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# **Evidence of Kramer extrapolation inaccuracy for predicting high field Nb3Sn properties**

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**Abstract**. Future applications requiring high magnetic fields, such as the proposed Future Circular Collider, demand a substantially higher critical current density,  $J_c$ , at fields  $\geq$ 16 T than is presently available in any commercial strand, so there is a strong effort to develop new routes to higher  $J_c$  Nb<sub>3</sub>Sn. As a consequence, evaluating the irreversibility field ( $H_{irr}$ ) of any new conductor to ensure reliable performance at these higher magnetic fields becomes essential. To predict the irreversibility field for  $Nb<sub>3</sub>Sn$  wires, critical current measurements,  $I<sub>c</sub>$ , are commonly performed in the 12-15 T range and the Kramer extrapolation is used to predict higher field properties. The Kramer extrapolation typically models the contribution only for sparse grain boundary pinning, yet  $Nb<sub>3</sub>Sn$  wires rely on a high density of grain boundaries to provide the flux pinning that enables their high critical current density. However, whole-field range VSM measurements up to 30 T recently showed for  $Nb<sub>3</sub>Sn RRP<sup>®</sup>$  wires that the field dependence of the pinning force curve significantly deviates from the typical grain boundary shape, leading to a 1-2 T overestimation of *Hirr* when extrapolated from the typical mid-field data taken only up to about 15 T. In this work we characterized a variety of both RRP® and PIT  $Nb<sub>3</sub>Sn$  wires by transport measurements up to 29 T at the Laboratoire National des Champs Magnétiques Intenses (LNCMI), part of the European Magnetic Field Laboratory in Grenoble, to verify whether or not such overestimation is related to the measurement technique and whether or not it is a common feature across different designs. Indeed we also found that when measured in transport the 12-15 T Kramer extrapolation overestimates the actual *Hirr* in both types of conductor with an inaccuracy of up to 1.6 T, confirming that high field characterization is a necessary tool to evaluate the actual high field performance of each  $Nb<sub>3</sub>Sn$ wire.

## **1. Introduction**

The 100 TeV Future Circular Collider (FCC) envisioned at CERN will require a large number of  $Nb<sub>3</sub>Sn$  bending magnets which will need to operate in the 16 T range [1,2]. Currently, only two wire manufacturing processes have demonstrated the potential to bring Nb<sub>3</sub>Sn into this high field operation range: the Rod Restack Process (RRP®) produced by Bruker OST [3], and the Powder In Tube (PIT) technique produced by Bruker EAS [4–6]. Despite recent efforts to further optimize the existing



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chemistry, architecture and heat treatment of these conductors, the *J<sup>c</sup>* appears to be limited well below the desired 1,500 A/mm<sup>2</sup> (16 T, 4.2 K) demanded for FCC [7]. In an effort to push Nb<sub>3</sub>Sn superconducting technology to its limits, the conductor community has been focussing R&D towards the introduction of additional pinning centers (APC) to increase  $J_c$  in the superconducting transport layer, and also to shift the maximum of the pinning force curve to higher fields. Currently there are multiple groups working on variants of the PIT process to introduce additional pinning centers. Fermilab and Ohio State University, in collaboration with Hyper Tech Research, Inc, reintroduced the previously developed internal oxidation technique, in which Nb1Zr is oxidized at final wire size to form  $ZrO<sub>2</sub>$  precipitates that both increase grain boundary density and provide additional pinning centres  $[8]$ . However, the need to supply oxygen to the Nb<sub>3</sub>Sn during reaction increases the complexity of production especially if non-PIT routes are considered. At the Applied Superconductivity Center (ASC), part of the National High Magnetic Field Laboratory in Tallahassee, Florida, significantly refined Nb<sub>3</sub>Sn grains were produced without using oxygen by adding Hf to the standard Nb4at%Ta alloy. In studies comparing Nb4Ta, Nb4Ta1Zr and Nb4Ta1Hf with and without a  $SnO<sub>2</sub>$  source, the highest  $J_c$ , well above the FCC specification, was found in a  $SnO_2$ -free wire of Nb4Ta1Hf. This surprising result appears to have its basis in the delaying of recrystallization of pure Nb or Nb4Ta which occurs during the A15 reaction above 600 °C. With Hf (or Zr) present in the alloy, the density of grain boundary diffusion paths of Sn into the alloy is greatly increased and maintained during the A15 reaction, allowing a much finer A15 grain size [9].

