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MULTIPLE SHOT AND MULTIPLE CHANNEL OPERATION
OF THE CPS FAST EJECTION SYSTEM

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Abstract :

A new system, serving all fast ejection channels of the CERN proton synchrotron, has been successfully taken into operation in autumn 1968. For the moment it has become possible to eject up to 3 consecutive bursts within one acceleration cycle. A fully new programming system permits preselection of the number of proton bunches to be ejected, the timing, the energy and the channel into which the burst is to be directed. The programme may vary from cycle to cycle. The new group of facilities has greatly improved the flexibility of beam sharing between simultaneous physics experiments.

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1. GENERAL

In 1963 a mobile small aperture kicker magnet in straight section 97, together with a mobile septum magnet a quarter or a betatron wavelength downstream in straight section 1, provided fast ejection¹⁾ into the south experimental hall. One could eject either 1 or all 20 circulating proton bunches. This system served mainly the neutrino experiment and later the g-2 experiment, when facilities had been extended to 1-5 bunches or 17-20 bunches. In a later stage, other fast ejection channels were installed using stationary septum magnets, in straight section 58 (1965)²⁾ and straight section 74 (1967)³⁾, serving the 2 m hydrogen bubble chamber in the east experimental area, respectively the 1 m heavy liquid bubble chamber in the neutrino area. An improved, radiation resistant version of the kicker magnet, permitting remote field polarity inversion, was installed in 1967⁴⁾. Channel 1 was dismantled in 1968 but may possibly be replaced by a channel starting from straight section 2. Channel 16, for ejection towards the ISR⁵⁾ is scheduled for first operation in 1970.

The rapidly growing demand for fast ejection (more channels, more experiments, double pulsing of the B.C.) made more efficient beam sharing between different channels necessary. Since the new generation of fast kicker facilities, under development elsewhere in CERN, proved to be a longer term project, it was decided in 1967 to rebuild the old system⁶⁾, aiming for installation in the summer shut down of 1968. This has been accomplished and the facilities are in operation since October 1968⁷⁾.

The new system, popularly called "Operation Straight Flush", permits ejection of up to 3 bursts into the same or different channels during the same accelerator cycle (multiple shot). The energy and timing (interdependent), the number of bunches to be ejected and the kicker magnet field polarity may be chosen for each shot. The minimum time interval between bursts is 150-200 ms, depending on energy. The programme may also be varied from cycle to cycle (sequencing).

These new kicker magnet facilities permit to serve all existing and presently planned fast extraction channels (fig. 1) and to cover all demand, probably for a few years to come.

Due to the numerous possibilities thus created, their use needs some experimenting and their full exploitation will be accomplished only gradually. Also, due to growing complexity of beam sharing schemes the urgent need for a complete and coherent beam diagnostic system is reconfirmed.

This programme required building completely new delay line pulse generators and spark gaps, incisive modification of the high voltage charging supply and construction of programmable controls for the latter, a new control and interlock system and, last but not least, a flexible programming and timing system to be able to take full advantage of the new facilities.

2. KICKER MAGNET

A central part of the fast ejection system is a mobile small aperture kicker magnet⁴⁾ of $20 \times 22 \text{ mm}^2$ useful aperture, located in the accelerator vacuum system which is locally enlarged to a tank. The magnet is moved by a hydraulic servoactuator outside the tank over a connection shaft sliding through a seal.

The kicker magnet is of the delay line type with 10Ω characteristic impedance and 85 ns filling time. The inductances given by ferrite rings, and the vacuum dielectric plate capacitors between the ferrite rings have the coaxial structure of fig. 2, the aperture being cut out of rings and plates. There are two magnet units, powered independently, fixed to a central support. The magnet may be excited up to 3000 - 3500 A, resulting in 0.12 - 0.14 Tm kick strength.

Mechanical switches, located right under the vacuum tank permit to commutate the current and hence the field direction, thus avoiding flashover difficulties encountered elsewhere with reversal of voltage polarity.

3. DELAY LINE PULSE GENERATORS

Each of the two delay line magnet units is powered through 80 m long transmission cables by a separate delay line pulser (fig. 3), using a spark gap switch (front gap). A second spark gap (tail gap) may connect the other end of the pulse forming network to a matched dumping resistor. By appropriate timing of these gaps the pulse length going to the kicker magnet may be varied between 0.1 and 2.1 μs . The RC section at the front gap gives a short rise time to the pulse, the third gap (clipping gap) gives a short fall time by short circuiting the line at the relevant moment⁸⁾. The construction is illustrated in fig. 4. The two pulsers may be operated simultaneously or separately.

