INELASTIC DIFFRACTIVE SCATTERING AT THE CERN ISR

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Abstract

The properties of the diffractive peak observed in the mass spectra of systems recoiling against observed high momentum protons emerging from pp collisions at the CERN ISR have been investigated. The cross-sections in this peak have been found to have a steep t-dependence which flattens out as |t| increases. The high mass side of the peak varies approximately as $1/M^2$ (where M is the missing mass of the recoiling system) and scales well in terms of the variable M^2/s . The position of the maximum has been observed to move to lower values of M^2/s as the kinematic boundary of this variable decreases with increasing s. The measured cross-sections, integrated up to $M^2/s = 0.05$, rise by $(15 \pm 5)\%$ over the s range 549 to 1464 GeV².

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Introduction

An earlier experiment at the ISR to study the reaction:

$$p + p \rightarrow p + X$$

has shown the existence of a peak in the mass spectrum of the unobserved system χ^{1}). This peak has been associated with the diffractive excitation of one of the incident protons; results on its shape and dependence on t and s have been subsequently published by several groups 2).

Several predictions have been made about the s-dependence of the diffractive excitation cross-section; a specific question which has been raised is the extent to which this process might contribute to the rise in the total cross-section measured through the ISR energy range 3)4). The aims of the present experiment have been both to extend the s and t ranges of the measurements of the inclusive proton spectrum and to improve their precision so that more accurate conclusions about scaling in the diffractive peak, and its contribution to the total inelastic cross-section, could be reached.

2. Experimental Method

A magnetic spectrometer placed above one of the circulating beams near intersection 2 at the ISR was used to detect emitted protons. The spectrometer, shown in fig. 1, consisted of 2 septum magnets whose apertures could be positioned to within 50 mm of the ISR beam, 3 bending magnets, a system of 21 magnetostrictive wire spark chambers, a series of trigger scintillation counters, and 3 gas Cerenkov counters. The position of the two septum magnets could be varied so that a total angular range from 30 to 180 mrad could be covered in successive settings with an angular width of \pm 5 mrad. The design and operation of the spectrometer have been described previously 5).

In the present experiment two changes were made to the normal spectrometer to improve the momentum resolution. The two ethylene-filled Cerenkov counters, which had previously been used

to distinguish protons from pions and kaons, were lifted out of the spectrometer to reduce the multiple scattering along the 30 m flight path. All positive high momentum particles were then assumed to be protons (the pion and kaon contamination having been measured to be less than 1 in 10^3 for particles having more than 90% of the maximum possible momentum⁶). Hall probes were mounted in all the spectrometer magnets so that the fields could be monitored to an accuracy of better than 1 part in 10^3 .

The production angle could be measured by the spectrometer with a precision of about 0.2 mrad, corresponding to an accuracy of $\sim 0.5\%$ in momentum transfer. The accuracy in the measured momentum, $\delta p/p$, varied between 0.6% and 1.1% FWHM from the lowest to the highest production angles (this variation was due to the different magnetic fields used at different angular settings; the resolution was nearly independent of the ISR beam energy, as the bending angles in the magnets depended only on the angular setting). The mean deviations of all spark positions from the calculated track were less than 0.1 mm. Tracks with spurious spark positions or secondary scatters were rejected by a consistency check on momenta, track angles and positions in different parts of the spectrometer. The production angle, the vertex position in the beam-beam plane and the momentum were fitted to the positions in the 12 chambers which determined the vertical coordinates. One kink in the fitted track was allowed, to take care of the effects of

The value of M, the missing mass of the system X, is related to the centre of mass energy $\mathbf{E}_{\mathbf{p}}$ of the observed proton by

multiple scattering.

$$M^2 = s + m_p^2 - 2 \sqrt{s} E_p$$
 (1)

For large values of s and for $M^2 >> m_p^2$ this can be approximated by

$$M^2 = s (1 - x), (2)$$

where x is the Feynman variable x = $2p_L/\sqrt{s}$. Thus the accuracy of M^2 depends on the accuracy with which the incident momenta and p_L are known. It can readily be shown that

$$(\delta M^2)^2 = (4(p_1 - p_3)\delta p_2)^2 + (4p_2\delta(p_1 - p_3))^2,$$
 (3)

where p_1 is the momentum of the incident proton in beam 1 (travelling towards the spectrometer), p_2 is that of the proton in beam 2 and p_3 is that of the proton detected in the spectrometer. In the case of low M^2 (<< s) the first term in the equation is much smaller than the second, even though there is a 2% uncertainty in p_2 because of the energy spread in the ISR. By extrapolation of the fitted track the radial position in beam 1 of the interaction point was determined to $\frac{1}{2}$ 1 mm; using the ISR momentum compaction function the value of p_1 for the intersecting proton could be determined to 0.2% (limited by the amplitude of the radial betatron oscillations). The effect of making this refinement is shown in fig. 2, which shows a measured momentum spectrum (35 mrad production angle, 11.7 to 12.1 GeV in beam1; 22.2 to 22.8 GeV in beam 2) which is dominated by elastic events. The error in M^2 is then given to a good approximation by

$$\delta M^2 \approx s \delta p_3/p_3 \approx s \delta x.$$
 (4)

It should be noted that the missing mass resolution in a colliding beam experiment is inherently worse by a factor s/M^2 than in experiments using a stationary target with measurement of the recoiling target particle. In particular, the mass resolution of the present experiment was not adequate to study the resonance structure seen, for example s^8 , in the region s^8 .

A large fraction of the high momentum protons detected by the spectrometer were p - p elastic scattering events; these had to be identified and removed. A hodoscope of 38 scintillation counters (the'forward detector' of reference⁹⁾) and a set of 6 spark chambers were arranged around the outgoing beam 2. The counters covered all angles from 8 to 250 mrad with a resolution of 16

mrad, and the chambers covered 10 to 50 mrad vertically and $\stackrel{+}{-}$ 20 mrad horizontally. Elastic events were identified by a single charged particle detected in this system in a direction colinear in the vertical plane (in the c.m. system) with the spectrometer particle. Multiple scattering and interactions in the ISR beam pipe and in the scintillation counters required the colinearity cut to be 6 - 8 mrad wide in order to include all elastic events. Small corrections were made to allow for the inelastic contribution which satisfied the colinearity condition, and for the inefficiency of the spark chamber system. Fig. 3 illustrates the identification of elastic events in the spark chamber system with 15.4 GeV in each ISR beam and the spectrometer set at 40 mrad. The inelastic events do peak at zero colinearity angle, but much more gently than the elastic events. The shape of the inelastic distribution has been deduced from subsamples of the same data which contained different fractions of elastic events. At small angles the elastic events can be recognised easily by this method. At large momentum transfers,

be recognised easily by this method. At large momentum transfers, however, the elastic events become too rare for their contribution to be accurately determined in this way. In these cases elastic events could still be identified by imposing the further constraint that no additional charged particles were produced (in addition to the forward hodoscope a barrel-shaped system of 140 counters) covered almost 4m steradians around the intersection region). Another small correction was applied to this selection method to compensate for accidental counts.

The missing mass distributions for all events which satisfied the elastic criteria were used to monitor the momentum resolution and to check the momentum scale of the spectrometer. Where necessary small corrections ($\lesssim 0.3\%$) were made to the measured proton momenta in a run to ensure that the elastic peak centred at the proton mass. This correction was then applied to the inelastic events obtained from the same run. Typical elastic and inelastic missing mass distributions are shown in fig. 4. The differential elastic cross-sections d_{σ}/dt were compared with the measurements

of Barbiellini et al. $^{10)}$ (normalised using the Coulomb scattering data of Amaldi et al. $^{3)}$), and good agreement was found. An example of this comparison, at s = 549 GeV^2 , is shown in fig. 5. The measured differential elastic cross-sections are given in table I.

The inelastic diffractive distribution is known to have a steep t-dependence; in order to detect as large a fraction of this cross-section as possible it was necessary to extend the range of **4-momentum** transfer to small values of |t| . The smallest |t|($\sim 0.2 \text{ GeV}^2$) was achieved by positioning the spectrometer to its minimum angle and using the lowest operational momentum of the ISR (11.8 GeV) in the beam moving towards the spectrometer (beam 1). The selected momentum transfer was then increased when required by raising the spectrometer to larger angles. The t-range of this relatively low t data was kept constant by running with 11.8 GeV in beam 1. The s-dependence was investigated by setting beam 2 successively at 11.8, 15.4, 22.5, 26.6 and 31.4 GeV. The s-range was further increased by running with higher equal energies in the two beams, but this did not cover the smallest values of |t|. In all, nine different combinations of beam momenta were used; they are listed in table II, together with the t-ranges covered. Only the six combinations which produced data in the low-t range have been directly used in the analysis of s-dependence.

The luminosity of the interaction region was continuously monitored by two independent systems, each consisting of two telescopes of three scintillation counters. One telescope from each system was positioned immediately below each beam pipe. In this configuration the elastic events were avoided, which would otherwise have caused excessive sensitivity to source position. Each telescope subtended a solid angle of about 8 x 10⁻⁴ steradian at the intersection. The scintillation counters were made large (10 cm high by 40 cm wide) compared with the size of the ISR beams (• 0.2 cm x 4 cms), so that small vertical and radial shifts between different runs at the same ISR energy had a negligible influence on the counting rates. The counting rates dN_M/dt of these monitors were thus proportional to the luminosity L at the

intersection:

$$\frac{dN_{M}}{dt} = \sigma_{M}L. \qquad (5)$$

The luminosity L is related to the beam velocities $\underline{\beta}_1 c$ and $\underline{\beta}_2 c$, the number of particles per unit length, n_1 and n_2 , in the beams, the crossing angle $\alpha (= 14.8^{\circ})$ and the effective height h_{eff} at the intersection, by

$$L = \frac{cn_1n_2}{h_{eff} \sin\alpha} \sqrt{(\beta_1 - \beta_2)^2 - (\beta_1 \times \beta_2)^2}$$

$$= \frac{\sqrt{\beta_1 \beta_2} \operatorname{cn}_1 \operatorname{n}_2}{\operatorname{h}_{eff} \operatorname{tg}(\frac{1}{2}\alpha)} \left\{ 1 + (1 - \beta_1 \beta_2) \operatorname{tg}^2(\frac{1}{2}\alpha) + \frac{(\beta_1 - \beta_2)^2}{\beta_1 \beta_2 \cos^2(\frac{1}{2}\alpha)} \right\}$$
(6)

For all combinations of beam momenta between 11.8 and 31.4 GeV this differs less than 0.7% from the usual approximation

$$L \approx \frac{\operatorname{cn_1^{n_2}}}{\operatorname{h_{eff}} \operatorname{tg}(\frac{1}{2} \alpha)} . \tag{7}$$

At each combination of beam momenta the proportionality constant σ_M was determined from repeated measurements using the Van der Meer method 11). The value of σ_M ranged from 50 μb at 11.8/11.8 GeV to 650 μb at 31.4/31.4 GeV for one of the counter systems, and from 100 to 1300 μb for the other. In general the luminosity constants σ_M obtained over a period of more than one year were found to be consistent to within $^+$ 3%. The luminosities measured with both the systems in intersection 2 were compared periodically with simultaneous measurements made in the other intersection regions of the ISR. This comparison showed that changes in the I2 spectrometer settings did not severely influence the luminosity monitoring system.

As the relative normalisation of the data at different

s-values is vital to the determination of any s-dependence, all data were passed through the same procedure of Monte Carlo acceptance calculation, cross-section determination and elastic subtraction. Subsets of data in which the track reconstruction efficiency was less than 70% were not included in the final data sample. The uncertainty in the absolute normalisation of the data, from the total analysis procedure, could be as much as 15%, but the relative normalisation of all the data is thought to be accurate to within 5%. The data discussed in this paper have been taken over a period of approximately two years.

3. Results

The data have been analysed as invariant cross-sections ${\rm Ed}^3\sigma/{\rm dp}^3$ in terms of (i) the transverse momentum ${\rm p}_{\rm T}$ and the Feynman variable x of the detected proton for the range $0.7 < {\rm x} < 1$, and (ii) the momentum transfer variable t and the missing mass ${\rm M}^2$, in finer detail around the peak.

The data are presented in tables III -XX . Fig. 6 (a) shows the dependence on p_T and x; 6(b)-(d) show the dependence on t and M^2 . The errors given in tables and figures are purely statistical. The data show Feynman scaling (dependence on x and p_T but not on s) to a good approximation over the entire range of x and p_T covered.

No attempt has been made to sub-divide the inelastic data into diffractive and non-diffractive components using model-dependent fits. The high-x non-diffractive events come from the tail of the proton fragmentation spectrum; this contribution has been estimated to be small in the region x > 0.95 and essentially s-independent when analysed in terms of x and p_T or M^2/s and t.

4. t-dependence

Within any restricted range of t, say 0.5 GeV², cross-sections at given values of M² and s can be well represented by a simple exponential Ae^{bt}. Over a wider range of t the parameter b depends on t. A parametrisation which is less sensitive to the t-range considered is

$$\frac{s}{\pi} \frac{d^2\sigma}{dM^2dt} = Aexp (bt + ct^2)$$
 (8)

Two examples of such fits are shown in fig. 7. The parameters $b(M^2)$ and $c(M^2)$ from fits at s = 549 GeV² in the range $0.15 \le |t| \le 1.45 \text{ GeV}^2$ are shown in fig. 8. Data at all measured s-values show high values of b at low values of M², followed by a constant lower value for $M^2/s > 0.01$. Similar slope-mass correlations have previously been reported from other experiments on inclusive proton production 8,13,14 , and from experiments on the exclusive reaction pp \rightarrow p(n π^+) in the diffractive region 15,16). In this experiment the effect is most clearly seen at $s = 549 \text{ GeV}^2$ (possibly because the effect depends on M^2 and not on M^2/s , and the mass resolution is the best at the lowest value of s). There is agreement between these experiments if there is a small increase of b with s and the limited mass resolution of the present experiment is taken into account. The value of b outside the low- ${
m M}^2$ peak is about half the value found in elastic scattering. No significant s-dependence has been observed in the range 549 to $1464 \text{ GeV}^2 \text{ in s.}$

A b decreasing with increasing M² is natural in a triple Regge description of the diffractive peak. The effect is further enhanced in this model by the non-diffractive background being more important at large M². An impact parameter description of the slope-mass correlation has been given by Humble ¹⁷, for example; the decrease of b with increasing M² is caused by an increasing contribution of higher order s-channel helicity flip amplitudes. Several earlier attempts to describe this slope-mass correlation as a kinematical consequence of the Deck effect have been criticised ¹⁸. The present data exclude a parametrisation

$$b = b_o + c/(M^2 - m_p^2),$$
 (9)

with $b_o \approx 3 \text{ GeV}^{-2}$, proposed by Lubatti and Moriyasu¹⁹.

In order to study the overall t-dependence of the diffractive

peak, the invariant cross-sections have been integrated over M²/s from the largest negative values (to include resolution effects) to $M^2/s = 0.05$. This upper limit is somewhat arbitrary, but over this region $\sim 98\%$ of the inclusive cross-section is estimated to be diffractive, by fitting to a formula of the triple Regge type. Extrapolation of the fits to high M², however, indicates that as much as one third of the total diffractive cross-section could be contained in the region $M^2/s > 0.05$. Fig. 9 shows the t-dependence of these integrated data over the entire measured range of the experiment. There is no indication of either the diffraction minimum seen in the t-dependence of the elastic scattering cross-section, nor of the break in the t-distribution of low mass excitation seen in the exclusive channel $pp \rightarrow p(n\pi^+)^{15}$. After integration over the range of excited masses the t-dependence of pp $\rightarrow \bar{p}(n\pi^+)$, measured at $\sqrt{s} = 53 \text{ GeV}^{15}$, and $pp \rightarrow p(p\pi^{+}\pi^{-})$, measured at $\sqrt{s} = 45 \text{ GeV}^{20}$, are very similar to that of the total diffractive cross-section for $M^2/s < 0.05$. This is illustrated in fig. 9. For $|t| < 0.6 \text{ GeV}^2$ each of these channels contributes about 10% to the total; at larger |t| the t-dependence of the total inelastic cross-section for $M^2/s < 0.05$ flattens out. Out to the largest momentum transfer ($|t| = 4 \text{ GeV}^2$) the s-dependence in the data is small; this indicates that large angle diffraction scattering is not a likely source of hightransverse momentum particles at large angles.

At small momentum transfers a triple Pomeron description has been successfully applied in the past 12). In such a description the t-dependence is mainly determined by the proton form factor squared, and to a lesser extent by a nearly t-independent Pomeron-proton total cross-section and a weak t-dependence from the slope of the Pomeron trajectory. Though such a description can be continued to larger momentum transfers another regularity appears for $|t| > 1 \text{ GeV}^2$, where the t-distribution starts to behave as

$$d\sigma/dt \propto s^{-m} f(\theta)$$
 (10)

Least squares fits in this region gave as best fitted value m = 3.85. The fits are shown in fig. 10. A power law

behaviour is expected at large angles on the basis of parton and constituent interchange models 21). It seems that at ISR energies a similar behaviour is observed at angles below 100 mrad.

 $\frac{5. \text{ M}^2/\text{s-dependence}}{\text{The M}^2/\text{s-dependence}}$ at two values of t is reproduced in fig. 11. The data are seen to scale well in terms of this variable through the high mass $(M^2/s > 0.01)$ diffractive region. The function s/M^2 is shown as a dashed line in fig. ll(a) to demonstrate the approximate M² dependence of the data. A crosssection which falls as s/M^2 is predicted for triple Pomeron coupling near t = 0 and has previously been reported by several aroups (12)(13)(22). The non-invariant cross-sections $d^2\sigma/dtdM^2$ would also be independent of s in a region where the invariant crosssection data both scale in terms of the variable M^2/s and also have a s/M^2 dependence. At larger |t| the spectra start to deviate from the s/M^2 dependence, but still show scaling in M^2/s . This is demonstrated in fig. 11(b) for $t = -1.45 \text{ GeV}^2$. The gradual change with t of the M^2/s dependence of the spectra has been the basis of an estimate of the Pomeron slope parameter, $\alpha_p \simeq 0.2$, in an earlier publication 12).

The behaviour of the cross-sections near the kinematic boundary $(M_p + M_\pi)^2/s$ can be deduced only indirectly in this experiment. Because of the experimental resolution only the mean position of the inelastic cross-section peak on the M^2/s -scale, defined as the weighted mean for $M^2/s < 0.02$, can be determined. It shows a small shift to lower M²/s with increasing s. The movement relative to the elastic peak position at $t = -0.3 \text{ GeV}^2$ is shown in fig. 12(a). The statistical errors in the mean values of M²/s correspond to accuracies of the order of $\frac{\delta p}{p} = \pm 2 \times 10^{-4}$. These accuracies have been achieved by taking mean values in samples of $\sim 10^5$ events per data point , and cannot be obtained from the data tables in which the M^2/s scale is adjusted with an

accuracy $\frac{\delta p}{p} \sim \pm 5 \times 10^{-4}$. Systematic errors resulting from the elastic subtraction procedure are t-dependent, but are also estimated to be of the order of $(1 \text{ to } 2) \times 10^{-4}$. The effect of the experimental resolution has been taken into account in calculating the mean position of the inelastic peak. The t-dependence of the quantity $\Delta M^2/s = \langle M^2/s \rangle_{\text{inel}} - m_p^2/s$ is shown at a mean value of $s = 1000 \text{ GeV}^2$ in fig. 12(b). This figure indicates that a simple M^2/s dependence, which would imply no t-dependence in $\Delta M^2/s$ is inadequate to describe the snape of the inelastic cross-section at very small values of M^2/s . The curves drawn on the figure have been calculated from a parametrisation of the data as

$$E d^{3}g/dp^{3} \propto (v/s)^{-1-0.2 t}$$
 (11)

with $v = M^2 - m_p^2 - t$, and a fixed lower limit in M_{min}^2 at 1.4 GeV². Such a parametrisation is compatible with the recent high resolution data of Akimov et al.⁸⁾ at small |t| and an s-range overlapping that of the present experiment. The s and t dependences of $\Delta M^2/s$ shown in fig. 12 are qualitatively described by this simple parametrisation, though a lower limit of $M_{min}^2 = 1.2$ GeV² would give better quantitative agreement with the data.

