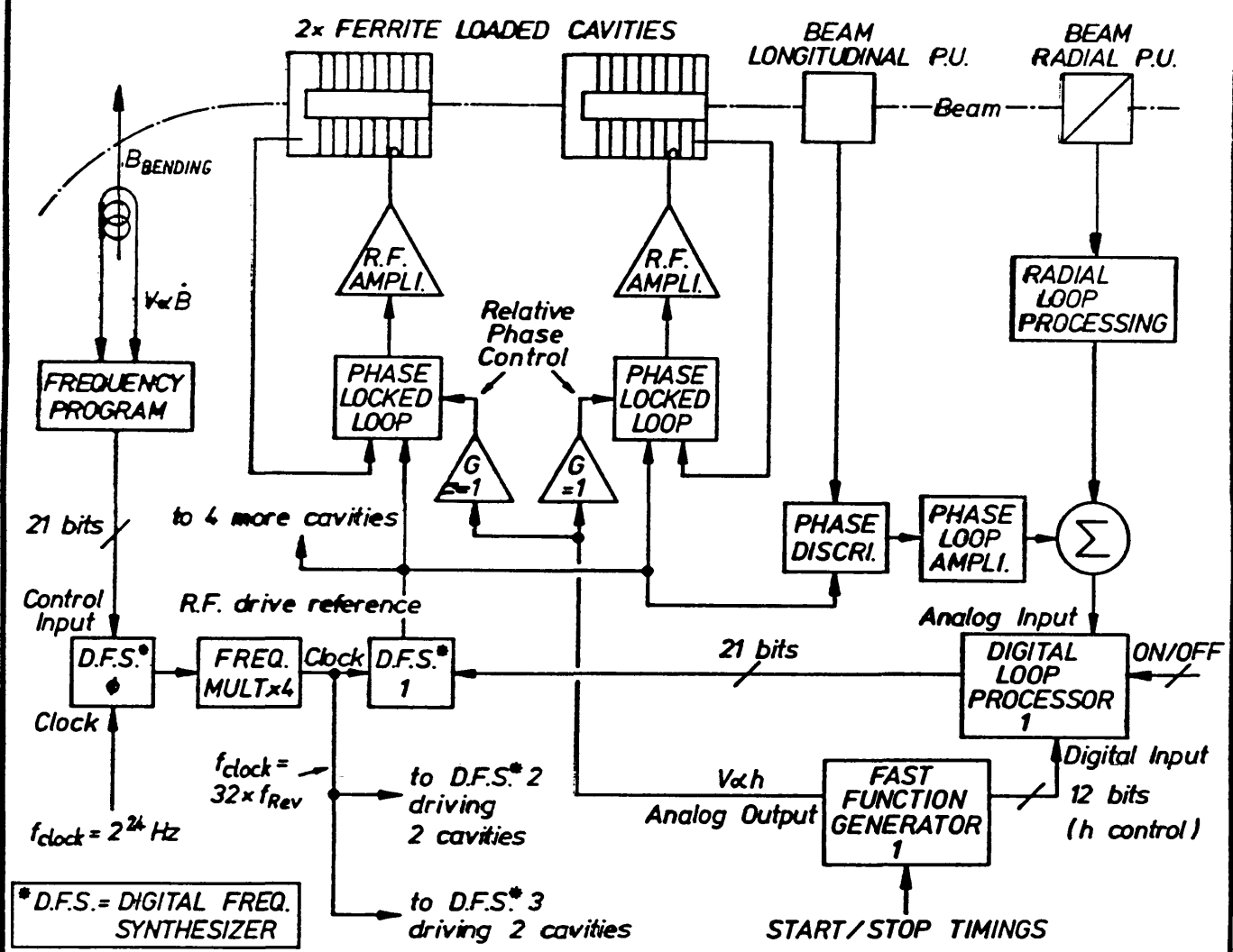


$h_c = 20$
 $h_c =$ FREQUEN
20
PROGRAMS

$h_c = 20$

USMAGE GROSSER/ROUGH MACHINING	±0.2	±0.5	±0.8	±1.2	±2	±3
MECANO. SOUDURE/WELDED STRUCTURE	±0.5	±1	±2	±3	±5	±7
TOLERANCES GENERALES						