The spark gaps are of the three electrode swinging cascade type⁹⁾ with an annular electrode shape to reduce the influence of erosion. The gaps are triggered by 30 kV Marx pulse generators, the overall jitter being typically 12 ns.

The pulse forming networks may be charged to 30 - 70 kV within 150 - 200 ms by a H.V. supply with ignitron switches in the primary circuit. A start pulse opens the ignitrons for full wave charging. When a voltage derived from a H.V. divider is equal to the programmed reference voltage, the phase cut angle jumps to the other side of the sine wave and the voltage is then held constant to within 1% by a servoloop.

4. ELECTRONIC CONTROLS

A program sequencer (fig. 5a) gives a synoptic display of the beam sharing scheme in case the program is varying from pulse to pulse. During accelerator operation this program sequencer is a slave of the main accelerator programmer; it then receives timing signals from the latter and retransmits them to the ejection system. During accelerator stops the program sequencer can generate autonomous programs for system test runs.

The kick and bunch selectors (fig. 5b) permit selection of the ejection parameters for each of the ejection areas programmed on the sequencer panel. The proton bunches are labelled earlier in the accelerator cycle such that it is possible to choose the first bunch and the number of bunches to be ejected for each of the subsequent shots.

The pre- and post-pulse units (fig. 5c) are preset scalars generating trigger pulses locked to the ejection pulse, before respectively after ejection. If the ejection moment is changed, the pre- and post-pulses follow automatically, maintaining the preset time interval before or after ejection. These pulses serve to synchronize the septum magnet pulse, the closed orbit deformations, RF beam steering perturbations, monitoring oscilloscope triggers, RF separators. The pulses are also available to experimental groups.

An interlock system protects ejection channels, kicker magnet and pulse generator in case of failures. There are general interlocks and area interlocks. The general interlocks switch off the power supply of the high voltage pulse generator in conditions of alarm from vacuum, temperature, pressure, overvoltage and overcurrent detectors in the kicker magnet or pulse generator. The area interlocks inhibit the firing of the pulse generator at ejection channels, in which ejection is forbidden by personal protection. There are other area interlocks in case of improper ejection into an area: if the pulses of the two kicker magnets are not equal (pulse balance), if the spark gap pressure does not correspond to the high voltage (pressure - HV balance) or if the field inverters are not in the correct position.

A monitoring system permits to display all fast high voltage signals of the kicker magnet and pulse generators as well as the magnetic kick and some low level signals on an oscilloscope for systems check out. Another scope may display slow signals such as the H.V. charging process or the kicker magnet movement.

A hydraulic programmer (fig. 6) generates an electric analog signal that is followed by the electrohydraulic servosystem¹⁰) moving the kicker magnet. The cycle is first composed of voltage steps, then smoothed by a filter and modulated onto the 400 c/s carrier wave of the feedback system.

5. OPERATIONAL EXPERIENCE

Since its first functioning in October 1968 the system has been in constant operation mostly in the double shot mode or in the triple shot mode. A number of machine development sessions have been held in order to exercise through some of the numerous new possibilities, which have by no means been exhausted. These possibilities are only gradually being discovered and included in the accelerator program, which has shown a growing complexity and diversity over the last year. The possibilities are expected to be fully exploited only some time from now.

The diagrams of fig. 7 illustrate the complexity of beam sharing schemes as practised to date.

Figs. 8, 9 and 10 give typical oscillograms taken at a machine development session, during which three partial fast ejections were made at 200 ms intervals at 19.2 GeV.

The extraction efficiency at present varies with accelerator stability and operational care and attention, but is lower in the average than in the old days of single shot ejection. The principal causes for this may be (i) larger beam diameter due to growing accelerator intensity, (ii) a bit marginal rise and fall time and intensity of the kick, (iii) growing complexity of beam sharing schemes. The first two causes can not easily be avoided and may possibly be coped with by a new generation of ejection equipment in some years from now. The third (and not the least) cause may be reduced by operator training, and more and well chosen beam diagnostic equipment.

As a whole, the system has been working surprisingly well, considering the short construction and testing time of hardly one year. This is borne out by the fact that 3 months after start-up the responsibility for the system was transferred to the very efficient MPS ejection maintenance team and since that date the construction team has never been bothered with requests for help.