6. s-dependence

The s-dependence of the total diffraction peak can be obtained after successive integrations over M²/s and t. Figs. 13 (a) and 13 (b) show examples of the s-dependence at fixed t for two different integration ranges in M²/s. In these figures, a 5% error has been added in quadrature to the statistical errors to take account of possible systematic uncertainties between the data at different s values. The cross-sections integrated over M²/s from - ∞ to 0.01 (fig. 13(a)) show a rise of \sim 35% over the s-range 549 to 1464 GeV². When the upper integration limit is increased to M²/s = 0.05 (fig.13(b)), this rise reduces to \sim 15%, demonstrating that the rise in the cross-section is concentrated in the low M² region where the kinematic range increases with s.

Table XXI lists cross-sections integrated to $M^2/s = 0.05$ for all s and t values covered in this experiment.

In order to estimate the s-dependence of the total single diffractive cross-section (with $M^2/s < 0.05$), the data have been integrated using the quadratic exponential t-dependence described in eqn. 8. This procedure can be applied in the low-s, low-t range of the experiment where measurements with asymmetric ISR energies have been done. Even at these s-values the procedure implies extrapolation over a factor of 3 in cross-section on the low | t | side. At s = 549 GeV^2 and 934 GeV^2 the t-ranges of the measurements have been extended to $0.15 < |t| < 1.45 \text{ GeV}^2$ and $0.25 < |t| < 2.00 \text{ GeV}^2$ respectively, so that a value of c could be determined from $|t| < 1.45 \text{ GeV}^2$. The t-ranges covered at the other s-values were too limited to determine c accurately, so the mean value found from the data with the larger t range $(c = 1.77 \pm 0.15 \text{ GeV}^{-4})$ was used at all s values. At small | t | the parametrisation can be approximated by a simple exponential with slope b. The values of b obtained in the present experiment show no significant s-dependence, and the mean value obtained, 7.13 \pm 0.05 GeV⁻², is in good agreement with the average value 7.0 $^{\pm}$ 0.4 GeV $^{-2}$ found in the region 0 < | t | < 0.5 GeV 2 by several experiments at FNAL 14)22)23). The parametrisation thus found has been integrated numerically in the range $0 < |t| < 1 \text{ GeV}^2$. The high | t | data (see fig. 9) can be approximated by a simple exponential function in the range $1.0 < |t| < 3.0 \text{ GeV}^2$. The contribution of this part is estimated from data at $s = 2783 \text{ GeV}^2$ to be \leq 1% of the total inelastic diffractive cross-section.

The integrated cross-sections have been doubled, to account for the equal probabilities of the reactions $p_1p_2 \rightarrow p_1X$ and $p_1p_2 \rightarrow Xp_2$, and are listed in column 2 of table XXII. The variation of the total single diffraction cross-section, σ_{SD} (M²/s < 0.05), is shown in fig. 14 and indicates a rise of (15 $^+$ 5)% over the measured s-range. The curves drawn on this figure represent the s-dependence of both a diffraction component which rises by the same amount as the total inelastic cross-section, and a diffractive component which remains a fixed fraction of the inelastic cross-

section. The data favour the second possibility, implying that the single diffractive cross-section (for $M^2/s < 0.05$) cannot account for a large fraction of the rise of the total inelastic cross-section. The result is in agreement with the more speculative conclusion reached in an earlier experiment 12).

Although the relative normalisations of the total inelastic cross-sections obtained above are thought to be accurate to $\sim 5\%$, their absolute normalisations are only known to within $\sim 15\%$. Comparisons of the elastic data obtained in the present experiment with published data 3 indicate that the small angle cross-sections reported here are higher by up to 15%.

The measured cross-sections integrated up to $M^2/s = 0.10$ are given in column 3 of table XXII; they are compared with results from both a hydrogen jet experiment 24 and several bubble chamber experiments $^{14}(22)(23)$ in fig. 15. The present cross-sections are $\sim 20\%$ higher than those found by Schamberger et al. 24 by extrapolation from a restricted t-range, |t| < 0.22 GeV using a single exponential in t. These authors, however, point out that their cross-sections could rise by as much as 10% if d_{0}/dt were to flatten out at large |t|. The flattening t-dependence found in the present experiment indicates that such a 10% rise is expected and the cross-sections deduced from reference 24 by making this increase are shown dotted in fig. 15. With this correction the results from the various experiments are in good agreement within the overlapping s-range.

7. Conclusions

The following properties of the diffractive peak have been determined.

1) t-dependence.

The dependence on t becomes weaker as |t| increases, and a simple exponential in t can only be used to describe the data over a limited t range. No indication of a diffractive dip has been observed in the range $0.2 < |t| < 4 \text{ GeV}^2$. For $|t| > 1 \text{ GeV}^2$ the t-dependence of the integrated diffractive peak can be approximated by a power law behaviour in s at fixed angle. The

t-slope decreases with increasing mass and eventually becomes mass independent.

2) M²-dependence.

For small |t| the long tail of the diffractive peak falls approximately as $1/M^2$ over the range $0.005 < M^2/s < 0.035$. A more complicated M^2 dependence is present at small values of M^2 , where a t-dependent effective cut off has been deduced from a shift of the peak of the inelastic cross-section towards the falling M_{min}^2/s limit as s increases.

3) s-dependence.

The data scale well in terms of the variable M^2/s ($\sim 1-x$) for $M^2/s > 0.01$. For smaller values of M^2/s the integrated crosssections rise with increasing s. This effect leads to a total single diffraction component which, when integrated up to $M^2/s = 0.05$ increases by $(15 \pm 5)\%$ over the range s = 549 to 1464 GeV^2 .

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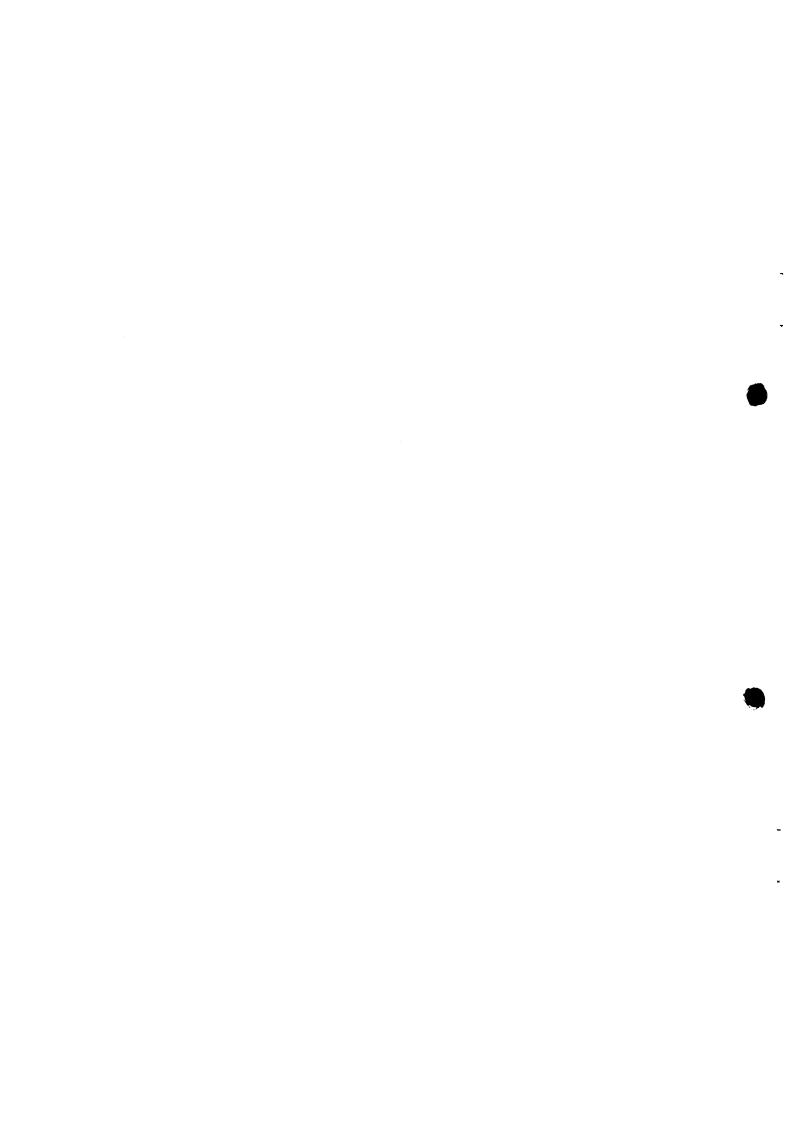
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Figure captions

- Fig. 1 Schematic side and plan view of the apparatus.
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- Fig. 15 Comparison of the single diffractive cross-section for

 ${
m M}^2/{
m s} < 0.10$ measured by several experiments. The data of ref. 24 have been increased by 10% (to account for the decreasing t-dependence at higher t observed by the present experiment) and are shown dotted.



-						
		ELASTIC	ELASTIC CROSS-SECTIONS $\frac{dg}{dt}$ (mb. GeV ⁻²)	$\frac{\alpha}{t}$ (mb. GeV ⁻²)		
-t (GeV ²)	s = 549 GeV ²	s = 725 GeV ²	$s = 934 \text{ GeV}^2$	s = 1047 GeV ²	s = 1239 GeV ²	s = 1464 GeV ²
0.15	16.77 ± 0.12	12.32 ± 0.17				
0.20	9.55 ± 0.06	8.84 ± 0.09		9.39 ± 0.22	9.74 ± 0.12	10.16 ± 0.08
0.25	5.40 ± 0.04	4.63 ± 0.04	5.27 ± 0.19	6.04 ± 0.15	4.64 ± 0.06	5.99 ± 0.05
0:30	3.15 ± 0.03	2.91 ± 0.03	3.02 ± 0.11	3.39 ± 0.09	. 2.80 ± 0.05	3.22 ± 0.04
0.35	2.04 ± 0.03	1.66 ± 0.02	1.98 ± 0.07	1.96 ± 0.08	1.64 ± 0.02	2.00 ± 0.03
0.40	1.20 ± 0.03		1.24 ± 0.04			
0.45	0.720 ± 0.023	0.67 ± 0.01	0.76 ± 0.03		0.644 ± 0.014	0.638 ± 0.016
05.0	0.425 ± 0.014	0.40 ± 0.01	0.44 ± 0.02		0.404 ± 0.009	0.337 ± 0.012
0.55	0.258 ± 0.010	0.20 ± 0.01	0.251 ± 0.010		0.243 ± 0.005	0.209 ± 0.009
09.0	0.175 ± 0.003		0.179 ± 0.009			0.135 ± 0.008
0.65	0.100 ± 0.006		0.106 ± 0.008		0.087 ± 0.003	
0.70	0.068 ± 0.005		0.069 ± 0.003			0.047 ± 0.006
0.75	0.047 ± 0.004		0.044 ± 0.004		0.033 ± 0.003	
03.0	0.025 ± 0.004		0.031 ± 0.003			
0.35	0.019 ± 0.002		0.021 ± 0.003			
0.90	0.011 ± 0.002		0.015 ± 0.002			
0.95	0.009 ± 0.002	·	0.007 ± 0.002			
1.00	0.006 ± 0.002					
1.05	0.005 ± 0.002		Table I			

TABLE II

t RANGE COVERED (GeV) ²	0.15 - 1.45	0.15 - 0.55	0.25 - 2.00	0.20 - 0.35	0.20 - 0.75	0.20 - 0.70	0.45 - 3.55	0.65 - 4.15	1.15 - 2.65
c.m. ENERGY s (GeV ²)	549	725	934	1047	1239	1464	1995	2783	3892
BEAM 2 MOMENTUM (GeV)	11.8	15.4	15.4	22.5	26.6	31.4	22.5	26.6	31.4
BEAM 1 MOMENTUM (GeV)	11.8	11.8	15.4	11.8	11.8	11.8	22.5	26.6	31.4

	p _T = 1.1	- GeV/c																			12 + 0 0	0.17 + 0.02	ı +	0.22 = 0.02	1 +	1 +	0.09 - 0.01	
	$p_T = 1.0$	GeV/c										0 28 + 0 0	0.29 + 0.02	+1	+	ı +	ı +	1 +1	0.20 ± 0.02	0.18 + 0.02	+1	+1	+	1 +	۱ +	50.0 - 10.1	1 +1	
	P _T = 0.9	GeV/c								0.47 ± 0.03	+1	+1	+1	+1	+1	+	+	+1	+1	+1	+1	+1	+1	+1	+	1 +	1 +1	
s = 549 GeV ²	P _T = 0.8	GeV/c								0.99 ± 0.04	+1		+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+	+	+1	- 1
	7.	GeV/c	2.13 ± 0.06	1.91 ± 0.05	+1	+1	+1	+1	+1	1.52 ± 0.04	1.59 ± 0.05	+1	+1	+1	+1	+1	+1	+1	1.47 ± 0.05	1.54 ± 0.06	1.71 ± 0.06	+1	+1	+1	+1	+1	+1	
4 E d ³ o/dp³ (m	b.0 = Tq	GeV/c	2.99 ± 0.08	2.95 ± 0.08	3.03 ± 0.08	+1	2.90 ± 0.08	2.66 ± 0.08	2.68 ± 0.08	2.60 ± 0.07	2.56 ± 0.08	2.60 ± 0.08	2.45 ± 0.08	2.47 ± 0.09	+1	+1	+1	2.51 ± 0.09	2.89 ± 0.10	3.37 ± 0.11	3.74 ± 0.12	4.32 ± 0.13	4.97 ± 0.13	+1	18.32 ± 0.25	+1	+1	
INELASTIC CROSS-SECTION E $d^3\sigma/d\bar{p}^3$ (mb.GeV ⁻²);	$P_T = 0.5$	GeV/c	4.51 ± 0.13	4.33 ± 0.14	4.64 ± 0.15	4.73 ± 0.15	4.51 ± 0.13	4.38 ± 0.15	4.48 ± 0.13	4.38 ± 0.14	5.17 ± 0.15	5.26 ± 0.15	4.94 ± 0.14	4.94 ± 0.14	4.99 ± 0.13	5.46 ± 0.14	5.39 ± 0.13	5.58 ± 0.14	5.62 ± 0.13	6.31 ± 0.14	6.57 ± 0.14	8.40 ± 0.16	9.65 ± 0.18	13.74 ± 0.21	33.42 ± 0.32	57 ±	0.31 ± 0.04	
INELAST	P _T = 0.4	GeV/c	8.66 ± 0.22	8.80 ± 0.25	9.01 ± 0.23	8.40 ± 0.21	8.91 ± 0.20	9.09 ± 0.21	8.74 ± 0.18	8.45 ± 0.18	9.42 ± 0.19	9.02 ± 0.18	9.18 ± 0.17	8.74 ± 0.17	9.45 ± 0.17	9.28 ± 0.18	+1	9.18 ± 0.17	9.24 ± 0.19	+1	+1	12.89 ± 0.25	+1	+1	41.52 ± 0.57	+1	0.64 ± 0.10	
	$p_T = 0.3$	GeV/c	12.95 ± 0.25	+1	12.87 ± 0.25	11.73 ± 0.25	11.62 ± 0.24	11.26 ± 0.24	11.05 ± 0.24	11.05 ± 0.24	+1	10.50 ± 0.28	10.03 ± 0.28	10.10 ± 0.31														
	×		.702	.715	.728	.740	.753	.766	.779	.792	804	.817	.830	.843	.856	.869	.881	.894	-907	.920	.933	.945	.958	.971	-984	766.	1.009	

	T	1															
	p _T = 0.8 GeV											0.9 ± 0.2	1.0 ± 0.1	1.0 ± 0.1	2.1 ± 0.1	2.7 ± 0.2	
725 GeV ²	p _T = 0.7 GeV								1.6 ± 0.2	1.5 ± 0.1	1.5 ± 0.1	1.4 ± 0.1	1.6 ± 0.1	2.0 ± 0.1	4.2 ± 0.2	5.7 ± 0.3	
$(GeV^{-2}); s = 7$	P _T = 0.6 GeV					2.8 ± 0.2	2.9 ± 0.2	2.5 ± 0.1	2.4 ± 0.1	2.6 ± 0.1	2.4 ± 0.1	2.5 ± 0.1	2.6 ± 0.1	3.5 ± 0.2	7.3 ± 0.4	12.2 ± 0.6	
INELASTIC CROSS-SECTION E $d^3\sigma/d\bar{p}^3$ (mb.GeV ⁻²); s = 725 GeV ²	P _T = 0.5 GeV		5.1 ± 0.3	4.4 ± 0.3	4.5 ± 0.2	4.5 ± 0.2	4.5 ± 0.2	4.5 ± 0.2	4.3 ± 0.2	4.0 ± 0.2	3.9 ± 0.2	4.4 ± 0.2	4.6 ± 0.3	5.8 ± 0.3	12.2 ± 0.6	29.2 ± 1.5	
CROSS-SECTION	P _T =0.4 GeV		7.5 ± 0.4	7.0 ± 0.4	7.1 ± 0.4	7.0 ± 0.4	6.8 ± 0.4	7.0 ± 0.4	6.8 ± 0.4	7.0 ± 0.4	7.1 ± 0.4	7.3 ± 0.4	7.8 ± 0.5	10.6 ± 0.6	22.8 ± 1.3	66.0 ± 3.6	
INELASTIC	$p_T = 0.3$ GeV		10.3 ± 0.6	10.2 ± 0.6	10.2 ± 0.6	10.2 ± 0.6	10.2 ± 0.6	10.7 ± 0.6	10.8 ± 0.6	11.5 ± 0.7	10.9 ± 0.8	12.1 ± 1.1	12.3 ± 1.2	14.9 ± 1.5	34.3 ± 3.1	169.2 ± 14.1	
	×		0.616	0.646	0.676	0.705	0.735	0.765	0.794	0.824	0.854	0.883	0.913	0.943	0.975	0.995	

TABLE IV

INELASTIC CROSS-SECTION E $d^3\sigma/d\bar{P}^3$ (mb.GeV ⁻²); s = 934 GeV ²	$p_T = 0.5$ $p_T = 0.6$ $p_T = 0.7$ $p_T = 0.8$ $p_T = 0.9$ $p_T = 1.0$ geV geV geV geV	.97 ± 0.27 3.00 ± 0.16 1.90 ± 0.16	3.26 ± 0.14	2.78 ± 0.11	.52 ± 0.17	2.53 ± 0.10 1.58 ± 0.07	.87 ± 0.19 2.60 ± 0.10 1.52 ± 0.06 0.79 ± 0.05	.87 ± 0.19 2.73 ± 0.11 1.34 ± 0.06 0.72 ± 0.04 0.42 ± 0.05	.05 ± 0.20 2.62 ± 0.10 1.39 ± 0.06 0.75 ± 0.04 0.40 ± 0.04	2.87 ± 0.11 1.52 ± 0.06 0.82 ± 0.04	3.41 ± 0.13 1.84 ± 0.07 0.95 ± 0.04 0.49 ± 0.03	5.05 ± 0.19 2.57 ± 0.10 1.34 ± 0.06 0.70 ± 0.04	17.73 ± 0.77 8.09 ± 0.31 4.11 ± 0.16 1.88 ± 0.07	1.47 ± 0.05 0.56 ± 0.05 0.26 ± 0.02 0.09 ± 0.01
INELASTIC CROSS-SECTION	.5	4.97 ± 0.27 3.00 ± 0.			4.52 ± 0.17 2.84 ± 0. 4.79 ± 0.18 2.63 ± 0.	4.78 ± 0.18 2.53 ± 0.	4.87 ± 0.19 2.60 ± 0.	4.87 ± 0.19 2.73 ± 0.	5.05 ± 0.20 2.62 ± 0.	5.75 ± 0.23 2.87 ± 0.	6.25 ± 0.26 3.41 ± 0 .	10.21 ± 0.45 5.05 ± 0.	29.96 ± 1.53 17.73 ± 0.	4.01 ± 0.38 1.47 ± 0.0
	x p _T = 0.4 GeV	0.676 8.1 ± 0.4			0.753 7.5 = 0.4	0.805 9.3 ± 0.5	0.831 8.7 ± 0.5		0.884 8.7 ± 0.7	0.910 9.9 ± 1.0	0.936 12.3 ± 1.6	0.963	0.992	1.008