The impact of these new approaches on the properties at magnetic fields  $\geq 16$  T is not yet fully understood and even the properties of conventional strands are seldom characterized beyond 16 T as such fields are not typically available outside the national high field laboratories. Thus it is valuable to make measurements from low to very high field that can then be used to model the field versus current behaviour over a broad range, enabling more reliable predictions based on measurements from more accessible lower field magnets (< 15 T). The common approach to characterizing wires for high field applications has been to use transport  $J_c$  data measured in the 12-15 T range, then extrapolate using the Kramer expression [10] to predict the irreversibility field  $(H_{irr})$  where the flux lines become fully depinned and  $J_c$  goes to zero. Thus  $H_{irr}$  is approximated as the Kramer field  $H_k$ , where the Kramer function (eq 1) goes to zero.

$$
f_{k}(\mu_{0}H) = [J_{c}(\mu_{0}H)]^{0.5} \cdot (\mu_{0}H)^{0.25}
$$
 (1)

This Kramer model takes into account only the contribution of sparse grain boundary pinning, consistent with the relatively low grain boundary density of 100-200 nm diameter grains. However, there are signs from recent measurements on the highest critical current density production wires (Bruker-OST RRP®) that the Kramer function can deviate from linearity making extrapolations from low or mid-fields inadequate for predictions of the high-field performance [11]. Moreover, the newer Zr or Hf wire designs can have significant point pinning as well as significantly denser grain boundary pinning due to their <100 nm grain diameters. They might thus be expected to further deviate from linearity, driving the need for a more appropriate extrapolation methods, as has recently been discussed [11].

## **2. Experimental Details**

High field measurements were performed using the 29 T high field resistive magnet at the Laboratoire National des Champs Magnétiques Intenses (LNCMI) in Grenoble, France. The LNCMI is one of three laboratories forming the European High Magnetic Field Laboratory (EMFL). This 24 MW resistive magnet has a 50 mm bore diameter (38 mm diameter cryostat) and field homogeneity of 860 ppm in a 1 cm sphere at the center.

We used a probe (supplied by the LNCMI) typically used for ReBCO tape measurements that simply terminates with two rectangular copper rods to which a sample holder is attached. As the cryostat diameter limits straight sample lengths to  $\leq$  38 mm, we preferred to prepare our Nb<sub>3</sub>Sn wire

samples on VAMAS (Versailles Project on Advanced Materials and Standards) barrels in order to characterize longer lengths.

The VAMAS barrels are made of Ti-6Al-4V alloy which has a similar thermal expansion coefficient as  $Nb<sub>3</sub>Sn$  [12], and are grooved to better support the strand. A thin ceramic layer is baked onto the barrel to prevent sticking of the wire and allow easy removal after measurement, allowing the barrels to be reused. Cu rings were then attached to the top and bottom of the VAMAS barrel, and the strand wound onto the barrel with the ends of the strands fixed to the Cu caps by soldering after heat treatment. Two pairs of voltage taps were then added; the first set measures voltage across the inner 6 turns (~60 cm), while the second set is attached to the Cu end caps and measures voltage across the entire length of the conductor ( $\sim$ 90 cm). The last step is to apply vacuum grease across the barrel to provide some support during measurement at cryogenic temperatures. The barrelled samples were mounted on the measurement probe such that the Lorentz force generated when injecting current is inward, thus providing support by the barrel. A typical sample mounted on the VAMAS barrel and ready for measurements is shown in figure 1.



**Figure 1.** The bottom image shows our VAMAS adapter with a sample mounted before attaching to the measurement probe, shown at the top.

The main advantage of VAMAS barrels over straight samples is that  $\sim$ 1 m of wire is used, and we can reliably measure the voltage across the inner 60 cm, 60 times the length of short samples where we typically measure the voltage over only 1 cm. It was, however, necessary to develop an adaptor which could hold a VAMAS barrel and connect to the LNCMI probe.