DESSIN, RUGOSITE, TOLERANCES
 SELON NORMES ISO
 DRAWINGS, RUGOSITY, TOLERANCES
 ACCORDING TO ISO STANDARDS

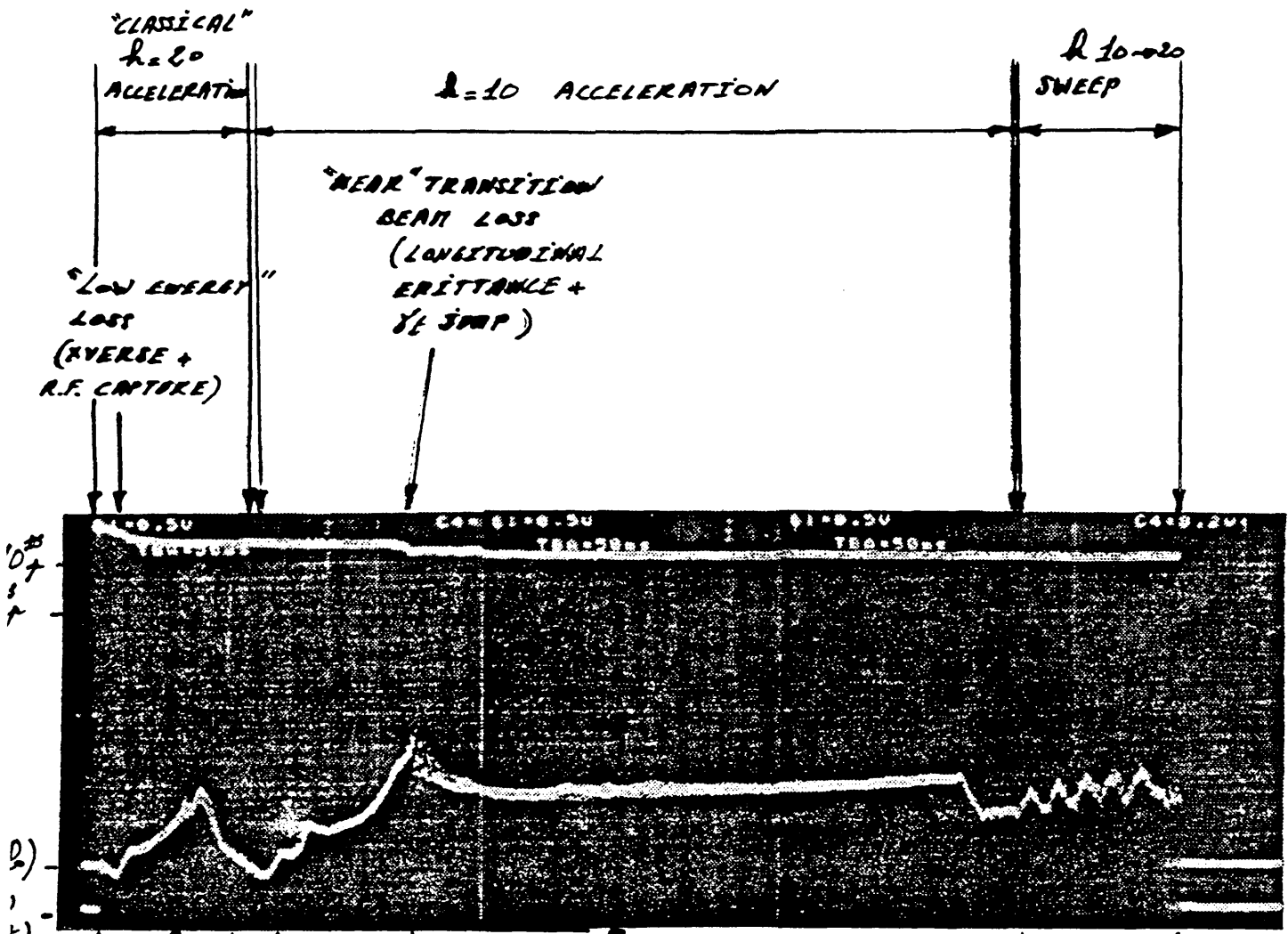


*D.F.S. = DIGITAL FREQ. SYNTHESIZER

QUANT.	DESCRIPTION	POS.	MATIERE	OBSERVATIONS	
	ENSEMBLE / ASSEMBLY		S. ENS / S. ASSY.		
	Fig. 2: Simplified block diagram of low level R.F.			ECHELLE SCALE	
				NOM	DATE
				DESSINE	23.2.87
				CONTOLE	
	VU				
	REPLACE				
	ORGANISATION EUROPEENNE POUR LA RECHERCHE NUCLEAIRE EUROPEAN ORGANIZATION FOR NUCLEAR RESEARCH GENEVE			INDICE	

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TYPICAL BEAT SIGNALS DURING A FULL CYCLE.