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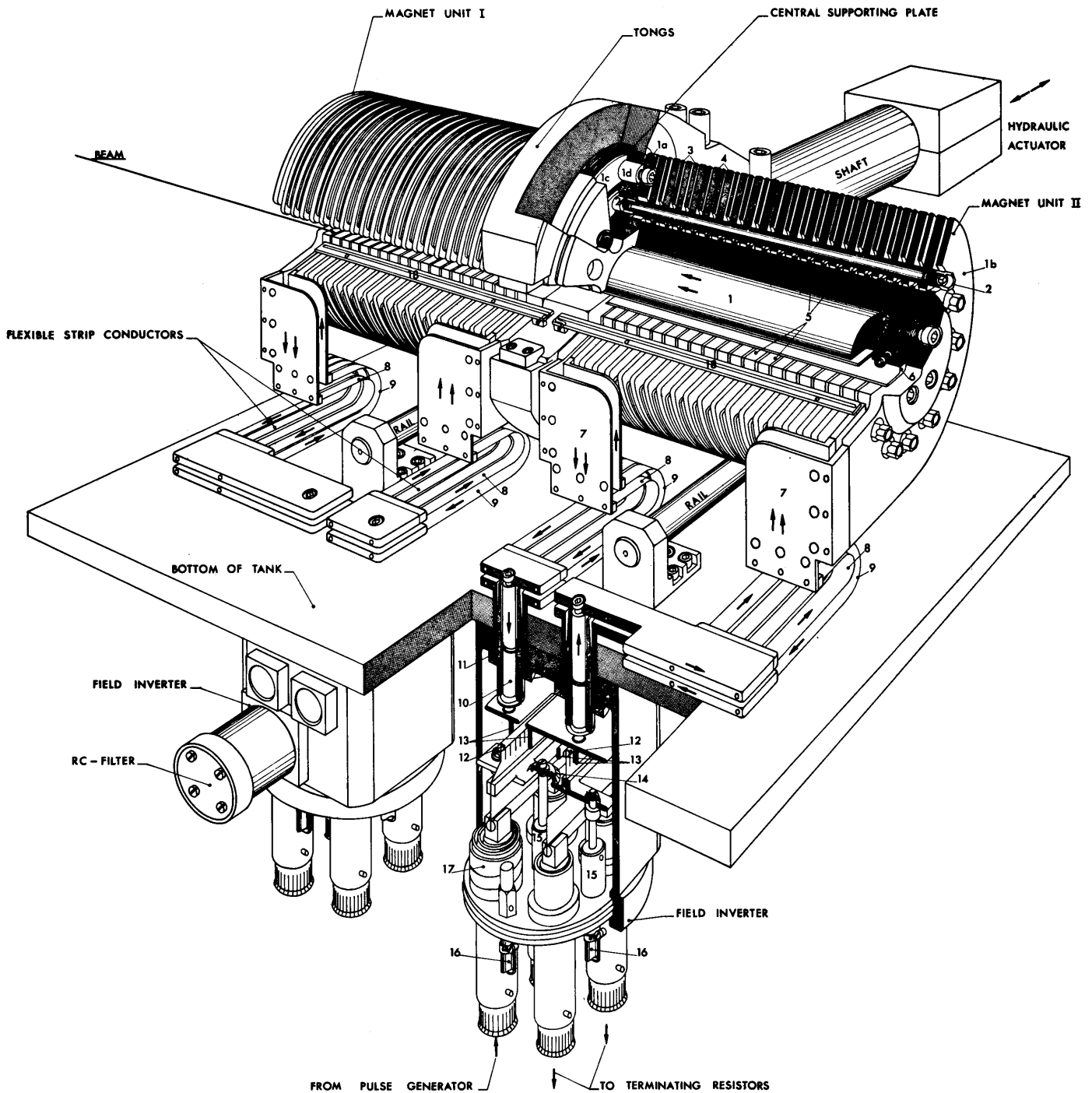


Fig.2 Perspective view and partial cut of the kicker magnet:

(1) inner conductor with (1 a) inner flange and (1 b) outer flange; (2) outer conductors, (1 c), (2 c) rings cast into central supporting plates; (1 d), (2 d) stubs welded onto rings; (3) large, thin capacitor plates of inner conductor; (4) small, thick capacitor plates of outer conductor; (5) ferrite rings, borne by inner conductor; (6) profile aligning ferrite rings; (7) plates supporting flexible strip conductors; (8) flexible strip conductors connected to inner conductor; (9) flexible strip conductors connected to outer conductor; (10) inner conductor of coaxial traversal connected to inner conductor of magnet unit; (11) earthed outer conductor connected to outer conductor of magnet; (12) moving contacts of field inverter; (13) fixed contacts of field inverter; (14) moving bypass contact; (15) pneumatic cylinders actuating field inverter; (16) pressurized air connections to cylinders; (17) electrostatic pickup ring for observation of incoming pulse; (18) long pickup loops for observing time dependence of magnetic kick.