The most challenging aspect of designing this adapter was that the as-prepared VAMAS barrels are  $\sim$ 32 mm in diameter with too little space between the barrel and the cryostat wall to run current leads around to the lower end of the barrel, thus requiring the current to be routed through the centre of the barrel. This demanded some complex geometries and, although we considered using a 3D printed Cu adapter, the final piece was classically machined from OFE Cu with RRR  $\sim$ 300.

For data processing we used a custom analysis script, executed in the IGOR software from WaveMetrics [13]. The software takes the raw data from the inner voltage taps as input, then removes any offset and resistive slope: the corrected I-V curves are fitted with the typical power law function.  $I_c$  is then determined from the fitting curve using the electric field of criterion 0.1  $\mu$ V/cm. In a few cases where the typical I-V characteristic was not obtained due to wire instability at low field and high current, the quench current was assumed to be *I<sup>c</sup>* .

#### *2.1. Samples measured*

We measured five different  $Nb<sub>3</sub>Sn$  wires, three PIT and two RRP (table 1). All three PIT samples are from the last generation of high-field conductors manufactured by Bruker EAS. They are Ta doped, 192 filament wires, 0.85 mm diameter and utilize a Nb bundle barrier that allows for a more aggressive reaction without degradation of RRR [14]. Of the three PIT conductors, wire 62902 (referring to billet number) was reacted with a typical heat treatment of  $415^{\circ}C/40$  h +  $620^{\circ}C/120$  h + 645°C/200 h, and wire 51603 was reacted using an inverted multistage heat treatment (IMHT) of  $660^{\circ}$ C/10h +  $620^{\circ}$ C/120h +  $640^{\circ}$ C/120h. This type of heat treatment (HT) has the benefit of a much improved small to large grain  $Nb<sub>3</sub>Sn$  ratio [6], as well as a higher temperature reaction stage which usually improves the high field properties [15]. Further details on the motivation for using an IMHT are described in [6]. We additionally measured another 51603 wire which was similarly heat treated but rolled to 15% deformation to simulate cabling deformation [14] and to investigate the effect of diffusion barrier breach and Sn leaking into the Cu [16] on the high field performance. Billets 62902 and 51603 are nominally the same. The RRP conductors have a 108/127 architecture with Ti doping. They were heat treated at  $210^{\circ}$ C/48h +  $400^{\circ}$ C/48h +  $650^{\circ}$ C/50h for the 0.7 mm diameter wire, and  $210^{\circ}$ C/48h + 400°C/48h + 665°C/50h for the 0.85 mm wire.

Wire	Billet	Deformation%	Wire diameter	<b>Heat Treatment</b>	Dopant
type			mm)		
<b>PIT</b>	62902	0%	0.85	$415/40+620/120+645/200$ (standard HT)	Тa
<b>PIT</b>	51603	0%	0.85	$660/10+620/120+640/120$ (IMHT)	Ta
PIT	51603	15%	0.85	$660/10+620/120+640/120$ (IMHT)	Ta
<b>RRP</b>	00019	0%	0.70	$210/48 + 400/48 + 650/50$	Ti
<b>RRP</b>	00385	0%	0.85	$210/48 + 400/48 + 665/50$	Ti

**Table 1**: Heat treatment details of Nb<sub>3</sub>Sn samples measured in high magnetic field at LNCMI.

## **3. Results and analysis**

We measured the five Nb<sub>3</sub>Sn barrels at increasing fields from  $10 T$  to the irreversibility field (25-26 T), defined as the field where the I-V curve shows only a resistive transition and there is no visible loss-free curve below the voltage criterion of 0.1  $\mu$ V/cm. All measurements are self-field corrected as described in [17]. An example of the raw I-V curves at the highest fields near *Hirr* are shown in figure 2. After correcting for resistive offset, fitting the data to reduce noise, and applying the self-field corrections, we can determine the non-Cu critical current density  $(J_c)$  for an applied magnetic field. In figure 3, this field dependence of the  $J_c$  is shown for all five samples over the entire field range. As previously described, the data in figure 3 can then be linearized using the Kramer function (eq.1) and its extrapolation to zero is thought to provide an approximation for the magnetic field  $(\mu_0 H_k)$  where  $J_c$ goes to zero, marking *Hirr*, the physical irreversibility field [10]. An example for the 0.85 mm RRP wire is shown in figure 4.