INJECTION @ 1.6eV

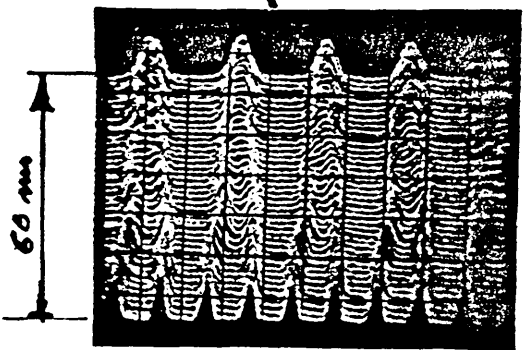
BEAM MERGING @ 3.5 GeV

TRANSITION

BATCH COMPRESSION @ 26 GeV

3.5 GeV LONGITUDINAL INST.

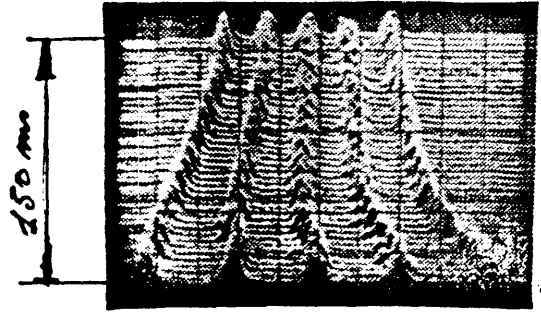
"HIGH ENERGY" LONGITUDINAL INSTABILITY



R=10
5 bunches

R=20
10 bunches

100 ns/div.



R=20

R=10

100 ns/div.

TIME

PRACTICAL EXPERIENCE WITH THAT NEW BEAM MANIPULATION.

LOW INTENSITY OPERATION ($< 2 \cdot 10^{12}$ ppp):

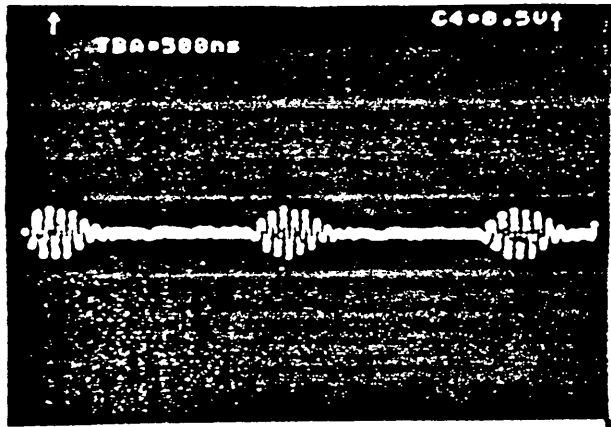
- Many iterations to come to a satisfactory lay-out giving reliable results.