TABLE V

INELAS	TIC CROSS-SECTION	E d ³ σ/dp ³ (mb.C	INELASTIC CROSS-SECTION E $d^3\sigma/d\bar{p}^3$ (mb.GeV ⁻²); s = 1047 GeV ²
×	p _T = 0.4 GeV	P _T = 0.5 GeV	P _T = 0.6 GeV
0.810	7.5 ± 0.4		
0.835	7.7 ± 0.4		
0,860	7.8 ± 0.4	4.7 ± 0.3	
0.885	8.4 ± 0.4	4.5 ± 0.3	
0.909	9.0 ± 0.4	5.7 ± 0.3	2.7 ± 0.4
0.934	10.7 ± 0.5	6.7 ± 0.3	3.1 ± 0.3
0.959	14.6 ± 0.7	8.7 ± 0.4	4.8 ± 0.3
0.987	46.1 ± 2.1	28.1 ± 1.1	16.0 ± 0.7
1.002	37.0 ± 2.8	17.6 ± 1.2	7.0 ± 0.5
1.028	0.02 ± 0.03	0.01 ± 0.01	0.01 ± 0.01
			

TABLE VII

	INELASTIC G	ROSS-SECTION E	d ³ σ/dp³ (mb.GeV	INELASTIC CROSS-SECTION E $d^3\sigma/d\bar{p}^3$ (mb.GeV ⁻²); s = 1464 GeV ²	;eV ²	
×	P _T = 0.3 GeV	p _T = 0,4 GeV	p _T = 0.5 GeV	p _T = 0.6 GeV	P _T = 0.7 GeV	$p_{T} = 0.8$ GeV
0.703	11.5 ± 0.5	8.78 ± 0.34	5.35 ± 0.23	3.20 ± 0.16	2.01 ± 0.26	
0.729	12.2 ± 0.5	8.89 ± 0.33	5.21 ± 0.21	3.01 ± 0.15	1.72 ± 0.16	
0.755	11.8 ± 0.5	8.66 ± 0.32	4.69 ± 0.19	2.97 ± 0.14	1.66 ± 0.12	
0.781	10.6 ± 0.5	9.09 ± 0.33	5.00 ± 0.20	3.14 ± 0.15	1.33 ± 0.09	
0.807	10.5 ± 0.5	8.95 ± 0.32	5.01 ± 0.19	3.05 ± 0.14	1.31 ± 0.09	-
0.833	10.3 ± 0.6	9.36 ± 0.34	4.96 ± 0.20	2.88 ± 0.13	1.68 ± 0.10	0.72 ± 0.09
0.859		8.77 ± 0.33	5.35 ± 0.21	2.99 ± 0.14	1.58 ± 0.09	0.50 ± 0.06
0.885		9.09 ± 0.35	5.28 ± 0.21	2.91 ± 0.13	1.54 ± 0.09	0.63 ± 0.06
0.911		10.05 ± 0.40	5.76 ± 0.22	3.19 ± 0.14	1.68 ± 0.09	0.55 ± 0.05
0.937		11.08 ± 0.46	6.74 ± 0.25	3.66 ± 0.16	2.06 ± 0.11	0.84 ± 0.06
0.964		14.55 ± 0.62	9.73 ± 0.35	5.62 ± 0.22	3.08 ± 0.14	1.14 ± 0.07
0.992		49.39 ± 1.88	32.67 ± 1.05	18.80 ± 0.62	10.00 ± 0.36	3.61 ± 0.16
1.009		8.64 ± 0.73	3.25 ± 0.16	1.16 # 0.07	90.0 ± 69.0	0.33 ± 0.04

TABLE VIII

	INELASTI	ASTIC CROSS-SECTION	$E d^3 o / d\bar{P}^3 \text{ (mb.GeV}^{-2})$;	GeV^{-2}); s = 15	$s = 1995 \text{ GeV}^2$	(continued)	
×	$p_T = 1.3$ GeV	$P_T = 1.4$ GeV	$P_T = 1.5$ GeV	p _T = 1.6 GeV	ρ _T = 1.7 GeV	p _T = 1.8 GeV	p _T = 1.9 GeV
		×10 ⁻³	×10 ⁻³	×10 ⁻³	×10 ⁻³	×10 ⁻³	×10 ⁻³
0.645	62 ± 5						
0.663	83 ± 6						
0.681	79 ± 5	27.3 ± 3.8					
0.699	. 9 7 62	31.3 ± 3.3					
0.716	61 ± 5	32.1 ± 2.9					
0.734	9 + 89	27.7 ± 2.6	12.1 ± 2.6				
0.752	62 ± 5	32.1 ± 2.7	13.4 ± 2.1				
0.770	60 ± 5	31.3 ± 2.8	11.5 ± 1.7				
0.788	27 ± 6	22.5 ± 2.6	+1	4.4 ± 1.5			
908.0	43 ± 5	26.5 ± 2.7		6.7 ± 1.5			
0.824	43 ± 5	22.0 ± 2.5	12.6 ± 1.6	5.2 ± 1.1	3.5 ± 1.6		
0.842	37 ± 5	18.5 ± 2.6	12.3 ± 1.6	6.1 ± 1.2	3.6 ± 1.4		
098.0	31 ± 5	17.0 ± 2.8	11.0 ± 1.5	+1	3.2 ± 1.0		
0.878	26 ± 4	19.2 ± 3.0	11.7 ± 1.7	+1	+1		
968.0	26 ± 5	10.3 ± 2.5	10.8 ± 1.7	+1	+1	3.7 ± 1.4	
0.913	27 ± 5	10.1 ± 2.3	7.6 ± 1.6	6.8 ± 1.1	+1	+1	
0.931	33 + 6	13.1 ± 3.0	11.2 ± 2.3	7.8 ± 1.4	+1	+1	
0.949	35 ± 5	21.6 ± 3.8	13.0 ± 2.4	+1	+1	+1	
0.967	51 + 8	18.7 ± 3.8	15.1 ± 3.0	9.8 ± 1.9	+1	+1	
0.985	82 ± 10	49.3 ± 6.3	23.8 ± 4.4	19.3 ± 2.9	+1	+1	2.1 ± 1.1
1.003	37 ± 7	16.8 ± 3.7	8.1 ± 2.4	5.8 ± 1.6	2.6 ± 0.7	0.5 + 0.3	+1
1.021		8.0 ± 8.0					!

TABLE IX

_	1-																								
		p ₊ = 2.3	GeV	0 TX																	+	1.2 - 0.9			
nved)		$p_{T} = 2.2$	GeV	VIV																+	ı +	1 +	C.O - 5.1		
V ² (continued)		$p_T = 2.1$	GeV	214												+	1 4 + 0 4	ı +	+		۱ +	1 +		}	-
$3 = 2783 \text{ GeV}^2$		$p_T = 2.0$. GeV										+ *	+	+	+	+1	+	+	+ 1	+	+	+1		
$E d^3 \sigma/d\bar{p}^3$ (mb.GeV ⁻²);		$p_T = 1.9$	GeV								2.5 ± 1.2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	
1		$P_T = 1.8$	GeV x10 ⁻³						3.2 ± 1.3	3.5 ± 1.1	+1	5.1 ± 1.3	+1	+1	+1	+1	+1	+1	+1	+1	+1	5.5 ± 1.3	+1		
INELASTIC CROSS-SECTION		$p_{T} = 1.7$	GeV x10 ⁻³					6.1 ± 2.2	6.2 ± 1.5	+1	3.7 ± 1.1	3.1 ± 0.8	+1	+1	+1	4.0 ± 0.9	+1	4.6 ± 1.1	4.3 ± 1.1	+1	7.2 ± 1.5	7.2 ± 1.7	1.7 ± 0.9		
INEL		$p_{T} = 1.6$	GeV ×10 ⁻³			11.0 ± 2.6	11.1 ± 2.5	7.1 ± 1.6	12.1 ± 2.0	5.8 ± 1.3	+1	+1	+1	+ 1	+1	+1	7.4 ± 1.5	10.4 ± 2.3	8.3 ± 1.8	8.8 ± 2.2	14.4 ± 2.6	19.6 ± 3.5	0.9 ± 0.7		
		$p_{T} = 1.5$	GeV ×10 ⁻³		22.4 ± 4.0	17.2 ± 3.9	+1	15.7 ± 2.2	+1	16.6 ± 2.6	+1	+1	+1	+1	+1	+1	12.6 ± 2.7	+1	+ 1	16.2 ± 3.2	16.9 ± 3.6	30.9 ± 4.4	2.6 ± 1.2		
		×		0.688	0.705	0.722	0.739	0.756	0.773	0.791	0.:08	0.825	0.842	0.859	0.876	0.893	0.910	0.927	0.944	0.961	0.978	0.995	1.012	1.029	

TABLE X

	4 P _T = 1.5																						14 ± 4	15 ± 4	24 ± 4	34 ± 5	4 + 1	
= 3892 GeV ²	$p_{T} = 1.4$																	17 ± 7	17 ± 5	14 ± 5	10 ± 3	15 ± 3	20 ± 3	29 ± 4	27 ± 3	9 ‡ 89	6 ± 1	
60	$p_{T} = 1.3$															34 ± 8	33 ± 7	29 ± 6	38 ± 6	26 ± 4	27 ± 4	37 ± 4	30 ± 4	42 ± 5	54 ± 6	145 ± 10		
$E d^3 \sigma / d\overline{p}^3$ (mb.GeV ⁻²);	$p_{T} = 1.2$	GeV ×10 ⁻³												86 ± 13	50 ± 9	49 ± 8	2 + 99	68 ± 7	9 + 09	54 ± 5	62 ± 6	9 7 69	9 + 69	85 ± 8	116 ± 10	296 ± 19	18 ± 4	
	p _T = 1.1	GeV ×10 ⁻³										152 ± 18	154 ± 15	142 ± 13	144 ± 11	134 ± 9	111 ± 8	104 ± 8	105 ± 8	106 ± 8	109 ± 8	6 = 001	110 ± 11	141 ± 13	+1	628 ± 42	18 ± 13	
INELASTIC CROSS-SECTION	$p_{T} = 1.0$	GeV ×10 ⁻³						342 ± 47	438 ± 33	339 ± 25	335 ± 21	302 ± 17	+1		+1	+1	229 ± 13	224 ± 13				180 ± 16	265 ± 26	321 ± 54	533 ± 115	1506 ± 200		
INELASTI	$p_{T} = 0.9$	GeV ×10 ⁻³					675 ± 42	673 ± 37	+1			+1			+1		403 ± 22			361 ± 30								
	p _T = 0.3	GeV∕.≎	1.09 ± 0.09	1.11 ± 0.07	1.18 ± 0.07	1.18 ± 0.05	1.02 ± 0.04	1.06 ± 0.05	1.05 ± 0.04	0.91 ± 0.04	0.91 ± 0.04	0.86 ± 0.04	0.86 ± 0.04	0.73 ± 0.04	0.79 ± 0.05	0.71 ± 0.05												
	×		0.625	0.641	0.657	0.673	0.689	0.705	0.721	0.737	0.753	0.769	0.735	0.801	0.818	0.834	0.850	0.866	0.882	0.898	0.914	0.930	0.946	0.962	0.978	0.994	1.010	

·	0.01 ± 0.01	0.10 ± 0.05	1.6 ± 0.3	7.1 ± 0.6	14.6 ± 0.6	14.2 ± 0.6	8.8 ± 0.4	6.1 ± 0.4	5.1 ± 0.3	4.5 ± 0.3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	2.3 ± 0.2	2.3 ± 0.3
$-t = 0.40$ Gev^2		0.4 ± 0.3	1.5 ± 0.4	+1	+1	17.8 ± 0.7	12.5 ± 0.6	8.2 ± 0.5	6.6 ± 0.4	5.7 ± 0.4	+1	+1	4.1 ± 0.3	+1	+1	3.6 ± 0.4	4.0 ± 0.4	3.5 ± 0.3		+1	+1	+1	2.8 ± 0.3	2.7 ± 0.3	2.8 ± 0.4	2.6 ± 0.4
$-t = 0.35$ Gev^2	0.03 ± 0.02	0.4 ± 0.2	3.2 ± 0.3	14.0 ± 0.6	25.8 ± 0.7	23.7 ± 0.7	15.5 ± 0.6	11.0 ± 0.4	8.9 ± 0.4	7.7 ± 0.4	7.7 ± 0.4		+1	+1	+1				4.1 ± 0.3						4.0 ± 0.4	4.1 ± 0.4
$-t = 0.30$ GeV^2	0.07 ± 0.02		5.7 ± 0.3	21.1 ± 0.6	38.1 ± 0.7	29.3 ± 0.6	18.8 ± 0.4	13.1 ± 0.4	11.3 ± 0.4	9.5 ± 0.3	+1	+1	+1	+1	+1	6.2 ± 0.3	6.0 ± 0.3	5.8 ± 0.3	+1	+1	+1	5.2 ± 0.3	4.8 ± 0.2	4.9 ± 0.3	4.9 ± 0.4	4.9 ± 0.4
$-t = 0.25$ Gev^2	0.11 ± 0.02	0.6 ± 0.1	7.5 ± 0.3	34.2 ± 0.8	52.1 ± 0.9	42.7 ± 0.7	26.9 ± 0.6	18.5 ± 0.4	16.3 ± 0.4	13.3 ± 0.4	10.9 ± 0.4	11.1 ± 0.4	9.3 ± 0.4	+1	+1	8.6 ± 0.3	+1	+1		+1	+1	7.0 ± 0.3	6.9 ± 0.3	7.1 ± 0.3	6.5 ± 0.4	6.5 ± 0.4
$-t = 0.20$ Gev^2	0.20 ± 0.05			51.3 ± 0.9	79.4 ± 1.0	60.7 ± 0.8	38.0 ± 0.8	26.7 ± 0.6	20.9 ± 0.5	18.2 ± 0.5	15.4 ± 0.4	14.7 ± 0.4	13.0 ± 0.4	12.1 ± 0.4	11.7 ± 0.4		10.3 ± 0.3	9.8 ± 0.3		+1	+1			9.5 ± 0.4	9.4 ± 0.4	8.7 ± 0.4
$-t = 0.15$ Gev^2	0.07 ± 0.04	1.14 ± 0.15	17.4 ± 0.5	86.7 ± 2.0	131.2 ± 2.2	87.8 ± 1.9	50.1 ± 1.3	38.9 ± 1.0	30.5 ± 0.9	25.9 ± 0.8	22.2 ± 0.6	18.3 ± 0.6	17.4 ± 0.6	16.3 ± 0.6	15.9 ± 0.5	14.1 ± 0.5	13.5 ± 0.5	12.9 ± 0.5	13.0 ± 0.5	13.1 ± 0.5	11.6 ± 0.5	12.4 ± 0.4	12.2 ± 0.4	11.6 ± 0.4	13.2 ± 0.5	13.3 ± 0.5
M ² /s	0137	0091	0046	0	.0046	.0091	.0137	.0182	.0226	.0273	.0319	.0364	.0410	.0456	.0501	.0547	.0592	.0638	.0683	.0729	.0775	.0820	.0867	.0912	9560.	.1002
$_{\rm M}^2$ (GeV ²)	-7.5	-5.0	-2.5	0.0	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0	32.5	35.0	. 37.5	40.0	42.5	45.0	47.5	50.0	52.5	55.0
	-t = 0.15 -t = 0.20 -t = 0.35 -t = 0.35 -t = 0.40 -t =	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$										

TABLE XII.

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		INELASTIC	ASTIC CROSS-SECTION S	$\frac{d^2q}{dtdM^2}$	$(mb.GeV^{-2}); s =$. 549 GeV ²	(00)	(continued)
H2		-t = 0.50	-t = 0.55	-t = 0.60	-t = 0.65	-t = 0.70	-t = 0.75	-t = 0.85
(GeV ²)	M^2/s	GeV ²	Gev ²	GeV ²	GeV ²	Gev^2	GeV ²	GeV ²
-7.5	0137		0.03 ± 0.02		0.08 ± 0.06		0.08 ± 0.03	
-5.0	0091	0.2 ± 0.2	0.5 ± 0.1	0.1 ± 0.1	0.3 ± 0.1	0.1 ± 0.1	0.23 ± 0.06	0.07 ± 0.05
-2.5	0046	•	1.6 ± 0.2	0.8 ± 0.1	1.1 ± 0.2		0.79 ± 0.06	0.48 ± 0.07
0.0	0	+1	5.5 ± 0.4	3.6 ± 0.2	3.6 ± 0.3	2.3 ± 0.2	2.06 ± 0.14	
2.5	.0046	11.3 ± 0.4	8.2 ± 0.3	6.9 ± 0.4	4.7 ± 0.2	4.0 ± 0.2	2.82 ± 0.14	
5.0	.0091	+1	7.0 ± 0.3	6.1 ± 0.3	4.0 ± 0.2	3.6 ± 0.2	2.75 ± 0.15	1.72 ± 0.08
7.5	.0137	7.4 ± 0.4	5.5 ± 0.3	3.9 ± 0.3	3.1 ± 0.2	2.4 ± 0.2	2.19 ± 0.15	1.46 ± 0.08
10.0	.0182	+ 1	3.9 ± 0.2	3.0 ± 0.2	2.6 ± 0.2	2.0 ± 0.2	1.63 ± 0.08	1.06 ± 0.07
12.5	.0226	+1	3.1 ± 0.2	2.6 ± 0.2	2.0 ± 0.1	1.8 ± 0.1	1.32 ± 0.08	0.92 ± 0.05
15.0	.0273	+1	2.5 ± 0.2	2.4 ± 0.2	1.6 ± 0.1	1.4 ± 0.1	1.20 ± 0.08	0.81 ± 0.05
17.5	.0319	2.8 ± 0.2	2.4 ± 0.2	1.7 ± 0.2	1.5 ± 0.1	1.2 ± 0.1	1.00 ± 0.08	0.83 ± 0.05
20.0	.0364	; +1	2.3 ± 0.2	1.8 ± 0.2	1.3 ± 0.1	1.1 ± 0.1	1.01 ± 0.08	0.69 ± 0.04
22.5	.0410	+1	2.0 ± 0.1	1.6 ± 0.2	1.3 ± 0.1	1.2 ± 0.1	1.02 ± 0.08	0.69 ± 0.05
25.0	.0456	0+1	1.9 ± 0.1	1.3 ± 0.2	1.2 ± 0.1	1.0 ± 0.1	0.98 ± 0.08	0.62 ± 0.05
27.5	.0501	+1	2.0 ± 0.1	1.6 ± 0.2	1.3 ± 0.1	0.9 ± 0.1	0.80 ± 08.08	0.62 ± 0.04
30.0	.0547	+1	1.7 ± 0.1	1.6 ± 0.2	1.0 ± 0.1	1.1 ± 0.1	0.74 ± 0.06	0.59 ± 0.05
32.5	.0592	+1	1.6 ± 0.1	1.4 ± 0.2	1.0 ± 0.1	1.1 ± 0.1	0.80 ± 0.06	0.58 ± 0.05
35.0	.0638	2.0 ± 0.2	1.8 ± 0.1	1.4 ± 0.1	1.2 ± 0.1	0.9 ± 0.1	0.88 ± 0.07	0.57 ± 0.05
37.5	.0683	1.7 ± 0.2	1.8 ± 0.1	1.1 ± 0.1	1.0 ± 0.1	0.8 ± 0.1	0.82 ± 0.07	0.49 ± 0.04
40.0	.0729	1.8 ± 0.2	1.8 ± 0.1	1.1 ± 0.1	1.0 ± 0.1	0.9 ± 0.1	0.77 ± 0.07	0.57 ± 0.04
42.5	.0775	2.3 ± 0.2	1.6 ± 0.1	1.3 ± 0.1	1.0 ± 0.1	1.0 ± 0.1	0.77 ± 0.07	0.61 ± 0.04
45.0	.0820	1.9 ± 0.2	1.6 ± 0.1	1.3 ± 0.1	1.0 ± 0.1	0.9 ± 0.1	0.69 ± 0.07	0.49 ± 0.04
47.5	.0867	2.2 ± 0.2	1.5 ± 0.1	1.3 ± 0.2	1.2 ± 0.1	0.9 ± 0.1	0.70 ± 0.07	0.54 ± 0.04
50.0	.0912	1.7 ± 0.2	1.5 ± 0.1	1.4 ± 0.2	1.1 ± 0.1	1.0 ± 0.1	0.75 ± 0.07	0.55 ± 0.04
52.5	9560.	1.8 ± 0.2	1.7 ± 0.2	1.4 ± 0.2	1.0 ± 0.1	0.9 ± 0.1	0.80 ± 0.10	0.00 ± 09.0
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TABLE XII