To improve the accuracy of the true  $H_{irr}$  values reported here, we considered the highest field where we saw little or no signal in the superconducting state, and also considered extrapolating the highest field measurements to further refine the  $H_{irr}$  value. For example, the 25.5 T curve in figure 2 shows that the wire begins its resistive transition below one amp, so we know the  $H_{irr}$  would be higher than 25.5 but lower than 26 T. To reduce this half Tesla uncertainty window, an extrapolation over the highest field data just below  $H_{irr}$  (24, 24.5, 25, 25.5 T) can be performed. For this wire we arrived at an *H<sub>irr</sub>* of 25.8 T; 1.6 T below the 27.4 T predicted by the Kramer extrapolation from the typical 12-15 T range. It is seen in figure 4 that the extrapolation from 20 T upwards is in close agreement with the reported *Hirr*, within 0.4 T in all cases (table 2). Since this manuscript focuses on the relative error of the predicted field rather than the absolute value, we normalized the extrapolated Kramer field (*Hk*) to

the measured irreversibility field (*Hirr*) and plot that value against the highest field in the extrapolated field range, starting extrapolations at 12 T (figure 5a). For example, the point at  $(\sim 19, 0.98)$  uses the data from 12-19 T, and predicts an *Hirr* 98% of the true value. All three PIT wires and the 0.85 mm RRP wire show over-predicted  $H_k$  values, while the 0.7 mm RRP shows a slight under-prediction. In figure 5b, the confidence interval from the extrapolations is shown to demonstrate variation in uncertainty depending on the field ranges that are used.

Only extrapolating up to 15 T can over-predict  $H_{irr}$  by 6% with confidence intervals exceeding 0.5 T. Including additional higher field measurements in the extrapolations show that closer to *Hirr* the over-prediction is  $\leq 3\%$  with the confidence interval dropping to about 0.2 T. As a matter of completeness, the PIT standard sample has no point at 15 T as we were unable to measure at 12 T, and the few points produce an unrealistically large confidence interval.

While the Kramer expression does approximately linearize the data, we found that  $f_k$  over-predicts *H*<sub>irr</sub> by up to 1.6 T when using the typical 12-15 T range for the extrapolation (see table 2). The actual irreversibility field, *Hirr*, and extrapolations, *H<sup>k</sup>* , from different ranges are shown in table 2 for all wires.

The round PIT wire with a standard HT and the 0.85 mm RRP wire had the highest *Hirr* at 26.1 and 25.8 T, respectively. The 0.7 mm RRP wire had the lowest *Hirr* of 24.9 T (however, we note that its



**Figure 2:** Raw I-V curves for RRP 0.85 mm wire from 24-25.5 T. Despite the  $\sim$ 100  $\mu$ V noise, the resistive transitions are clearly seen.



**Figure 4:** Kramer plot of mid-field and highfield extrapolations. The legend indicates the field ranges of the different extrapolations.



**Figure 3:** *J<sup>c</sup>* dependence on applied magnetic field for all samples. All PIT wires are 0.85 mm diameter.

**Table 2:** Measured  $H_{irr}$  values compared to  $H_k$ extrapolations from different field ranges. The extrapolation in the typical 12-15 T range shows an over prediction of *Hirr* by up to 1.5 T. Extrapolation from fields above 20 T are much closer to the true value.



HT is 15°C lower than for the 0.85 mm RRP wire). The PIT wires which underwent the IMHT, both round and rolled, had *Hirr* of 25.5 T, about 0.5 T less than the PIT wire with the recommended standard HT.