Burning in was done during the many machine developments.

- Adjustment time was very long, due to the large number of control parameters (amplitude, phase, timing, ...).
- Synchronization before ejection was difficult and implied modifying the sequence of events.

HIGH INTENSITY OPERATION (up to $1.55 \cdot 10^{13}$ ppp).

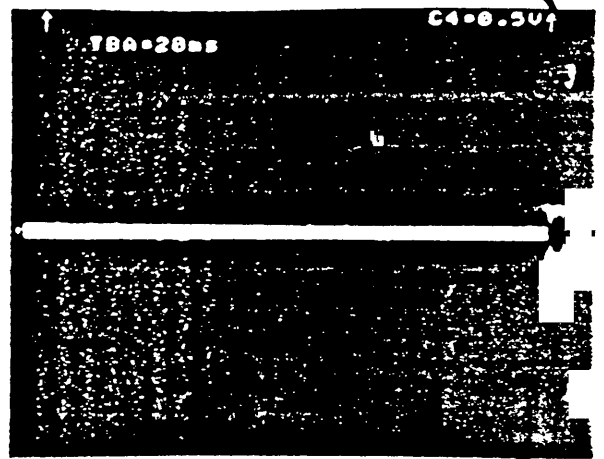
- Short circuiting unused cavities is mandatory.
(\Rightarrow hard work! $\approx 3 \cdot 10^6$ operations in 6 weeks)
- Complementary feedbacks had to be implemented:
 - Forward damping (on φ_s below transition, on \hat{Y}_{xx} above).
 - $h=1$ beam phase loop against coherent dipolar bunch phase oscillation.
- A few phase perturbations were necessary to handle the transient cavity beam loading.



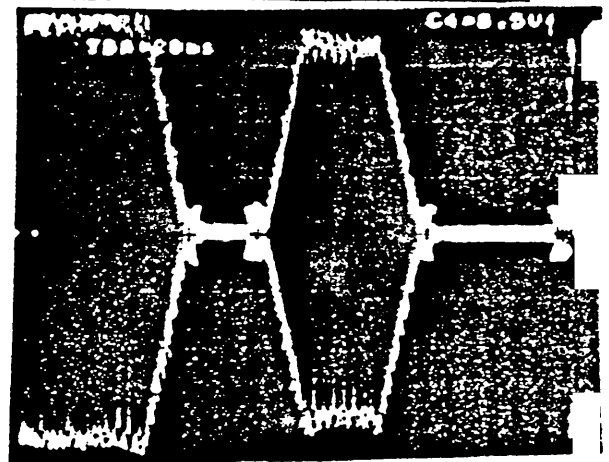
CLOSE UP VIEW OF BEAM
INDUCED VOLTAGE
ON A NON-SHORT CIRCUITED
CAVITY

C4110
1

BUNCH LENGTH
COMPRESSION



C51

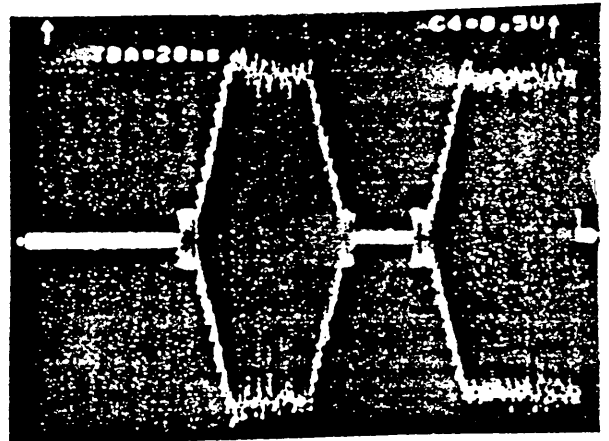


C36

VOLTAGE ON THE CAVITY
GAPS DURING THE 266V
PROCESS.