	-t = 0.55	+ 70		ı +	1 +		+1	+1	+1	+1	+ 1	+ (+1	2.4 ± 0.3	+1		+1		+1	+1	+1	+1	+	+1	+1	+1
	$-\mathbf{t} = 0.50$ Gev^2	+ 3	1 +1	1 + 1	++	+1	+1	+ 1	+ 1	+ 1	4.6 ± 0.3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	1.6 ± 0.2	1.8 ± 0.2
25 GeV ²	$-t = 0.45$ Gev^2	+1 90	+1	+1	+1	+1	14.7 ± 0.6	15.4 ± 0.7	10.6 ± 0.5	8.1 ± 0.5	6.6 ± 0.4	+1	+1	3.6 ± 0.3	+1	+1	+1	+1	3.0 ± 0.3	2.9 ± 0.2	2.4 ± 0.2	+1	+1	+1	+1	2.2 ± 0.3
(mb.GeV ⁻²); s = 725 GeV ²	$-t = 0.35$ Gev^2	.05 ± .04	+1	+1	+1	+1	29.7 ± 1.0	25.0 ± 1.0	19.3 ± 0.9	12.4 ‡ 0.7	10.1 ± 0.6	8.7 ± 0.6	+1	6.1 ± 0.4	5.9 ± 0.4	+1	4.2 ± 0.4	4.3 ± 0.4	4.3 ± 0.4	4.2 ± 0.3	4.1 ± 0.4	3.8 ± 0.4	3.5 ± 0.3	3.7 ± 0.3	3.4 ± 0.3	3.9 ± 0.4
$\frac{s}{\pi} \frac{d^2_{\sigma}}{dt dM^2} $ (mb	$-t = 0.30$ Gev^2	.06 ± .03	+1	+1	+1	27.4 ± 1.1	34.0 ± 1.3	31.9 ± 1.3	24.0 ± 1.1	16.7 ± 0.9	13.0 ± 0.8	11.0 ± 0.7	9.4 ± 0.6	8.0 ± 0.8	6.7 ± 0.6	+1	9.0 = 9.9	6.4 ± 0.5	5.9 ± 0.5	5.1 ± 0.5	4.8 ± 0.4	5.2 ± 0.5	4.5 ± 0.4	5.3 ± 0.5	5.0 ± 0.5	5.0 ± 0.5
.NELASTIC CROSS-SECTION	-t = 0.25 GeV ²	.08 ± .13	.53 ± .07	3.7 ± 0.3	17.8 ± 0.6	48.8 ± 1.0	57.4 ± 1.3	43.6 ± 1.2	28.8 ± 1.1	21.0 ± 1.1	15.3 ± 0.9	12.9 ± 0.9	11.2 ± 0.9	9.5 ± 0.7	9.6 ± 0.8	8.2 ± 0.7	8.8 ± 0.7	7.7 ± 0.6	8.1 ± 0.7	7.9 ± 0.7	7.6 ± 0.6	5.8 ± 0.5	5.9 ± 0.5	6.5 ± 0.6	6.0 ± 0.6	6.0 ± 0.6
INELASTIC	$-\mathbf{t} = 0.20$ Gev^2	.28 ± .12	1.4 ± 0.3	7.6 ± 0.6	47.8 ± 1.5	118.2 ± 2.6	104.9 ± 2.6	74.2 ± 2.2	46.0 ± 1.6	34.5 ± 1.4	24.2 ± 1.1	20.7 ± 1.0	19.2 ± 1.0	18.3 ± 1.0	15.5 ± 0.9	13.2 ± 0.9	14.1 ± 0.8	14.2 ± 0.8	11.6 ± 0.8	11.2 ± 0.7	12.6 ± 0.7	9.6 ± 0.7	10.2 ± 0.7	11.9 ± 0.7	9.8 ± 0.7	10.3 ± 0.7
	$-t = 0.15$ Gev^2	.05 ± .04	.49 ± .13	5.0 ± 0.5	50.3 ± 1.8	148.3 ± 3.3	136.3 = 4.0	82.8 ± 4.5	+1 -	36.1 = 3.5	26.1 ± 2.8	23.7 ± 2.9	19.7 ± 2.8	14.8 ± 2.4	15.3 ± 2.5	13.5 ± 2.2	12.3 ± 2.2	12.6 ± 2.4	14.6 ± 2.4	9.5 ± 2.0	10.4 ± 2.1	10.8 ± 2.2	11.9 ± 2.4	11.8 ± 2.4	9.8 ± 2.4	9.9 ± 2.4
	M ² /s	0124	0600-				.0048	.0083	.0117	.0152	.0186	.0221	.0255	.0290	.0324	.0359	.0393	.0428	.0462	.0497	.0531	.0566	0090.	.0634	6990.	.0703
	M ² (GeV ²)	-9.0	-6.5	-4.0	-1.5	1.0	3.5	0.9	8.5	11.0	13.5	16.0	18.5	21.0	23.5	26.0	28.5	31.0	33.5	36.0	38.5	41.0	43.5	46.0	48.5	51.0

			INELA	INELASTIC CROSS-SECTION	ION 8 d20	$(mb.GeV^{-2})$; s = 934 GeV^2	= 934 Gev ²		
H ² (GeV ²)	H2/s	$-t = 0.25$ Gev^2	$-t = 0.30$ Gev^2	$-t = 0.35$ GeV^2	$-t = 0.40$ Gev^2	$-t = 0.45$ Gev^2	$-t = 0.50$ Gev^2	$-t = 0.55$ Gev^2	$-t = 0.60$ Gev^2
-18	0193		200. ± 200.	.002 ± .002					
-14	0150	. 4 + .%	.05 ± .03	.03 ± .02	.03 ± .03	10. ± 10.	.02 ± .02	.01 ± .01	10. ± 10.
-10	0107	.25 ± .17	.19 ± .11	.17 ± .04	.12 ± .05	.07 ± .04	50. ± 60.	.03 ± .02	+1
9	0064	2.1 ± 1.4	2.1 ± 0.4	3.3 ± .2	1.5 ± .2	.84 ± .16	.91 ± .15	.41 ± .12	+1
-2	0021	25.7 ± 2.2	20.5 ± .8	15.5 ± .6	9. ± 0.6	8.0 ± .5	4.8 ± .4	2.54 ± .40	2.52 ± .29
7	.0021	64.7 ± 2.7	50.0 ± .8	32.5 ± .8	25.5 ± .8	22.0 ± .7	12.7 ± .5	9.10 ± .55	+1
9	.0064	65.0 ± 2.7	38.3 ± .8	30.8 ± .8	26.0 ± .8	18.0 ± .6	13.1 ± .6	9.66 ± .44	+1
01	.0107	33.0 ± 2.1	21.5 ± .6	19.2 ± .7	13.5 ± .7	11.2 ± .6	8.0 ± .4	6.18 ± .36	6.14 ± .33
14	.0150	19.5 ± 1.6	13.1 ± .6	12.2 + .6	9.2 ± .5	4. ± 6.9	5.6 ± .4	4.13 ± .30	3.76 ± .27
18	.0193	18.8 ± 1.6	12.8 ± .5	9.5 ± .5	7.2 ± .5	5.0 ± .3	4.3 ± .3	3.34 ± .26	3.21 ± .24
22	.0236	16.4 ± 1.4	10.1 ± .5	8.1 ± .5	5.5 ± .4	4.9 ± .3	3.8 ± .3	2.68 ± .23	2.96 ± .22
26	.0279	13.4 ± 1.3	8.1 ± .4	6.7 ± .5	5.0 ± .4	4.7 ± .3	3.7 ± .3	2.49 ± .20	2.22 ± .21
30	.0321	12.0 ± 1.3	7.7 ± .4	6.1 ± .4	4.9 ± .4	3.9 ± .3	2.6 ± .3	2.37 ± .20	1.79 ± .19
34	.0364	11.6 ± 1.2	7.3 ± .4	6.0 ± .4	4.2 ± .4	3.6 ± .2	2.5 ± .3	2.18 ± .20	1.74 ± .19
38	.0407	10.2 ± 1.2	6.9 ± .4	5.8 ± .4	4.5 ± .4	3.3 ± .2	3.0 ± .3	1.80 ± .16	1.81 ± .18
42	.0450	9.4 ± 1.1	6.8 ± .4	4. 5 ± .4	4.6 ± .4	3.2 ± .2	2.6 ± .3	1.76 ± .17	1.71 ± .18
46	.0493	9.1 ± 1.1	6.6 ± .4	4.8 ± .3	3.5 ± .4	3.1 ± .2	2.3 ± .3	1.80 ± .17	1.47 ± .18
20	.0536	7.2 ± 1.0	5.4 ± .3	4.9 ± .3	3.2 ± .3	2.6 ± .2 ·	2.4 ± .3	1.76 ± .16	1.36 ± .19
54	.0578	7.4 ± 1.0	6.4 ± .4	4.4 ± .3	3.2 ± .3	2.8 ± .2	1.9 ± .3	1.73 ± .16	1.34 ± .19
58	.0621	7.5 ± 1.0	5.7 ± .3	4.4 ± .3	3.7 ± .2	2.8 ± .3	2.0 ± .2	1.73 ± .16	1.39 ± .19
62	.0664	7.8 ± 1.0	5.0 ± .3	4.1 ± .3	3.1 ± .2	2.7 ± .3	2.2 ± .2	1.60 ± .17	1.40 ± .19
99	.0707	6.9 ± 1.0	4.5 ± .3	4.1 ± .3	3.0 ± .2	2.6 ± .3	2.1 ± .2	1.56 ± .16	1.45 ± .19
20	.0750	5.3 ± .9	4.9 ± .3	4.0 ± .3	3.1 ± .2	2.3 ± .2	1.9 ± .2	1.35 ± .16	1.53 ± .18
74	.0793	6. ± 9.9	5.1 ± .3	4.2 ± .3	3.2 ± .2	2.5 ± .2	1.9 ± .2	1.44 ± .16	1.22 ± .18
78	.0836	6.5 ± 1.0	4.5 ± .3	4.2 ± .3	3.1 ± .2	2.3 ± .3	2.3 ± .2	1.57 ± .17	1.03 ± .16
82	.0878	7.3 ± 1.0	4.5 + .3	4.0 ± .3	3.0 ± .2	2.3 ± .2	2.1 ± .2	1.42 ± .18	1.20 ± .15
98	.0921	7.8 ± 1.0	5.1 ± .3	4.2 ± .3	3.2 ± .2	2.4 ± 43	1.9 ± .2	.1.40 ± .18	1.30 ± .14
8	.0964	5.8 ± 0.9	4.7 ± .3	4.3 ± .3	3.4 ± .2	2.1 ± .3	2.0 ± .2	1.52 ± .19	1.06 ± .14
94	.1007	6.5 ± 1.4	4.7 ± .4	3.7 ± .6	2.9 ± .3	2.1 ± .4	1.9 ± .3	1.21 ± .28	.94 ± .20
				,					

GeV ² (continued)	-t = 2.00	GeV ²			100. ± 100.	900· + 900·	+1	.039 ± .008	.038 ± .008	.042 ± .007	.036 ± .007	.031 ± .006	.026 ± .006	.023 ± .006	.026 ± .006	.020 ± .006	.025 ± .006	.032 ± .006	.027 ± .006	.024 ± .005	.020 ± .005	.021 ± .004	.015 ± .004	.012 ± .004	.017 ± .005	.015 ± .005	.018 ± .005	.031 ± .005	.030 ± .005	.022 ± .005	.019 ± .004
$(mb.GeV^{-2})_{; s} = 934 GeV^{2}$	-t = 1.60	Gev ²		.006 ± .002	.005 ± .002	.027 ± .004	700. ± 620.	.154 ± .010	010. ± 691.	.126 ± .009	800° - 760°	111 ± .008	700. ± 060.	700. ± 920.	• 000 ÷ 000	900. ± 690.	.071 ± .006	.062 ± .006	.055 ± .005	.053 ± .005	900° - 090°	.054 ± .005	.053 ± .005	900. ± 890.	.064 ± .006	.053 ± .005	.054 ± .005	.053 ± .005	900. ± 890.	500. ± 850.	800. ± 290.
* d2g	-t = 1.45	GeV^2		.004 ± .004	.011 ± .005	.043 ± .008	.128 ± .018	.225 ± .020	.236 ± .019	.191 ± .017	.147 ± .016	.132 ± .015	.132 ± .014	.120 ± .013	.106 ± .012	.093 ± .012	.087 ± .012	.099 ± .011	.092 ± .011	.080 ± .011	.073 ± .011	.089 ± .011	.097 ± .011	.089 ± .011	.096 ± .011	.092 ± .010	.080 ± .010	.085 ± .010	.088 ± .010	.079 ± .010	.083 ± .013
INELASTIC CROSS-SECTION	-t = 1.25	GeV ²		.003 ± .003	.015 ± .006	.065 ± .012	.249 ± .037	.450 ± .039	.396 ± .036	.328 ± .033	.272 ± .030	.222 ± .026	.166 ± .024	.168 ± .023	.157 ± .023	.150 ± .022	.154 ± .023	.159 ± .022	.154 ± .021	.135 ± .021	.136 ± .020	130 ± 181.	.158 ± .021	137 ± .019	113 ± .019	.120 ± .021	.133 ± .022	.159 ± .020	.133 ± .018	.112 ± .018	.134 ± .020
INELA	-t = 0.95	GeV ²		.00 ± .01	.03 ± .02	.10 ± .05	.42 ± .13	1.00 ± .17	1.38 ± .18	1.33 ± .17	.77 ± .15	.74 ± .13	.63 ± .14	.42 ± .11	.62 ± .13	.56 ± .12	.50 ± .11	.29 ± .10	.20 ± .08	.32 ± .10	.25 ± .09	.30 ± .10	.40 ± .10	.41 ± .10	.27 ± .10	.33 ± .10	.42 ± .12	.41 ± .14	.33 ± .15	.22 ± .16	.22 ± .26
	,	M ² /s	0193	0150	0107	0064	0021	.0021	1900	.0107	.0150	.0193	.0236	.0279	.0321	.0364	.0407	.0450	.0493	.0536	.0578	.0621	.0664	.0707	.0750	.0793	.0836	.0878	.0921	.0964	.1007
	¥2,	(Gev ²)	-18	-14		9	77	7	•	10	14	18	22	58	30	34	38	42	94	20	54	28	62	99	20	7.	78	82	98	%	94

TABLE XIV

TABLE XV

	_+ = 0.35	GeV^2	.03 ± .06	.09 ± .10	1.6 ± 0.5	13.5 ± 1.5	44.4 ± 3.5	29.0 ± 2.2	19.4 ± 1.8	12.0 ± 1.3	8.9 ± 1.1	5.3 ± 0.8	8.6 ± 1.3	4.8 ± 0.9	5.9 ± 1.0	4.1 ± 0.8	5.3 ± 0.9	3.2 ± 0.7	5.3 ± 0.9	3.5 ± 0.9	4.0 ± 0.8	3.6 ± 0.8	5.1 ± 1.1	5.1 ± 1.1	3.4 ± 0.9	2.3 ± 0.7	3.5 ± 0.7	5.2 ± 1.0	3.1 ± 0.9	2.9 ± 0.8
$s = 1047 \text{ GeV}^2$	-+ = 0.30	GeV^2	.04 ± .06	.38 ± .18	2.8 ± 0.5	23.2 ± 2.0	51.6 ± 3.3	36.7 ± 2.2	20.8 ± 1.4	15.0 ± 1.3	11.6 ± 1.1	9.4 ± 0.9	9.7 ± 1.0	8.7 ± 0.9	6.7 ± 0.8	7.3 ± 0.9	7.4 ± 1.0	8.0 = 9.9	4.3 ± 0.7	4.7 ± 0.7	5.1 ± 0.8	5.0 ± 0.7	5.0 ± 0.8	4.9 ± 0.8	5.1 ± 0.8	5.6 ± 0.8	4.7 ± 0.7	4.3 ± 0.7	4.0 ± 0.7	3.6 ± 0.6
$\frac{d^2_{\sigma}}{d^4d^{M^2}} (mb.GeV^{-2})_{;}$		Gev ²	90. ± 90.	.30 ± .14	3.6 ± 0.6	30.2 ± 2.6	67.8 ± 4.4	50.5 ± 2.7	34.6 ± 1.9	18.3 ± 1.2	16.4 ± 1.2	11.2 ± 0.9	10.9 ± 0.9	12.4 ± 1.0	8.0 ± 6.8	7.0 ± 0.8	7.9 ± 0.8	8.2 ± 0.8	9.2 ± 0.9	8.3 + 0.8	7.5 ± 0.8	6.5 ± 0.7	7.2 ± 0.8	8.1 ± 0.9	8.0 ± 9.9	6.3 ± 0.8	5.5 ± 0.7	7.0 ± 0.8	6.1 ± 0.7	5.5 ± 0.7
• =	-t = 0.20	Gev^2	.08 ±.03	.28 ± .15	3.9 ± .7	39.0 ± 3.6	87.3 ± 5.9	69.9 ± 3.7	37.8 ± 2.2	21.7 ± 1.5	21.5 ± 1.5	16.4 ± 1.1	12.6 ± 1.0	13.1 ± 1.0	11.2 ± 0.9	14.2 ± 1.1	6.0 = 6.6	7.6 ± 0.7	8.8 ± 0.7	8.3 ± 0.7	7.9 ± 0.7	9.7 ± 0.8	8.0 ± 0.7	8.7 ± 0.9	8.0 ± 2.9	7.6 ± 0.9	7.3 ± 0.9	6.7 ± 0.8	8.0 ± 0.9	6.6 ± 0.8
INELASTIC CROSS-SECTION	M ² /s		0173	0126	0078	0030	.0018	.0065	.0113	.0161	.0209	.0256	.0304	.0352	.0400	.0447	.0495	.0543	.0591	.0639	9890.	.0734	.0782	.0830	.0877	.0925	.0973	.1021	.1068	.1116
INE	₹2	(GeV) ²	-18.2	-13.2	-8.2	-3.2	1.8	8.8	11.8	16.8	21.8	26.8	31.8	36.8	41.8	46.8	51.8	56.8	61.8	8.99	71.8	76.8	81.8	8.98	91.8	8.96	101.8	106.8	111.8	116.8