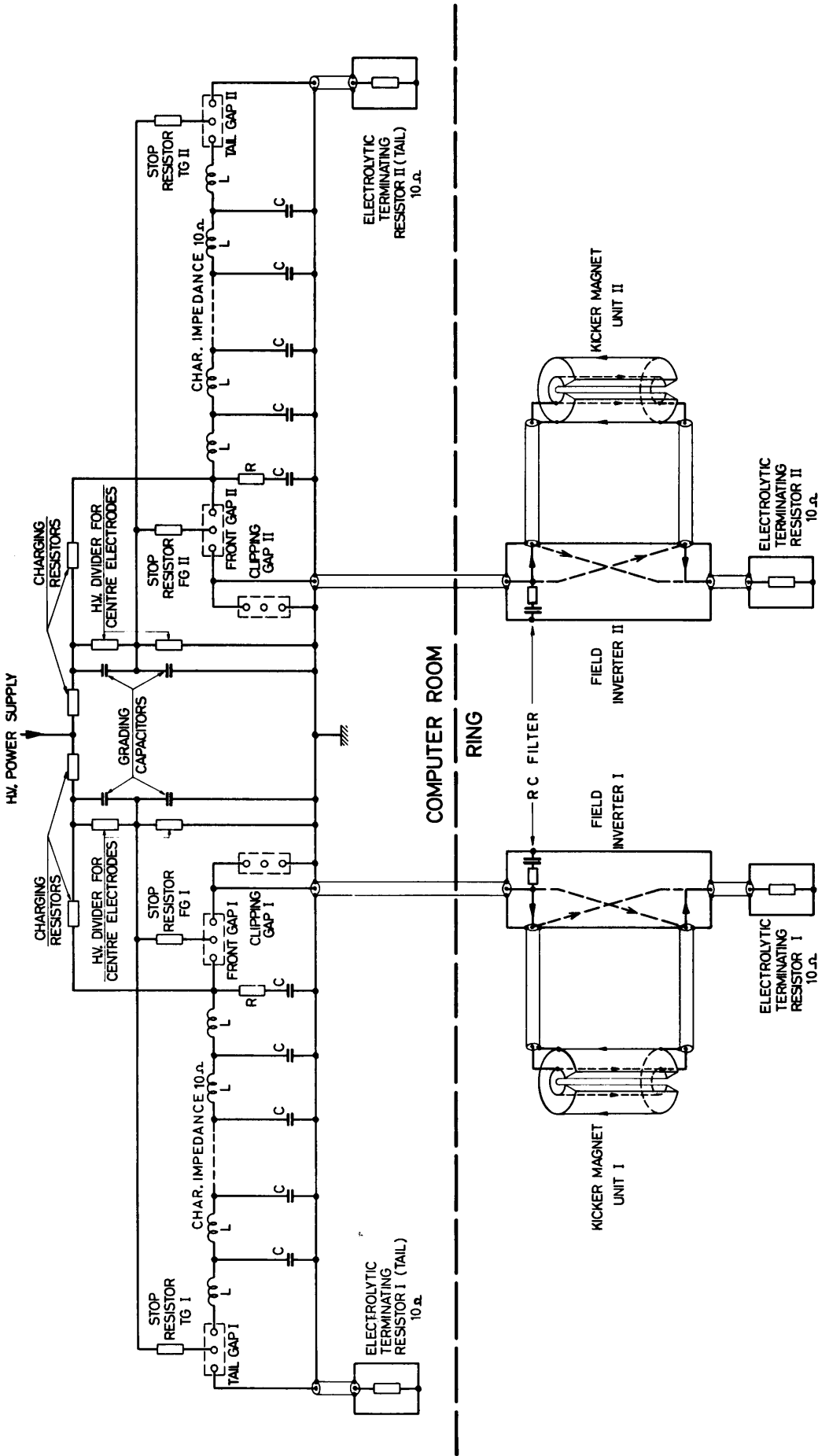


FIGURE 3 SIMPLIFIED DIAGRAM OF THE H.V. PULSE CIRCUITS. The kicker magnet consists of two units, each with a mechanical field inverter, permitting inversion of the current. Each unit is excited by its own line type pulser. The pulse duration can be adjusted by relative timing of front gap, tailgap and clipping gap.