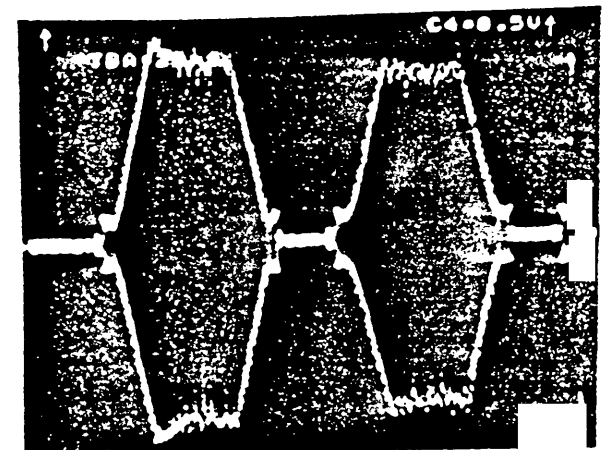
$$\frac{I}{f} = 1.42 \times 10^{13} \text{ III}.$$

C56



Note: - gap short circuits are
pulsed.

- Hereward damping
modulates the R.F.
envelope.



C86

BEAM CHARACTERISTICS.

PRESENT PERFORMANCE.

- + - 1.5×10^{13} ppp sent on target with $\sim 2 \cdot 10^{12}$ ppp lost between P.S.B. output and P.S. extraction.
- - Bunch length: ~ 30 ns
- - "Ghost" bunches: $\sim 1.5 \times 10^{12}$ ppp.

Overall performance: $\sim 10\%$ improvement of the stacking rate compared to the other beam (40% expected).

PROBLEMS.

- Longitudinal beam instability above transition energy, asking for enormous longitudinal emittances.
($\epsilon_L \approx 2 \text{ e.V.}$ for $2 \cdot 10^{12}$ ppp).
 \Rightarrow long bunches \Rightarrow poor bunch rotation efficiency in the A.C.
 $\Rightarrow \sim$ full buckets during manipulations \Rightarrow diffusion of particles outside the central buckets.
- Strong periodic transient beam loading generating large bunch shape oscillations \Rightarrow filamentation...

DIRECTIONS OF WORK.

- ① Fight against periodic transient beam loading in the cavities: \Rightarrow
 - Improvement of the gap relays control, to reduce dead time, while preserving reliability.
 - Development of a "One turn delay feedback" around each cavity.
- ②. Against longitudinal coupled bunch instabilities:
 - \Rightarrow • Search for offending impedances.
 - Damping system around $h = 38,7$ above transition energy.
- ③. Operational improvements:
 - \Rightarrow • Improved "Hereward damping".
 - Better synchronization logic.
 - P.C. controlled monitoring.
 - Control parameters reorganization.
(which will allow using "AA" cycles).
- ④. Machine study and office thinking!

PREVISIONS.

Best case : - Intensity increase (present level dictated by P.S.B. beam quality + P.S. losses) : $\sim \pm 10\%$.

- Smaller bunch emittances giving a better yield and an improved bunch rotation efficiency.

? ...

\Rightarrow Need for: - machine development time.

- machine specialists time and engineering support.

R.S. 2/00

FIRST IDEAS ABOUT A "ONE-TURN
DELAY FEEDBACK" ON THE P.S. FERRITE
CAVITIES

1989 Aims:

- ①. Proof of principle: - hardwarewise.
- beamwise.
- ②. Get some benefits during the p/f run.
⇒ Implementation of a limited capability system.