	$-t = 0.35$ G_{ev}^2	A = 0	-1 +	.2910	1.6 ± 0.3	8.0 + 0.5	25.5 ± 1.1	33.7 ± 1.0	33.7 ± 1.0	23.5 ± 0.9	16.9 ± 0.9	12.0 ± 0.6	10.4 ± 0.5	7.4 ± 0.6	+1	6.7 ± 0.4	6.0 ± 0.5	5.6 ± 0.4	5.3 ± 0.4	5.9 ± 0.4	4.7 ± 0.4	4.7 ± 0.4	4.0 ± 0.3	4.2 ± 0.4	4.2 ± 0.4	4.4 ± 0.4	3.1 ± 0.3	3.8 ± 0.3	3.6 ± 0.4	4.3 ± 0.4
= 1239 GeV ²	-t = 0.30	4	- 1 -	.36 ± .16	2.5 - 0.5	13.5 ± 1.0	37.3 ± 1.9	51.5 ± 2.1	42.9 ± 2.1	29.6 ± 1.6	20.4 ± 1.2	14.9 ± 1.2	13.3 ± 1.0	11.2 ± 0.9	8.0 ± 0.8	8.6 ± 0.8	8.8 ± 0.8	7.0 ± 0.8	6.7 ± 0.7	5.1 ± 0.7	6.3 ± 0.7	6.8 ± 0.7	5.2 ± 0.7	6.0 ± 0.7	9.0 = 0.9	5.3 ± 0.6	5.6 ± 0.8	6.4 ± 0.8	5.6 ± 0.6	4.8 ± 0.6
(mb.GeV ⁻²); s	-t = 0.25	4 70	-1 +	.9122	3.6 ± 0.5	15.2 ± 0.9	55.1 ± 1.8	76.5 ± 2.2	59.8 ± 1.9	39.4 ± 1.4	27.3 ± 1.0	22.3 ± 1.3	17.2 ± 0.8	13.9 ± 0.8	12.9 ± 0.8	12.1 ± 0.8	6.5 ± 0.7	10.4 ± 0.8	10.0 ± 0.7	8.4 ± 0.7	8.3 ± 0.7	7.8 ± 0.7	8.3 ± 0.7	6.7 ± 0.7	6.6 ± 0.7	7.2 ± 0.6	7.2 ± 0.6	6.4 ± 0.6	6.5 ± 0.5	6.5 ± 0.5
CCTION s do	$-\mathbf{t} = 0.20$ $C_{20}V^{2}$	+	-1 +	-1 -	2.9 ± 0.7	15.4 ± 1.8	64.7 ± 3.3	93.3 ± 4.0	97.5 ± 3.7	57.7 ± 2.8	41.4 ± 2.3	36.6 ± 2.3	29.8 ± 2.0	23.1 ± 1.8	16.6 ± 1.5	17.8 ± 1.6	16.0 ± 1.6	14.9 ± 1.5	16.8 ± 1.6	11.5 ± 1.3	14.9 ± 1.5	11.9 ± 1.4	15.1 ± 1.5	12.6 ± 1.5	11.8 ± 1.4	12.9 ± 1.5	12.3 ± 1.4	12.6 ± 1.6	10.6 ± 1.3	11.9 ± 1.5
INELASTIC CROSS_SECTION	M ² / _e	0/ =	0137	0105	0073	0040	0008	+.0024	.0057	6800.	.0121	.0153	9810.	.0218	.0250	.0283	.0315	.0348	.0379	.0412	.0444	.0476	.0509	.0541	.0573	.0605	.0638	0/90.	.0702	.0735
INELAST	M ² (GaV ²)	(Aao)	-1-	-13	٥	-5	-1	က	7	11	15	19	23	27	31	35	39	43	47	51	55	59	63	29	71	75	79	83	87	91

TABLE XVI

(continued)	$-t = 0.75$ $6ev^2$.15 ± .08	.07 ± .03	.22 ± .07	.77 ± .13	2.1 ± 0.2	3.1 ± 0.3	3.5 ± 0.3	3.1 ± 0.3	2.6 ± 0.2	1.2 ± 0.2	1.5 ± 0.2	1.2 ± 0.2	1.0 ± 0.2	0.9 ± 0.1	0.8 ± 0.2	0.8 ± 0.1	0.8 ± 0.1	0.6 ± 0.1	0.7 ± 0.1	0.8 ± 0.1	0.7 ± 0.1	0.6 ± 0.1	0.5 ± 0.1	0.7 ± 0.1	0.9 ± 0.1	0.7 ± 0.1	0.6 ± 0.1	0.5 ± 0.1
Gev ²	$-t = 0.65$ GeV^{2}	70. ± 70.	.14 ± .07	.44 ± .05	1.4 ± 0.2	3.2 ± 0.2	6.2 ± 0.2	6.6 ± 0.2	4.5 ± 0.2	3.1 ± 0.1	2.9 ± 0.1	2.3 ± 0.1	1.7 ± 0.1	1.7 ± 0.1	1.6 ± 0.1	1.2 ± 0.1	1.3 ± 0.1	1.3 ± 0.1	1.1 ± 0.1	0.8 ± 0.1	1.0 ± 0.1	1.1 ± 0.1	1.0 ± 0.1	0.9 ± 0.1	1.0 ± 0.1	0.9 ± 0.1	0.9 ± 0.1	0.9 ± 0.1	1.0 ± 0.1
$(mb.GeV^{-2})$; s = 1239 GeV^{2}	$-t = 0.55$ Gev^2	50. ± 50.	.17 ± .05	.74 ± .12	2.4 ± 0.2	6.8 ± 0.3	9.4 ± 0.3	11.3 ± 0.3	8.4 ± 0.3	6.1 ± 0.2	3.7 ± 0.2	3.4 ± 0.2	3.4 ± 0.2	3.1 ± 0.2	2.6 ± 0.2	2.4 ± 0.1	1.8 ± 0.1	1.9 ± 0.1	1.7 ± 0.1	1.6 ± 0.1	1.7 ± 0.1	1.6 ± 0.1	1.6 ± 0.1	1.6 ± 0.1	1.3 ± 0.1	1.3 ± 0.1	1.6 ± 0.1	1.4 ± 0.1	1.4 ± 0.1
$\frac{s}{\pi} \frac{d^2\sigma}{dtdM^2}$ (mb.0	$-t = 0.50$ GeV^2	.10 ± .05	.19 ± .06	.75 ± .05	2.9 ± 0.1	8.9 ± 0.3	14.3 ± 0.5	14.0 ± 0.5	10.2 ± 0.4	8.9 ± 0.4	6.2 ± 0.4	4.6 ± 0.3	3.8 ± 0.3	3.7 ± 0.3	3.3 ± 0.2	3.0 ± 0.2	2.7 ± 0.2	2.6 ± 0.2	2.3 ± 0.2	2.5 ± 0.2		2.2 ± 0.2	2.2 ± 0.2	2.2 ± 0.2	1.7 ± 0.2	2.0 ± 0.2	1.8 ± 0.2	1.8 ± 0.2	1.5 ± 0.1
INELASTIC CROSS-SECTION	$-t = 0.45$ GeV^2	50. ± 70.	.32 ± .05	1.3 ± 0.2	5.1 ± 0.4	12.9 ± 0.5	18.4 ± 0.6	17.1 ± 0.7	13.6 ± 0.6	9.5 ± 0.4	7.6 ± 0.4	5.4 ± 0.4	4.9 ± 0.4	4.9 ± 0.3	4.2 ± 0.3	3.6 ± 0.3	2.9 ± 0.2	3.1 ± 0.2	2.9 ± 0.2	3.0 ± 0.2	2.4 ± 0.2	2.8 ± 0.2	2.4 ± 0.2	2.6 ± 0.2	2.6 ± 0.2	2.3 ± 0.2	2.2 ± 0.2	2.4 ± 0.2	2.1 ± 0.2
INELASTI	M ² /s	0137	0105	0073	0040	0008	+.0024	.0057	.0089	.0121	.0153	.0186	.0218	.0250	.0283	.0315	.0348	.0379	.0412	.0444	.0476	.0509	.0541	.0573	5090.	.0638	0/90.	.0702	.0735
	${\rm M}^2$ (GeV ²)	-17	-13	6-	-5	7	က	7	11	15	19	23	27	31	35	39	43	47	51	55	26	63	29	71	75	23	83	87	91

INELASTIC CROSS-SECTION $\frac{s}{\pi} \frac{d^2\sigma}{dtdM^2}$ (mb.GeV⁻²); s = 1464 (GeV²)

ſ -	T																										
$-t = 0.45$ Gev^2	.19 ± .04	.94 ± .09	+1	12.0 ± 0.8	18.9 ± 0.8	+1	+1	+1	7.6 ± 0.6	6.1 ± 0.6	5.1 ± 0.4	4.5 ± 0.3	4.6 ± 0.4	4.2 ± 0.3	2.7 ± 0.3	3.2 ± 0.3	2.9 ± 0.3	2.9 ± 0.3	2.6 ± 0.3	2.7 ± 0.4	2.8 ± 0.4	2.5 ± 0.3	3.3 ± 0.4	2.6 ± 0.3	2.1 ± 0.3	2.3 ± 0.3	1.8 ± 0.3
$-t = 0.35$ Gev^2	.22 ± .17	1.3 ± 0.1	6.2 ± 0.4	+1	33.6 ± 1.6	35.4 ± 1.5	25.1 ± 1.3	16.3 ± 1.2	12.1 ± 0.8	9.8 ± 0.8	10.1 ± 0.7	6.8 ± 0.7	7.4 ± 0.7	6.9 ± 0.7	5.5 ± 0.6	4.7 ± 0.5	5.4 ± 0.6	4.7 ± 0.5	5.1 ± 0.5	4.0 ± 0.5	4.3 ± 0.5	4.1 ± 0.6	4.4 ± 0.5	3.8 ± 0.4	3.9 ± 0.4	4.4 ± 0.4	4.5 ± 0.5
$-t = 0.30$ Gev^2	.32 ± .18	2.0 ± 0.4	8.7 ± 1.0	29.1 ± 1.2	47.4 ± 1.5	42.6 ± 1.2	40.0 ± 1.5	21.5 ± 1.0	18.1 ± 0.9	11.2 ± 0.7	13.0 ± 0.7	7.9 ± 0.5	8.1 ± 0.6	6.2 ± 0.5	8.1 ± 0.6	9.2 ± 0.6	6.6 ± 0.5	6.8 ± 0.4	6.4 ± 0.5	5.8 ± 0.4	4.9 ± 0.4	4.0 ± 0.5	6.3 ± 0.5	6.0 ± 0.4	5.5 ± 0.4	4.6 ± 0.4	4.3 ± 0.4
$-t = 0.25$ Gev^2	.60 ± .20	+1	13.3 ± 0.4	+1	72.1 ± 1.4	60.0 ± 1.6	41.2 ± 1.4	23.9 ± 1.1	19.9 ± 1.1	16.0 ± 0.8	15.0 ± 0.8	12.7 ± 0.7	10.7 ± 0.7	10.7 ± 0.7	10.2 ± 0.7	9.8 ± 0.7	9.5 ± 0.6	8.3 ± 0.7	8.3 ± 0.5	7.8 ± 0.5	7.7 ± 0.5	8.0 ± 0.5	7.4 ± 0.5	7.1 ± 0.5	+1	+1	6.5 ± 0.5
$-t = 0.20$ Gev^2	.90 ± .29	2.7 ± 0.2	15.2 ± 0.6	56.4 ± 1.0	+1	80.7 ± 1.9	52.5 ± 1.7	32.3 ± 1.7	27.8 ± 1.4	22.5 ± 1.1	18.2 ± 1.1	16.0 ± 1.1	15.0 ± 0.9	14.6 ± 0.9	13.2 ± 0.8	13.2 ± 0.9	12.3 ± 0.8	13.8 ± 0.7	10.9 ± 0.7	12.5 ± 1.0	9.5 ± 0.6	11.3 ± 0.7	8.9 ± 0.7	10.6 ± 0.6	8.7 ± 0.9	9.4 ± 0.8	9.9 ± 0.7
M ² /s	0113	0079	0044	0010	+.0024	.0058	2600.	.0126	.0160	.0195	.0229	.0263	.0297	.0331	.0365	.0400	.0434	.0468	.0502	.0536	.0570	.0604	.0639	.0673	.0707	.0741	.0775
$\rm M^2$ $(\rm GeV^2)$	-16.5	-11.5	-6.5	-1.5	3.5	8.5	13.5	18.5	23.5	28.5	33.5	38.5	43.5	48.5	53.5	58.5	63.5	68.5	73.5	78.5	83.5	88.5	93.5	98.5	103.5	108.5	113.5

TABLE XVII

INELASTIC CROSS-SECTION $\frac{s}{\pi} \frac{d^2\sigma}{dtdM^2}$ (mb.GeV⁻²); $s = 1464(\text{GeV}^2)$

(continued)

$-t = 0.50$ $-t = 0.55$ Gev^2
.34 ± .13
1.1 ± 0.2
.4 ± 0.4
8.8 ± 0.7
13.7 ± 0.6
9.0 = 2.1
9.6 ± 0.5
+1
5.1 ± 0.5
3.7 ± 0.3
.3 ± 0.3
7 ± 0.4
.3 ± 0.4
.3 ± 0.3
3.0 ± 0.3
5 ± 0.3
.7 ± 0.3
.4 ± 0.3
2 ± 0.2
9 ± 0.2
2.4 ± 0.3
9 ± 0.3
9 ± 0.3
2 ± 0.3
.2 ± 0.3
.0 + 0.
.1 ± 0.0

TABLE XVII

		NI	ELASTIC CROSS-S	ECTION # d ² /e	INELASTIC CROSS-SECTION $\frac{s}{\pi} d^2 \sigma/dt dM^2 \text{ (mb.GeV}^{-2});$	$3 = 1995 \text{GeV}^2$			
1	μ ² (Gev ²)	M ² /s	-t = 0.45 GeV ²	-t = 0.55 GeV ²	-t = 0.65 GeV ²	-t = 0.75 GeV ²	-t = 0.85 GeV ²	-t = 0.95 GeV ²	
	-27.3	0137				0.02 ± 0.02		0.01 ± 0.02	
	-17.3	0087			0.1 ± 0.1	0.07 ± 0.04		0	
	- 7.3	0037			2.0 ± 0.4	1.60 ± 0.25	0.79 ± 0.17	0.46 ± 0.10	
	2.7	.0014			12.3 ± 1.1	7.06 ± 0.56	4.08 ± 0.39	2.46 ± 0.23	
	12.7	.0064		8.3 ± 0.8	6.6 ± 0.7	3.42 ± 0.34	3.31 ± 0.36	+1	
	22.7	.0114		5.2 ± 0.6	3.6 ± 0.6	3.03 ± 0.34	1.32 ± 0.18	1.10 ± 0.15	
	32.7	.0164		4.4 ± 0.6	3.2 ± 0.6	1.61 ± 0.23	0.78 ± 0.12	0.59 ± 0.11	
	42.7	.0214		4.3 ± 0.6	1.7 ± 0.4	1.28 ± 0.20	0.69 ± 0.12	0.71 ± 0.14	
	52.7	.0264		2.2 ± 0.4	1.2 ± 0.3	0.92 ± 0.17	0.61 ± 0.11	0.77 ± 0.15	
	62.7	.0314		3.1 ± 0.5	1.4 ± 0.2	0.72 ± 0.14	0.79 ± 0.14	0.31 ± 0.09	
	72.7	.0364		2.8 ± 0.5	1.1 ± 0.2	0.91 ± 0.17	0.62 ± 0.11	0.47 ± 0.11	
	82.7	.0415		1.5 ± 0.3	1.4 ± 0.2	0.75 ± 0.16	0.71 ± 0.13	0.32 ± 0.08	
	92.7	.0465	,	1.4 ± 0.3	1.1 ± 0.2	0.87 ± 0.17	0.46 ± 0.10	+1	
	102.7	.0515	1.7 ± 0.4	1.7 ± 0.4	1.3 ± 0.2	0.93 ± 0.18	0.53 ± 0.10	0.44 ± 0.09	
	112.7	.0565	2.5 ± 0.5	1.5 ± 0.4	1.1 ± 0.2	0.55 ± 0.11	0.59 ± 0.12	0.20 ± 0.06	
	122.7	.0615		2.5 ± 0.5	0.8 ± 0.2	0.56 ± 0.11	0.49 ± 0.11	0.32 ± 0.07	
	132.7	.0665	1.9 ± 0.4	2.1 ± 0.4		0.75 ± 0.12	0.35 ± 0.10	0.32 ± 0.08	
	142.7	.0715	2.2 ± 0.4	1.9 ± 0.4	1.3 ± 0.2	0.60 ± 0.11	0.44 ± 0.12	0.30 ± 0.07	
	152.7	.0765	2.1 ± 0.4	1.3 ± 0.2	1.0 ± 0.2	0.49 ± 0.10	0.60 ± 0.12	0.28 ± 0.07	
	162.7	.0815	2.1 ± 0.5	1.9 ± 0.3	1.0 ± 0.2	0.66 ± 0.11	0.42 ± 0.11	0.30 ± 0.07	
	172.7	9980.	1.9 ± 0.4	1.0 ± 0.2	1.3 ± 0.2	0.81 ± 0.13	0.50 ± 0.12	0.22 ± 0.06	
	182.7	.0916	2.7 ± 0.5	2.1 ± 0.3	1.0 ± 0.2	0.73 ± 0.13	0.44 ± 0.11	0.35 ± C.08	
	192.7	9960.	1.6 ± 0.3	1.4 ± 0.2	1.0 ± 0.2	0.70 ± 0.12	0.51 ± 0.12	0.48 ± 0.10	
	202.7	.1016	2.2 ± 0.5	1.8 ± 0.2	0.8 ± 0.2	0.79 ± 0.13	0.57 ± 0.10	0.24 ± 0.06	
	212.7	.1066	2.5 ± 0.4	1.5 ± 0.2	1.0 ± 0.2	0.79 ± 0.13	0.56 ± 0.11	0.33 ± 0.08	
	222.7	.1116	2.7 ± 0.5	1.6 ± 0.2	0.9 ± 0.2	0.75 ± 0.13	0.39 ± 0.08	0.35 ± 0.08	
	232.7	.1166	2.3 ± 0.4	1.7 ± 0.2	1.0 ± 0.2	0.62 ± 0.12	0.40 ± 0.08	0.41 ± 0.09	
									┑