**Figure 5:** In plot (a) we normalized the extrapolated Kramer field  $(H_k)$  to the measured irreversibility field (*Hirr*) and plotted this value against the highest field in the extrapolated field range, starting at 12 T. For example, the point at  $(\sim 19, 0.98)$  uses the data from 12-19 T, and predicts an  $H_{irr}$  98% of the true value. The 0.85 mm wires all have over predicted  $H_k$  values, while the 0.7 mm is slightly under predicted. In (b), the confidence interval from the extrapolations is shown. The PIT standard sample has no point at 15 T as we were unable to measure at 12 T, and the few points produce an unrealistically large confidence interval. It can be seen that the confidence interval falls to  $\sim 0.2$  T by 20 T for all samples.

#### **4. Discussion**

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For many years, Nb<sub>3</sub>Sn wires have been characterized by measuring  $J_c$  from 12 to 15 T using the Kramer extrapolation to predict the irreversibility field. There is a well-developed correlation between higher  $J_c$  at 12-15 T and higher  $H_{irr}$ . As we are considering Nb<sub>3</sub>Sn for magnets operating at up to about 20 T, it is important to know the true high field properties to fully understand their operating margins. To this end it was recently found by Tarantini *et al.* [11] that this commonly used mid-field Kramer extrapolation consistently over predicts *Hirr* by more than 2 T using Vibrating Sample Magnetometry (VSM) up to 30 T. The data reported here confirms these earlier VSM conclusions that *Hirr* cannot be reliably predicted using Kramer extrapolations from 12-15 T for RRP wires and also demonstrates that the same issue exists for PIT conductors (figure 5). We also demonstrate that this inaccuracy is not dependent on the measurement technique, as both transport and VSM show similar overestimations. Using different field ranges above 15 T for the extrapolation can reduce this inaccuracy to only  $\sim 0.5$  T. However, this requires access to magnets generating more than 15 T, which are not commonly available for such measurements.

We also validated here that the 0.7 mm RRP wire has almost 1 T lower  $H_{irr}$  than the 0.85 mm RRP wire, likely impacted by the 15 °C lower HT temperature as lower reaction temperatures have been shown to produce lower *Hirr* values [18]. Additionally, this wires Kramer extrapolation was the only to under predict its *Hirr*, though more measurements are required to properly interpret this result.

This set of PIT samples also allowed us to study how the new IMHT would affect *Hirr*, and if rolled wires had different high field performance then round wires. Despite the degradation in *J<sup>c</sup>* , produced by rolling, the PIT IMHT wires had the same *Hirr* for both round and rolled samples. This suggests that the initial part of the small grain A15 layer which forms before the Sn leaks out maintains a high Sn content in these wires, even in filaments which are compromised from rolling. Additionally, the Snpoor Nb3Sn which forms towards the end of the reaction likely only contributes to transport current at lower fields.

The overall 0.6 T reduction of *Hirr* from the typical HT to the IMHT may be due to a reduced amount of Sn in the Nb<sub>3</sub>Sn layer. In fact, the high temperature stage seems to cause a higher  $A15$ phase nucleation rate which generates a thicker small grain A15 layer. However, the overall Sn content of the A15 layer may be lower, supressing *Hirr*. Further analysis to determine the composition of the Nb3Sn layer by EDS mapping will be performed to verify this hypothesis.

Additionally, there is commonly known to be slight curvature in the Kramer extrapolation depending on the field range [19][20], however, we found it difficult to resolve with our 0.5 T steps. We will determine if these wires do show similar behaviour during future measurements.

#### 5. **Conclusions**

The Kramer extrapolation of measurements in the mid-field range from 12-15 T has been widely used to predict the irreversibility field of  $Nb<sub>3</sub>Sn$  wires. The high field transport measurements presented here show that the Kramer extrapolation typically overestimates *Hirr* by up to 1.6 T for PIT and RRP wires reacted with various heat treatments. Although there are ongoing efforts to determine a reliable extrapolation method, our results suggest that the only way to reliably determine  $H_{irr}$  of these conductors is to measure transport current until *Hirr* is reached. Additionally, our investigation reveals that, although the inverted multistage heat treatment forms more  $Nb<sub>3</sub>Sn$  [6,21], this is accomplished by negatively affecting  $J_c$  and  $H_{irr}$ . On the other hand the rolled PIT conductor shows lower  $J_c$  than its round equivalent but maintains an identical *Hirr*. The causes of these behaviours require further investigations.

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