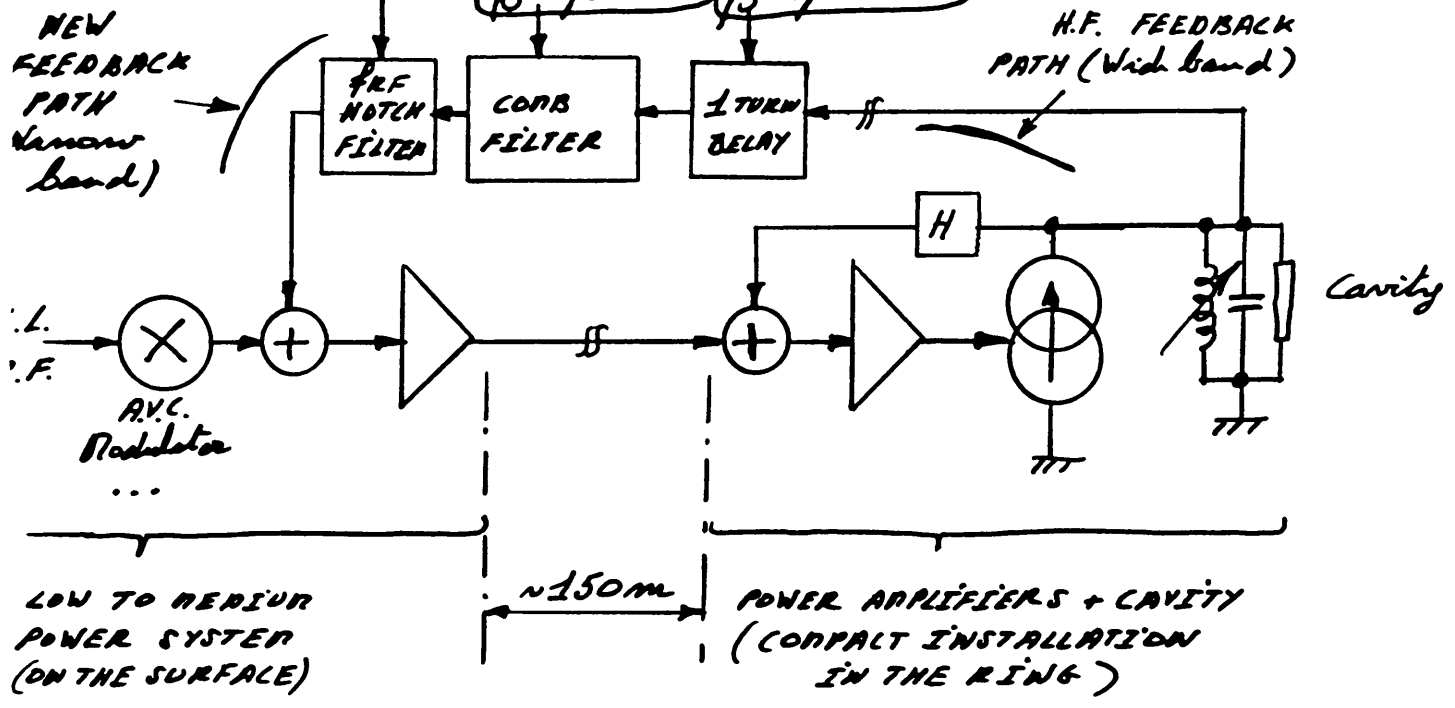
1989 Hardware specifications.

- ①. Fixed energy system. ⇒ No need for variable delay and
(26 GeV) variable tune of the comb filter
⇒ but need for tunable notch filter remains,
to be able to cover all the "Batch compression"
process.
- ②. Analog design providing ≈ 12 dB impedance reduction
on the first ± 3 revolution frequency sidebands
around the cavity tune.