TABLE XVIII

<u> </u>	×10_2		10	11	_																						
			30 +	47 ± 1	41 ± 11	53 ± 14	17 ± 7	36 ± 10	8 + 5	14 ± 6	19 ± 7	+1	19 ± 7	23 ± 7	20 ± 6	18 ± 6	21 ± 7	10 ± 4	3 + 3	9 + 5	18 ± 6	18 ± 6	11 ± 5	24 + 8	19 ± 7	10 ± 5	26 ± 7
$-t = 1.75$ Gev^2	×10_2	4 + 4	61 ± 15	138 ± 22	96 ± 18	65 ± 14	66 ± 15	56 ± 13	83 ± 21	31 ± 10	57 ± 14	40 ± 12	30 ± 10	41 ± 11	44 ± 11	49 ± 11	52 ± 14	+1	30 ± 9	44 ± 11	26 ± 8	35 ± 10	58 ± 12	44 ± 12	33 ± 9	44 ± 12	29 ± 9
$-t = 1.45$ Gev^2	×10_2		87 ± 21	328 ± 41	351 ± 44	224 ± 33	150 ± 30	84 ± 21	118 ± 27	75 ± 20	79 ± 22	75 ± 20	91 ± 25	145 ± 31	118 ± 28	111 ± 26	55 ± 19	+1	+1	69 ‡ 19	+1	+1	88 ± 21	75 ± 19	134 ± 29	112 ± 25	97 ± 21
$-t = 1.25$ Gev^2			0.25 ± 0.06	0.74 ± 0.14	0.74 ± 0.15	0.32 ± 0.07	0.36 ± 0.08	0.26 ± 0.06	0.16 ± 0.05	0.29 ± 0.07	0.19 ± 0.07	0.05 ± 0.03	0.16 ± 0.06	0.09 ± 0.04	0.02 ± 0.02	0.18 ± 0.06	0.12 ± 0.05	0.15 ± 0.07	0.13 ± 0.05	0.06 ± 0.04	0.20 ± 0.06	0.09 ± 0.04	0.10 ± 0.05	0.02 ± 0.02	0.13 ± 0.05	0.15 ± 0.06	0.17 ± 0.06
$-t = 1.15$ Gev^2	i .	0.02 ± 0.02	0.13 ± 0.04	1.09 ± 0.14	1.03 ± 0.14	0.74 ± 0.13	0.23 ± 0.07	0.31 ± 0.08	0.26 ± 0.07	0.29 ± 0.09	0.23 ± 0.08	0.13 ± 0.05	0.31 ± 0.10	0.26 ± 0.09	0.17 ± 0.05	0.22 ± 0.06	0.18 ± 0.05	0.16 ± 0.05	0.22 ± 0.06	0.17 ± 0.05	0.16 ± 0.06	0.14 ± 0.05	0.11 ± 0.04	0.17 ± 0.05	0.18 ± 0.05	0.31 ± 0.07	0.21 ± 0.06
$-t = 1.05$ Gev^2		0.02 ± 0.02	0.48 ± 0.10	1.24 ± 0.15	1.12 ± 0.16	0.62 ± 0.11	0.41 ± 0.08	0.27 ± 0.07	0.41 ± 0.09	0.29 ± 0.07	0.31 ± 0.08	0.35 ± 0.08				0.38 ± 0.09	0.15 ± 0.05			0.17 ± 0.07	0.13 ± 0.05	0.34 ± 0.10	0.13 ± 0.06	0.46 ± 0.10			0.12 ± 0.04
M ² /s	0137	0087	0037	.0014	.0064	.0114	.0164	.0214	.0264	.0314	.0364	.0415	.0465	.0515	.0565	.0615	.0665	.0715	.0765	.0815	9980.	.0916	9960.	.1016	1066	.1116	.1166
M ² (GeV ²)	-27.3	-17.3	- 7.3	2.7	12.7	22.7	32.7	42.7	52.7	62.7	72.7	82.7	92.7	102.7	112.7	122.7	132.7	142.7	152.7	162.7	172.7	182.7	192.7	202.7	212.7	222.7	232.7
	-t = 1.05 $-t = 1.15$ $-t = 1.25$ $-t = 1.45$ $-t =$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

TABLE XVIII

$d^2\sigma/dtdM^2$ (mb.GeV ⁻²); s = 2783 GeV ²	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 ± 2 10 ± 10	73 ± 53 5	±3 27 ±	15 ± 4 23 ± 17 8 ± 4	18 ± 5 82 ± 26 13 ± 5	10 ± 3 75 ± 25 10 ± 4	23 ± 5 68 ± 28 21 ± 6	7 ± 3 5 ± 5 11 ± 4	11 ± 4 64 ± 26 7 ± 3	9 ± 3 26 ± 15 15 ± 5	7 ± 3 67 ± 24 9 ± 4		5 ± 3 53 ± 21 11 ± 4	12 ± 4 30 ± 15 9 ± 3	13 ± 4 41 ± 23 11 ± 4	4 ± 2 8 ± 8 18 ± 5	11 ± 4 70 ± 24 13 ± 5	4 ± 2 43 ± 21 13 ± 5	11 ± 4 53 ± 24 29 ± 8	7 ± 3 38 ± 17 22 ± 6	8 ± 3 43 ± 22 15 ± 5	12 ± 4 11 ± 11 17 ± 5	11 ± 4 56 ± 26 23 ± 6	6 ± 3 54 ± 24 10 ± 4	17 ± 5 128 ± 33 12 ± 5	9 ± 4 70 ± 28 14 ± 5	12 ± 5 41 ± 20 10 ± 4
o ⊨	$-t = 2.35$ $6ev^2$ $\times 10^{-3}$	3 ± 2	+1 -		+1	30 ± 7	12 ± 5	15 ± 5	18 ± 6	11 ± 4	14 ± 5	13 ± 5	17 ± 6	4 + 3	9 + 4	7 ± 3	10 ± 4	15 ± 4	15 ± 5	14 ± 5	11 ± 4	10 ± 3	6 + 3	12 ± 4	21 ± 5	14 ± 4	13 ± 4	24 ± 6
INELASTIC CROSS-SECTION	$-t = 2.05$ Gev^2 $\times 10^{-3}$	-	+1 +	++ +	+1	+1	+1	47 ± 11	24 ± 7	28 ± 8	24 ± 7	26 ± 7	16 ± 6	15 ± 5	13 ± 5	24 ± 7	13 ± 5	23 ± 6	22 ± 6	25 ± 8	21 ± 7	16 ± 6	19 ± 6	20 ± 6	28 ± 8	38 + 8	19 ± 6	24 ± 6
	$-t = 1.75$ Gev^2 $\times 10^{-3}$		4	++ 3	+1 -	+1	92 ± 16	55 ± 12	57 ± 12	40 ± 10	72 ± 13	31 ± 8	50 ± 11	43 ± 10	54 ± 11	30 ± 8		28 ± 8	53 ± 11		42 ± 10	51 ± 11	45 ± 10	60 ± 11	56 ± 11	57 ± 12	48 ± 11	59 ± 11
	$-t = 1.45$ ev^2 $\times 10^{-3}$	8 +1 +	+1 +	+1 +	+1 -	+1	152 ± 22	148 ± 21	148 ± 19	96 ± 16	116 ± 16	78 ± 14	90 ‡ 06	70 ± 12	75 ± 12	65 ± 12	103 ± 15	116 ± 16	91 ± 14	70 ± 13	73 ± 13	72 ± 12	92 ± 14	107 ± 16	88 ± 15	69 ± 12	99 ± 15	100 ± 15
	M ² /s	0135	0036	0027	.0027	9800.	.0135	.0189	.0243	.0296	.0350	.0404	.0458	.0512	.0566	.0620	.0674	.0728	.0782	.0836	.0889	.0943	2660.	.1051	.1105	.1159	.1213	.1267
	M ² (GeV ²)	-37.5	-22.5	- 7.5	7.5	22.5	37.5	52.2	67.5	82.5	97.5	112.5	127.5	142.5	157.5	172.5	187.5	202.5	217.5	232.5	247.5	262.5	277.5	292.5	307.5	322.5	337.5	352.5

TABLE XIX

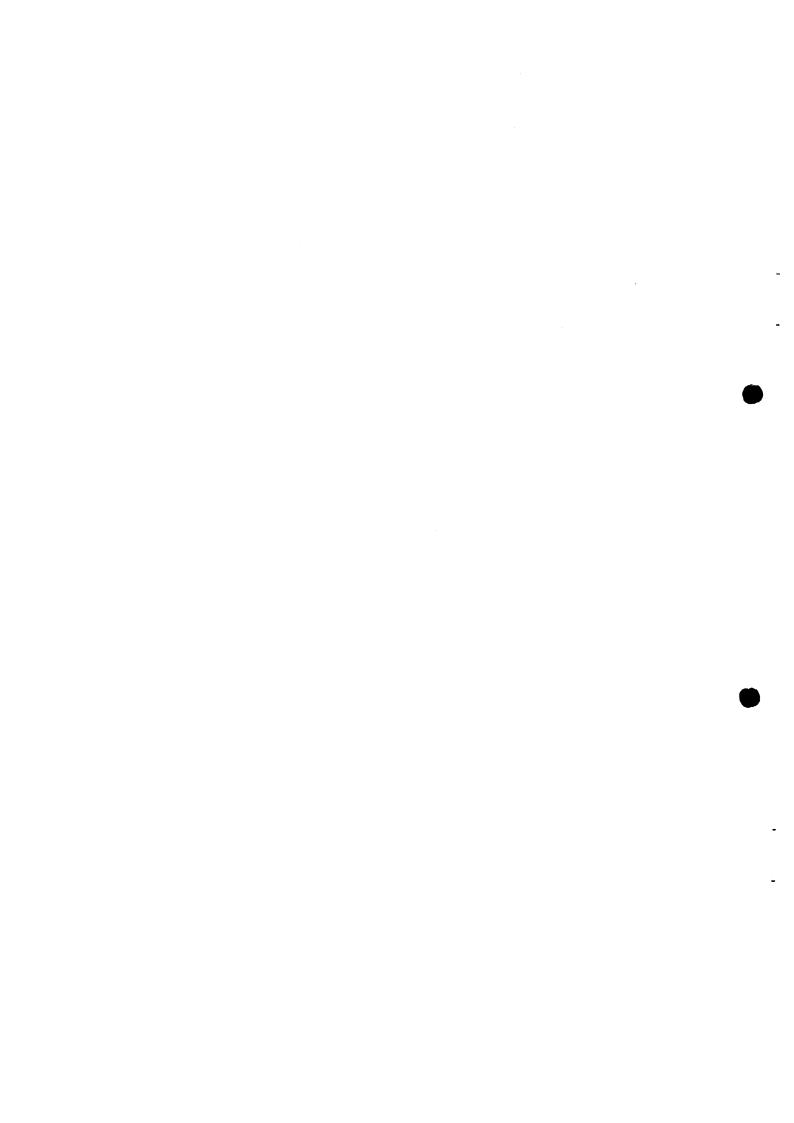
- 1	$-t = 2.65$ Gev^2 $x10^{-3}$	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
1	$-t = 2.35$ Gev^2 $\times 10^{-3}$	2 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	16.5 ± 6.5
= 3892 GeV ²	$-t = 2.05$ $6eV^2$ $\times 10^{-3}$	2 4 4 6 7 7 8 8 7 7 8 8 8 7 4 8 9 7 4 8 9 7 4 8 9 7 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1+ 1+ 11
•	$-t = 1.75$ Gev^2 $x10^{-3}$	100 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	54 ± 8 41 ± 7
SS-SE	$-t = 1.45$ Gev^2 $x10^{-3}$	25 ± 3 278 ± 27 243 ± 27 246 ± 25 164 ± 19 117 ± 16 117 ± 16 117 ± 11 117 ± 11 117 ± 12 118 ± 12 119 ± 12 110 ± 12 111 ± 11 111 ± 17 112 ± 13 113 ± 12 114 ± 11 115 ± 12 116 ± 12 117 ± 11 118 ± 11 119 ± 12 110 ± 12 110 ± 12 110 ± 12 111 ± 12 111 ± 12 112 ± 12 113 ± 12 114 ± 11 117 ± 11 118 ± 11 119 ± 12 110 ± 12	90 ± 10 82 ± 10
	$-t = 1.25$ GeV^2	0.25 ± 0.05 0.36 ± 0.09 0.36 ± 0.09 0.20 ± 0.04 0.10 ± 0.03 0.11 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.11 ± 0.03 0.12 ± 0.03 0.13 ± 0.03 0.14 ± 0.03 0.17 ± 0.03 0.18 ± 0.03 0.19 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.15 ± 0.03 0.15 ± 0.03 0.15 ± 0.03	0.14 ± 0.02 0.14 ± 0.02
	-t = 1.15 Gev ²	0.01 ± 0.01 0.02 ± 0.02 0.59 ± 0.08 0.31 ± 0.08 0.31 ± 0.05 0.22 ± 0.04 0.16 ± 0.04 0.16 ± 0.03 0.19 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.11 ± 0.03 0.12 ± 0.03 0.13 ± 0.03 0.10 ± 0.03 0.10 ± 0.03 0.11 ± 0.03 0.12 ± 0.03 0.13 ± 0.03 0.10 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.12 ± 0.03 0.13 ± 0.03 0.10 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.11 ± 0.03 0.12 ± 0.03 0.13 ± 0.03 0.19 ± 0.03	0.19 ± 0.03
	M ² /s	012800260026 .00270028 .0128 .0139 .0231 .0231 .0233 .0334 .0335 .0437 .0488 .0591 .0642 .0642 .06797 .0848 .0848 .06797 .0848 .0879 .1002	.1156 .1203
	M ² (GeV ²)	- 50 - 30 - 10 10 30 110 130 130 170 170 170 170 170 170 170 17	450

Table XXI

0.0055 ± 0.0005 0.0032 ± 0.0003 0.0130 ± 0.0010 0.0015 ± 0.0003 0.046 ± 0.004 0.028 ± 0.002 0.065 ± 0.005 3892 0.00097 ± 0.00016 0.00024 ± 0.00008 0.0132 ± 0.0010 0.0069 ± 0.0006 0.0031 ± 0.0003 0.0022 ± 0.0002 0.162 ± 0.012 0.118 ± 0.009 0.079 ± 0.006 0.051 ± 0.004 0.029 ± 0.002 0.225 ± 0.029 0.31 ± 0.04 2783 0.00039 ± 0.00008 0.00110 ± 0.00014 0.00061 ± 0.00009 0.0020 ± 0.0002 0.0049 ± 0.0006 0.0031 ± 0.0004 0.0116 ± 0.0011 0.225 ± 0.016 0.149 ± 0.012 0.092 ± 0.008 0.076 ± 0.007 0.056 ± 0.006 0.027 ± 0.002 0.57 ± 0.04 0.35 ± 0.03 1995 $M^2/\epsilon \leqslant 0.05$ (5% error added in quadrature) 3.09 ± 0.18 2.35 ± 0.14 0.97 ± 0.06 0.68 ± 0.04 1.32 ± 0.08 0.54 ± 0.04 0.34 ± 0.03 4.1 ± 0.2 1464 1.00 ± 0.06 3.07 ± 0.18 1.24 ± 0.07 0.74 ± 0.04 2.29 ± 0.14 0.43 ± 0.03 0.26 ± 0.02 4.3 ± 0.3 1239 5.4 ± 0.3 4.2 ± 0.3 3.16 ± 0.20 2.44 ± 0.16 1047 INELASTIC CROSS-SECTIONS do/dt (mb.Gev-2); 0.0245 ± 0.0015 0.0170 ± 0.0010 0.0053 ± 0.0004 0.251 ± 0.015 0.041 ± 0.003 0.192 ± 0.013 0.157 ± 0.012 0.119 ± 0.008 0.60 ± 0.04 1.65 ± 0.10 0.31 ± 0.02 1.29 ± 0.08 0.91 ± 0.06 0.35 ± 0.02 2.78 ± 0.17 2.17 ± 0.13 0.68 ± 0.04 934 0.85 ± 0.05 2.38 ± 0.14 1.10 ± 0.07 1.85 ± 0.11 3.4 ± 0.2 7.1 ± 0.5 6.3 ± 0.4 725 0.050 ± 0.004 0.041 ± 0.004 0.072 ± 0.005 0.025 ± 0.003 0.126 ± 0.009 0.182 ± 0.011 0.42 ± 0.03 2.58 ± 0.15 1.99 ± 0.12 1.46 ± 0.09 1.12 ± 0.07 0.91 ± 0.06 0.49 ± 0.03 0.33 ± 0.02 0.69 ± 0.04 + 0.5 3.7 ± 0.2 5.2 ± 0.3 549 (GeV^2) (Gev^2) 1.45 1.60 1.75 2.00 2.05 2.65 2.95 3.10 0.60 0.80 0.85 0.95 1.05 1.15 1.25 2.35 0.25 0.30 0.35 0.40 0.45 0.50 0.55 0.65 0.70 0.75

TABLE XXII

$^{\sigma}$ SD $M^2/s < 0.10$	7.61 ± 0.23	7.24 ± 0.53	7.78 ± 0.25	7.84 ± 0.30	8.28 ± 0.31	8.23 ± 0.19	
$^{\circ}$ SD M^2 s < 0.05	6.07 ± 0.17	6.05 ± 0.22	6.37 ± 0.15	6.32 ± 0.22	7.01 ± 0.28	6.80 ± 0.29	
s (GeV ²)	549	725	934	1047	1239	1464	