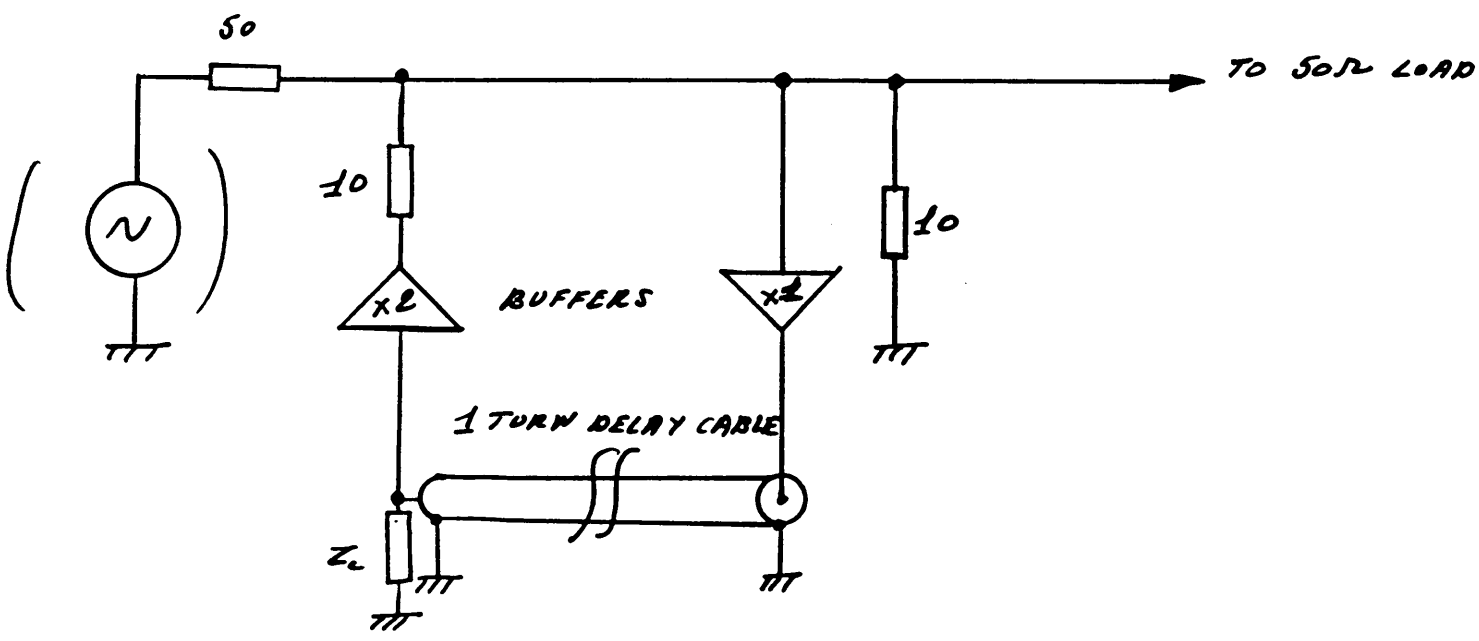
Design options adopted.

- ①. Fully analog design.
- ②. Wide band without mixing (no frequency translation).
- ③. Reuse of maximum part of old feedforward compensation
(Controls, cabling, ...)

Cavity time dependent
(β dependent) (β dependent)