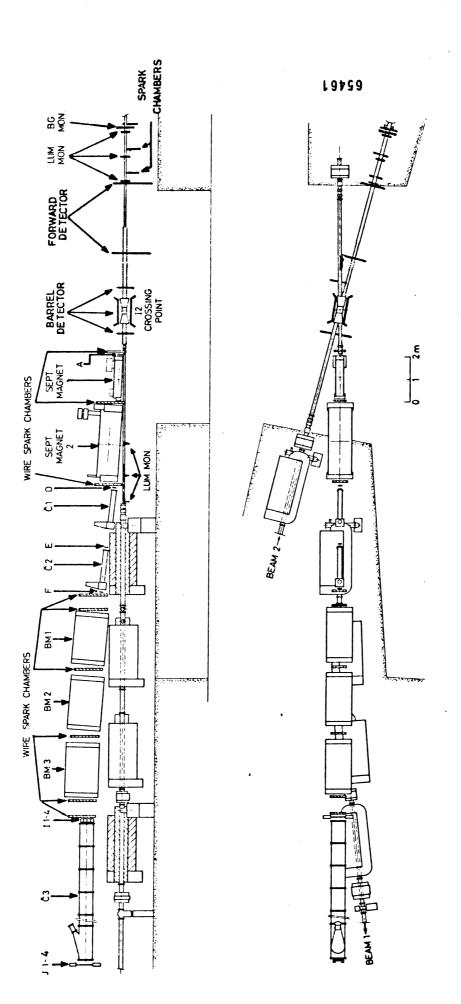


Fig. 1

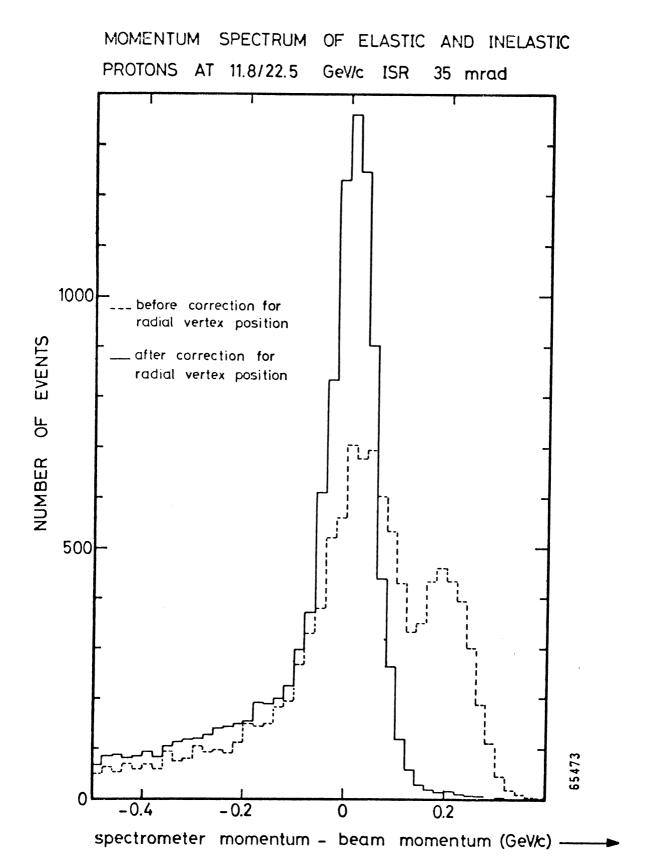


Fig. 2

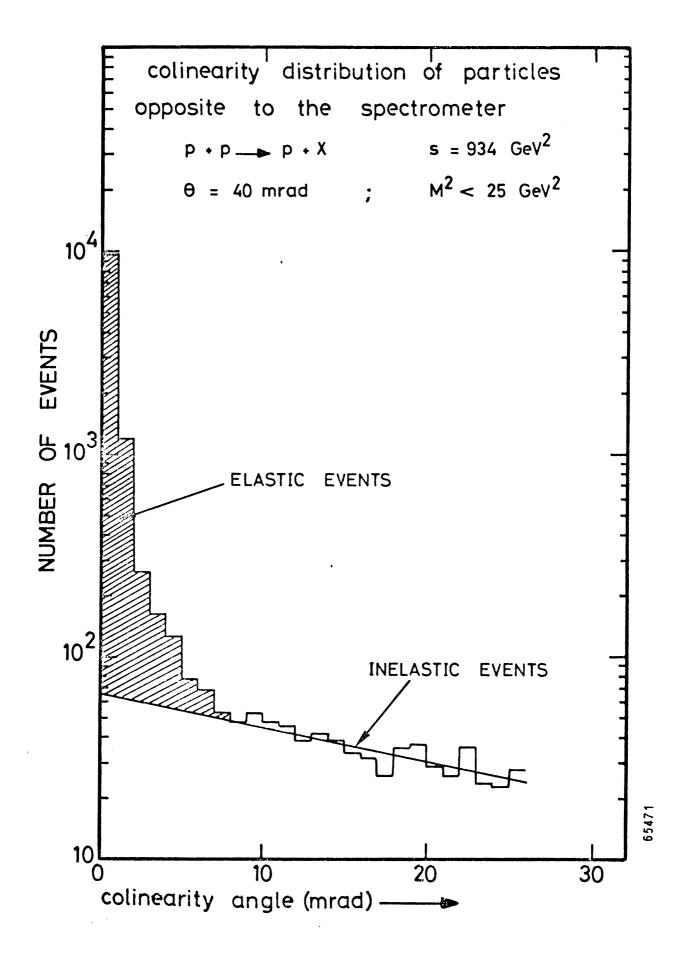


Fig. 3

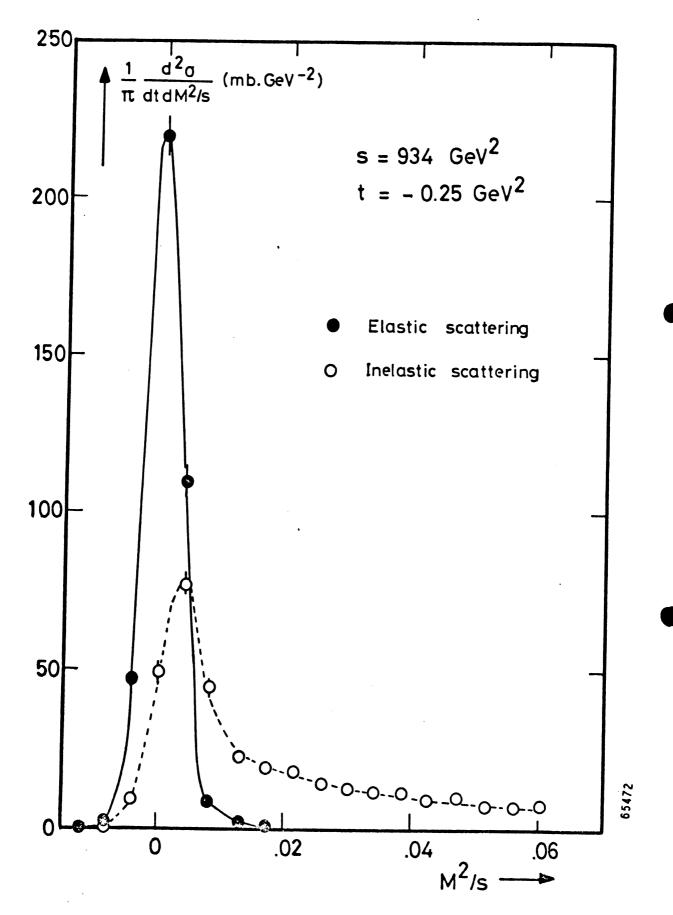


Fig. 4

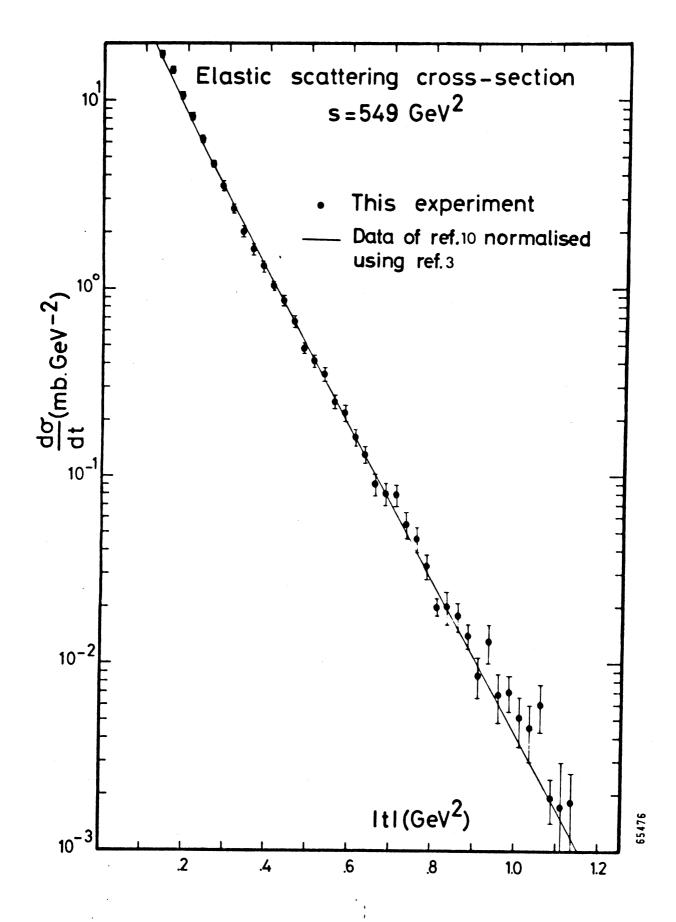
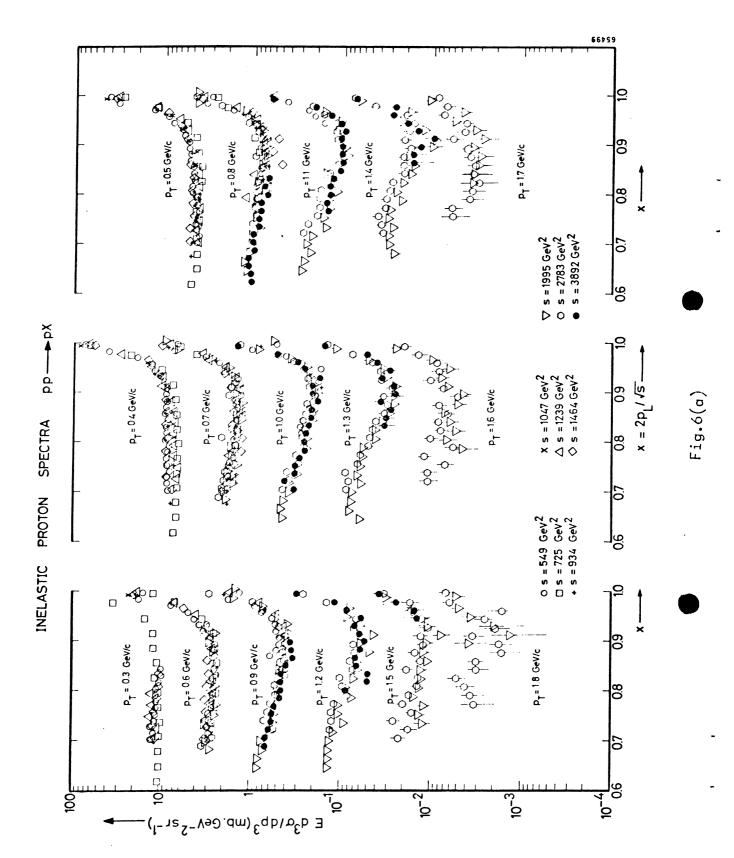
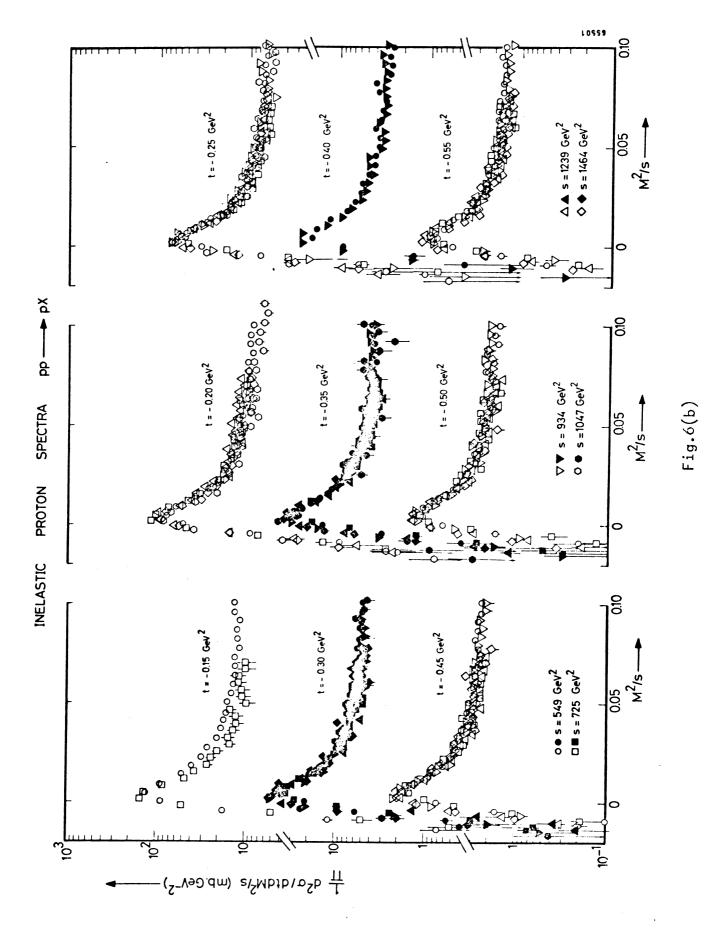
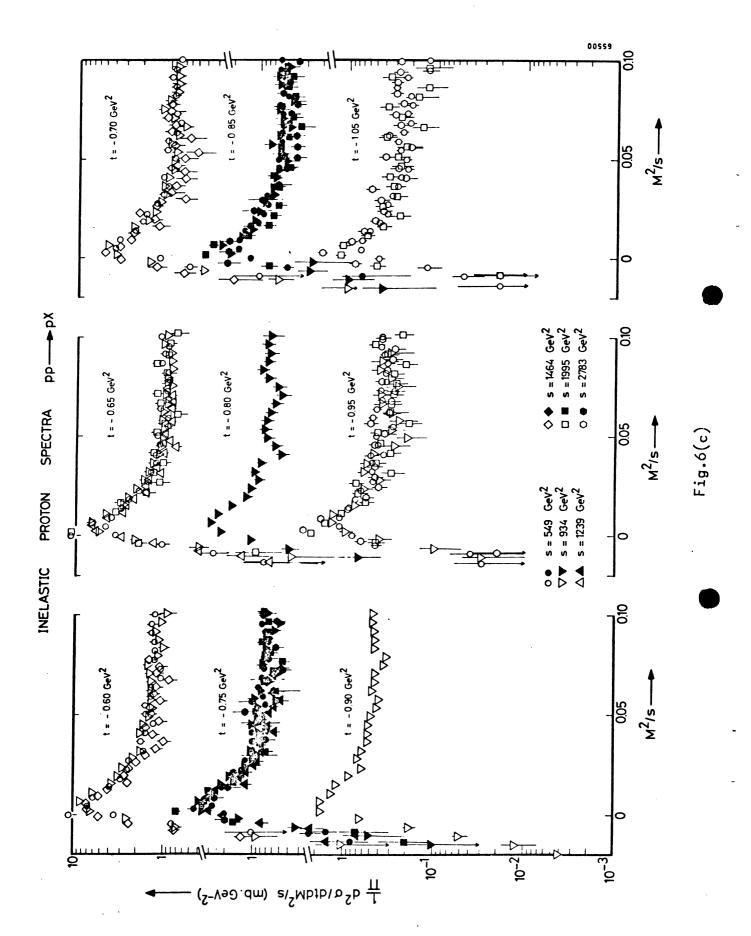
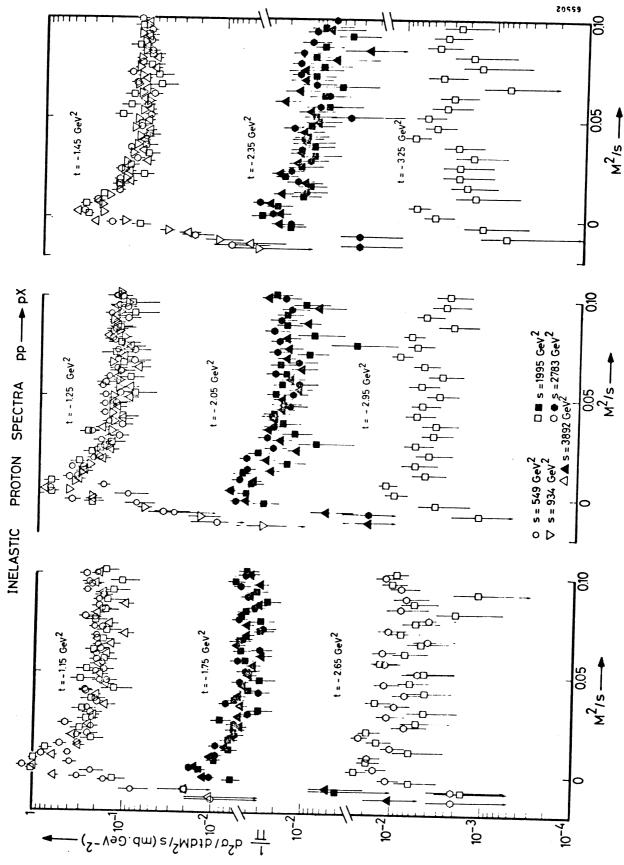