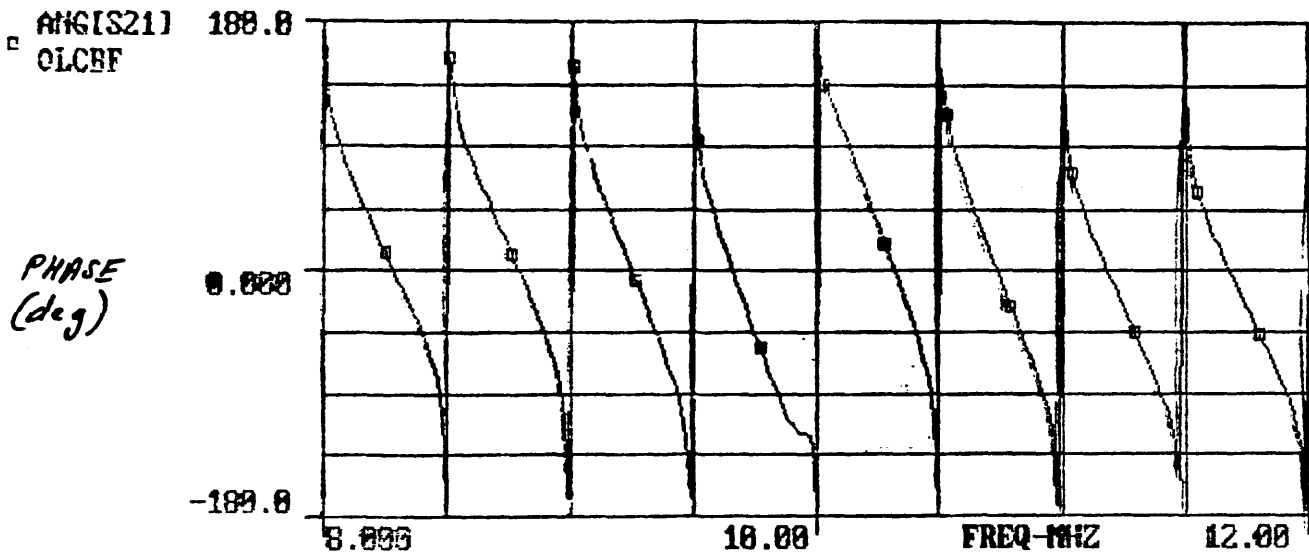
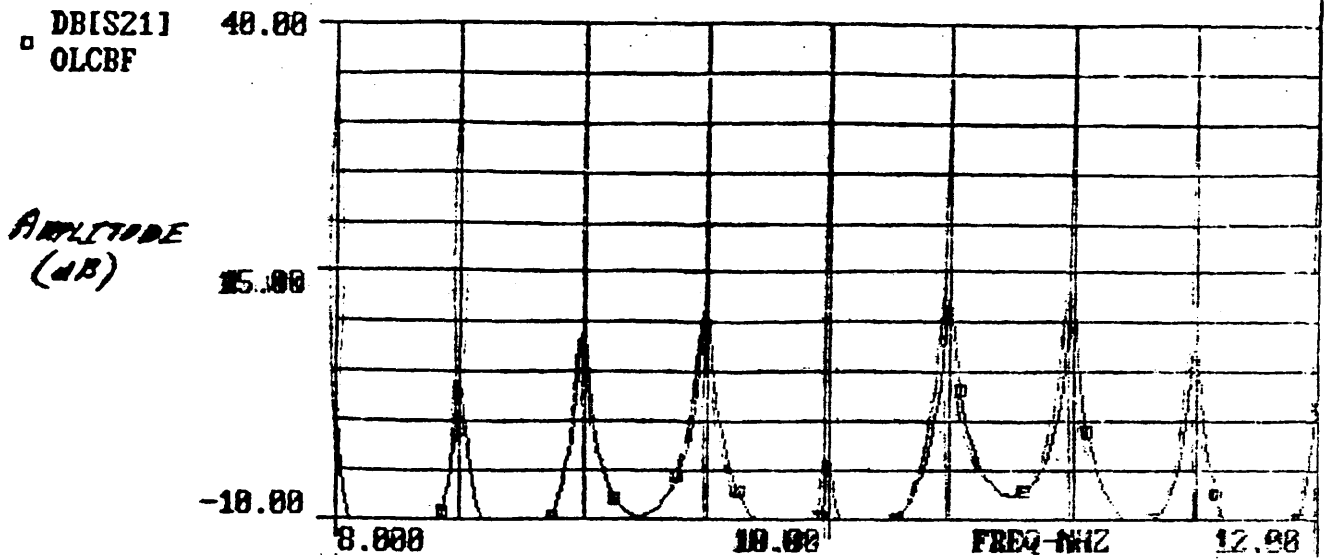


OVERALL IMPLEMENTATION



"EASY-MINDED" IMPLEMENTATION OF AN ANALOG RECURSIVE FILTER.

CORB FILTER OPEN LOOP XFER FUNCTION.



CLOSED LOOP CAVITY IMPEDANCE

F: 9.501 Y: 29.66 dF: 0.031 dY: -13.33