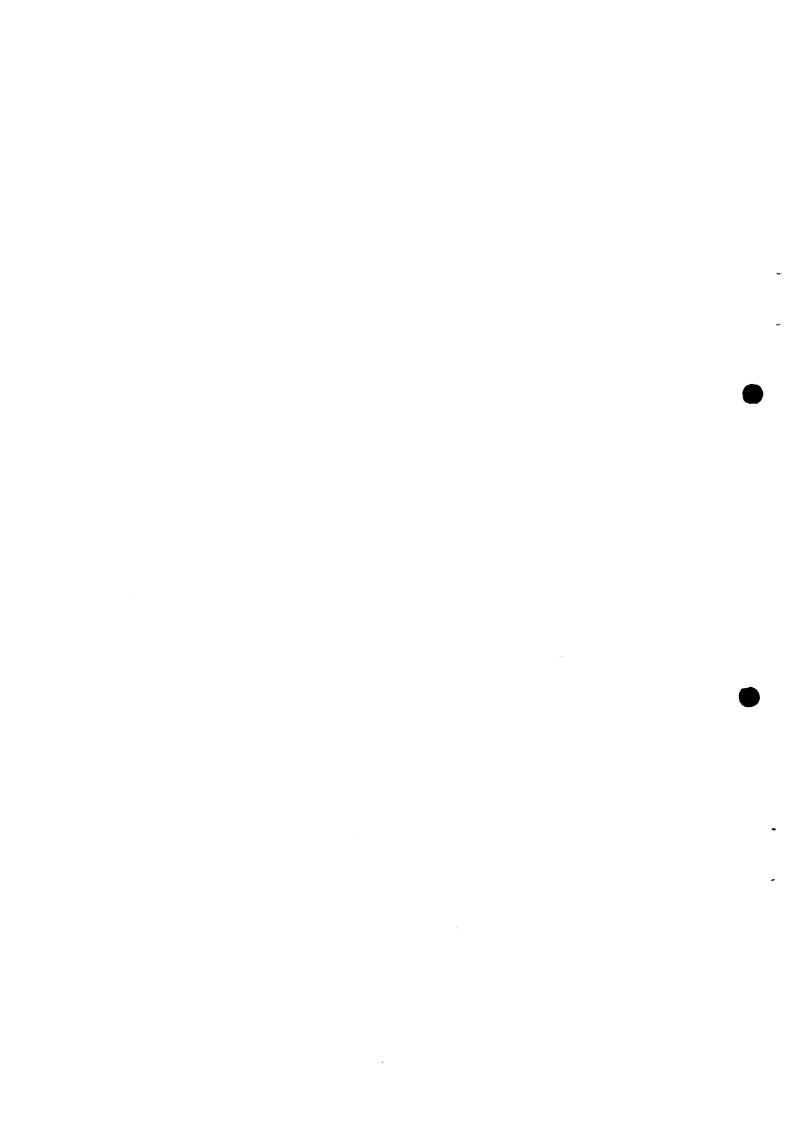
Fig. 5











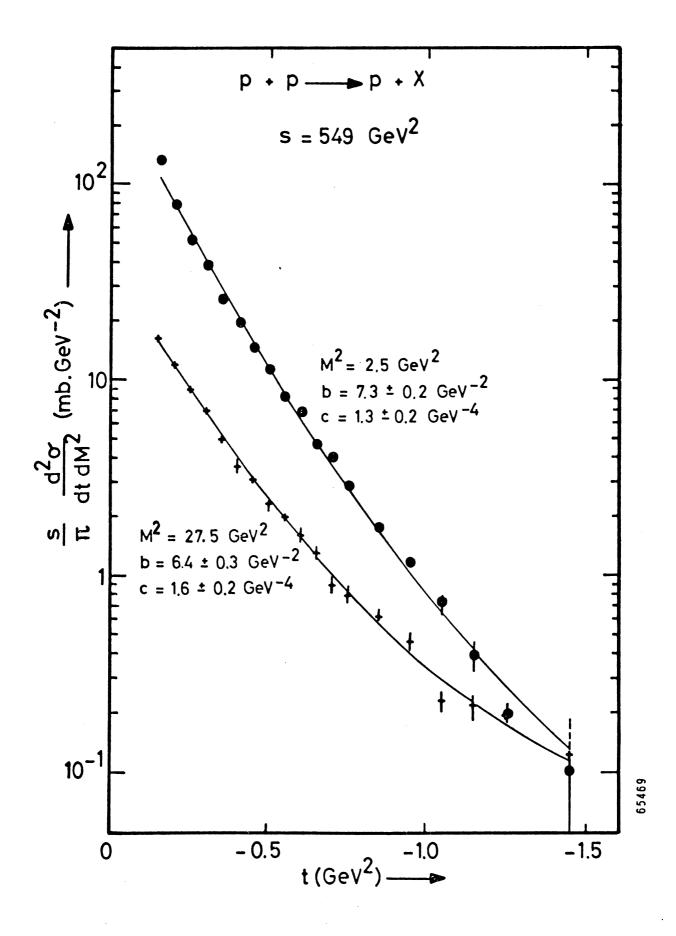


Fig. 7

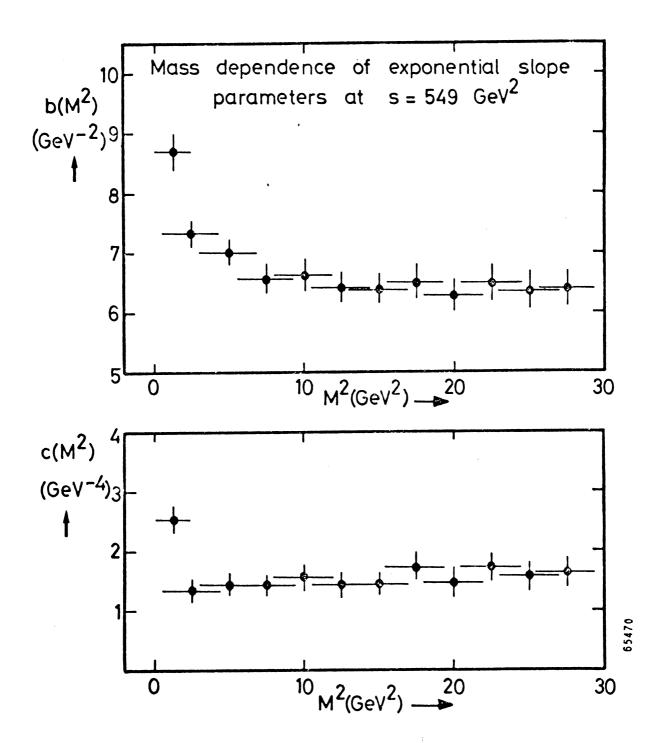


Fig.8

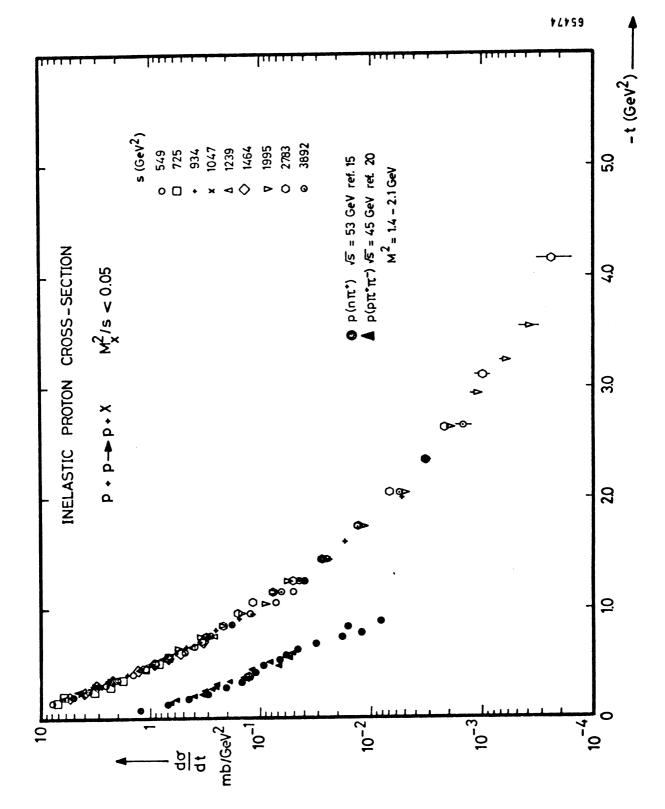
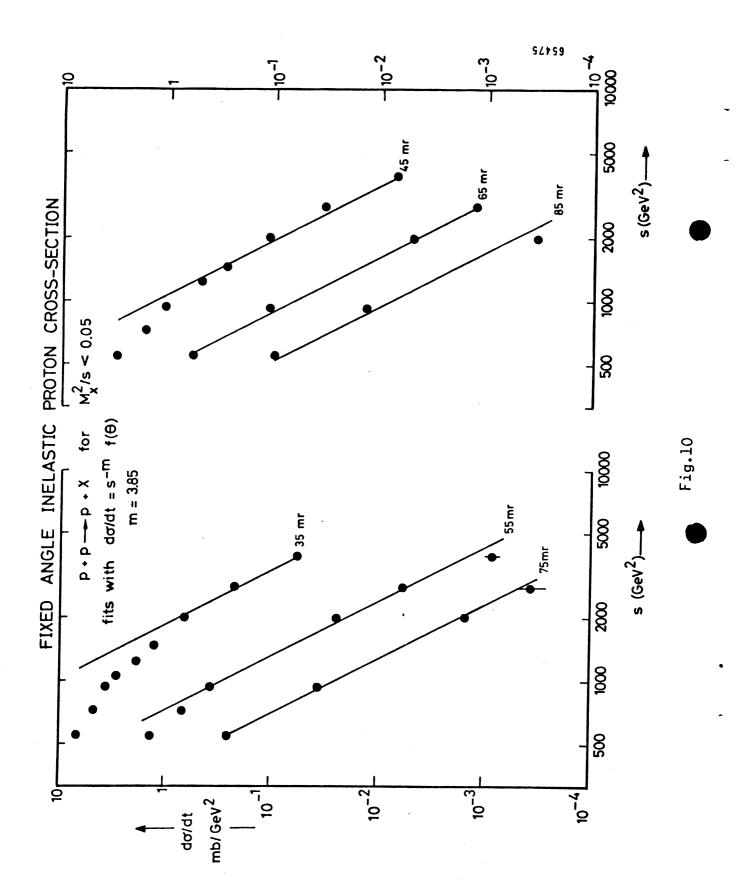


Fig. 9



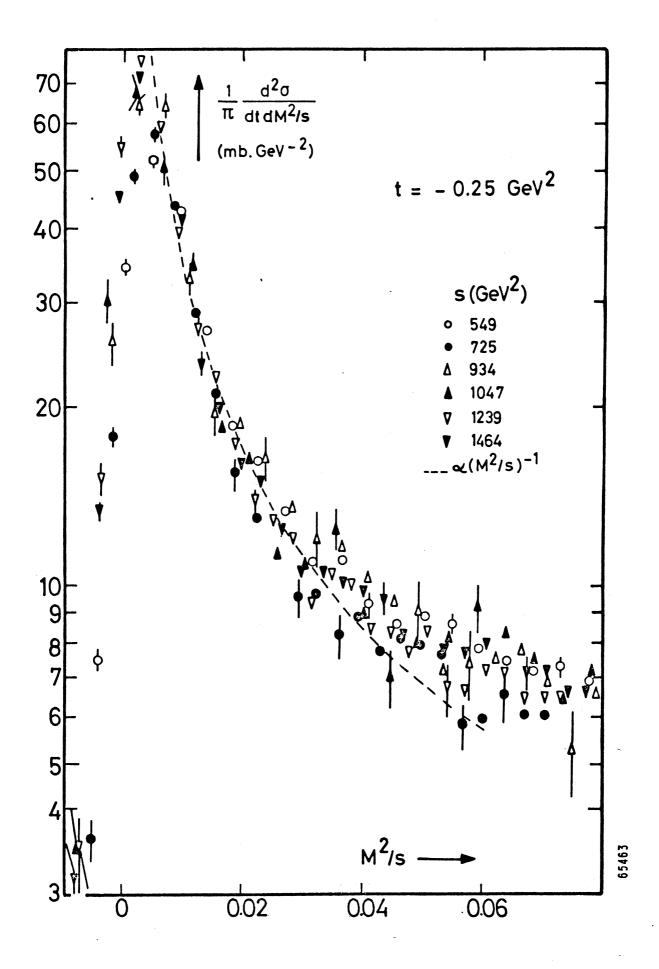


Fig.ll(a)

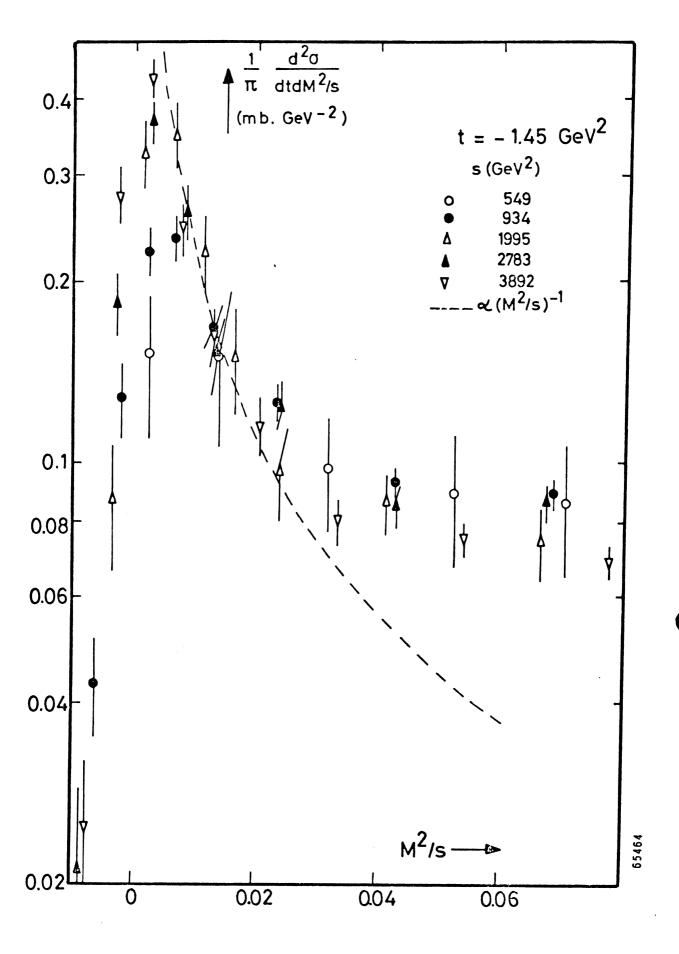
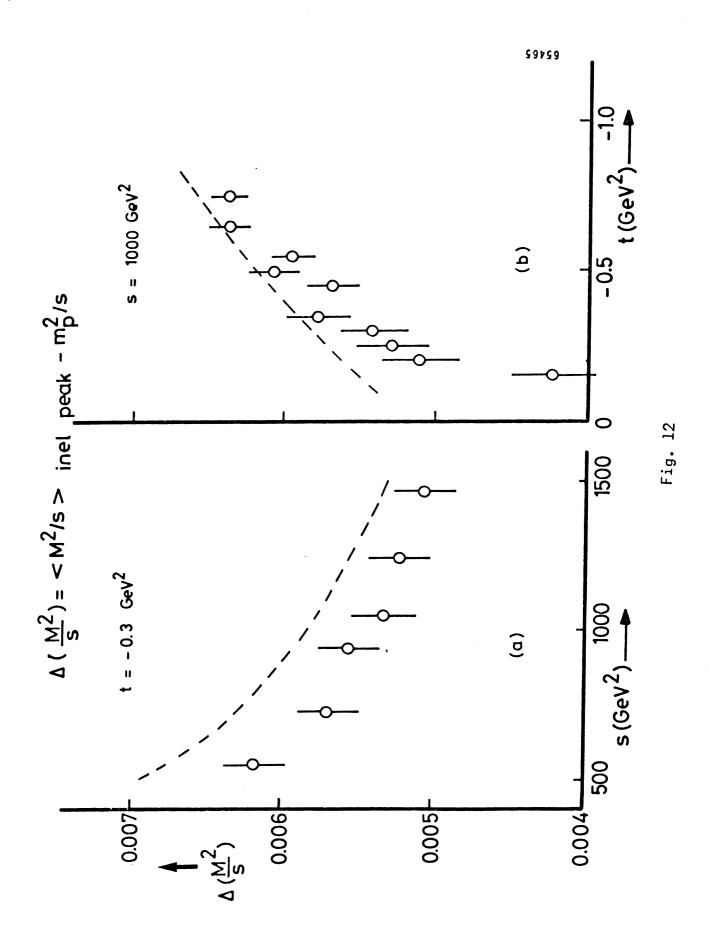


Fig.ll(b)



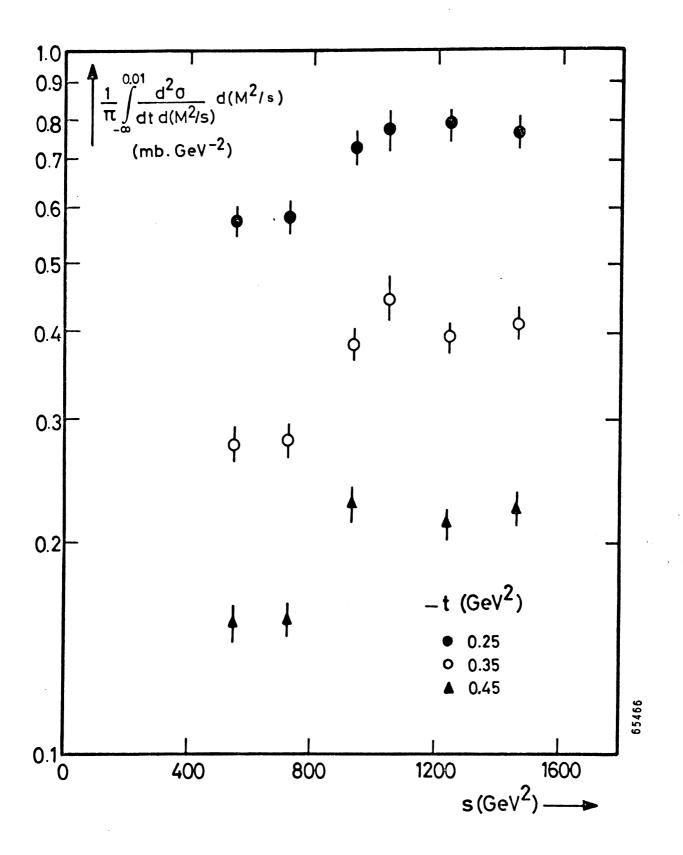
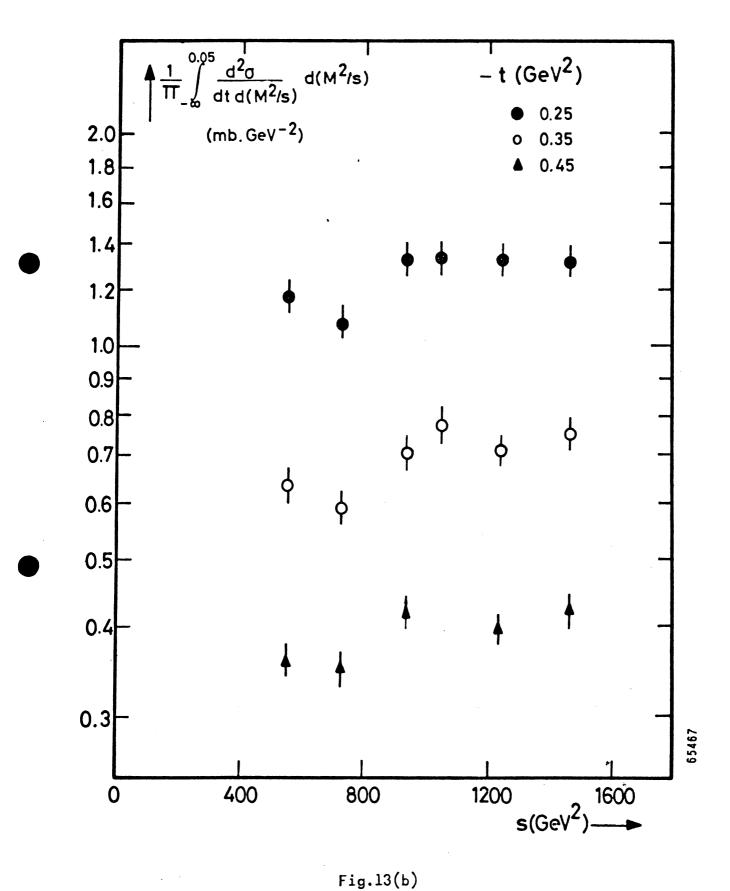


Fig.13(a)



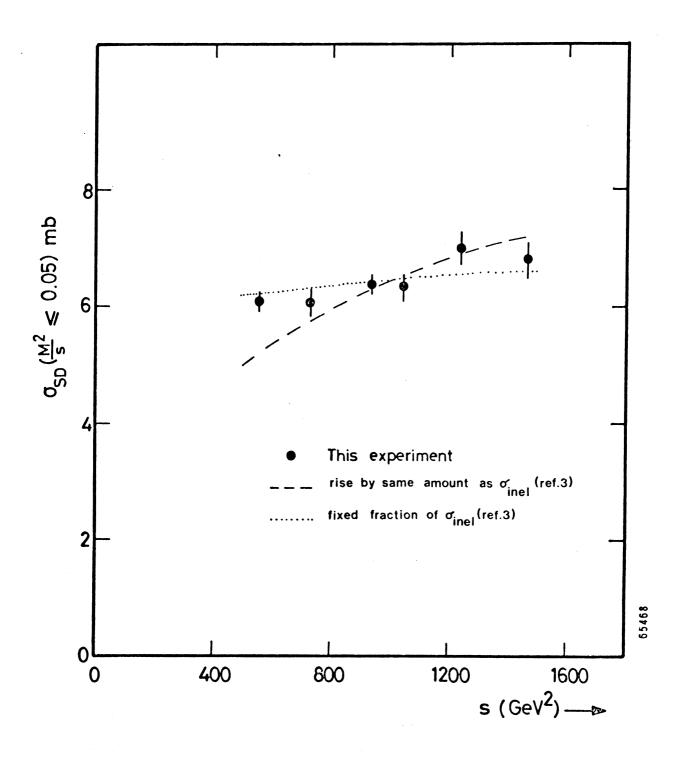


Fig. 14

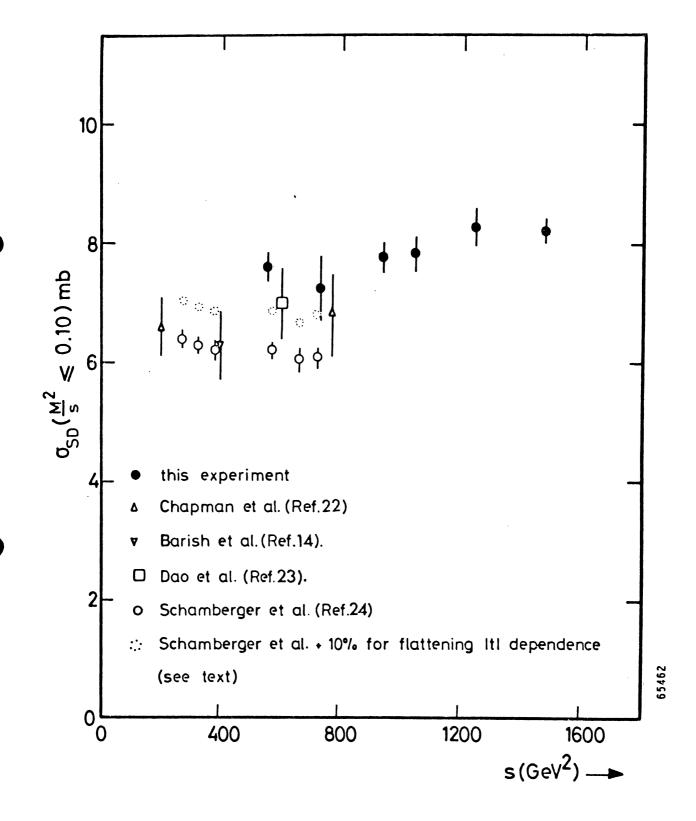


Fig. 15