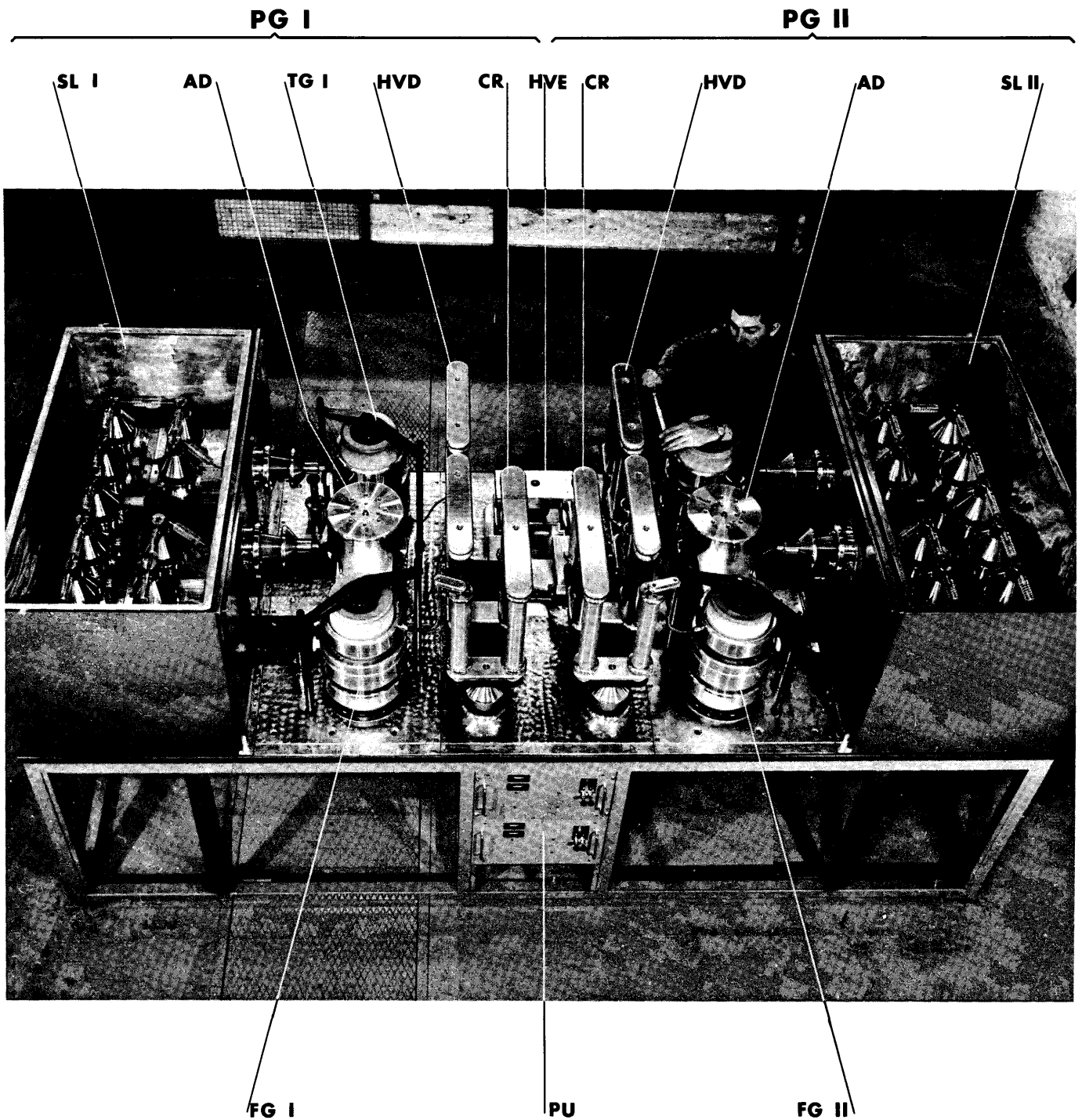


Fig. 4 Delay line pulse generators being assembled for life tests
 PG = pulse generator; SL = storage line; FG = front gap; TG = tail gap;
 AD = RC section for steep pulse front; HVD = high voltage divider for
 center electrode of sparkgaps; CR = charging resistor; HVE = high
 voltage entry from power supply; PU = air pressure unit for sparkgap.

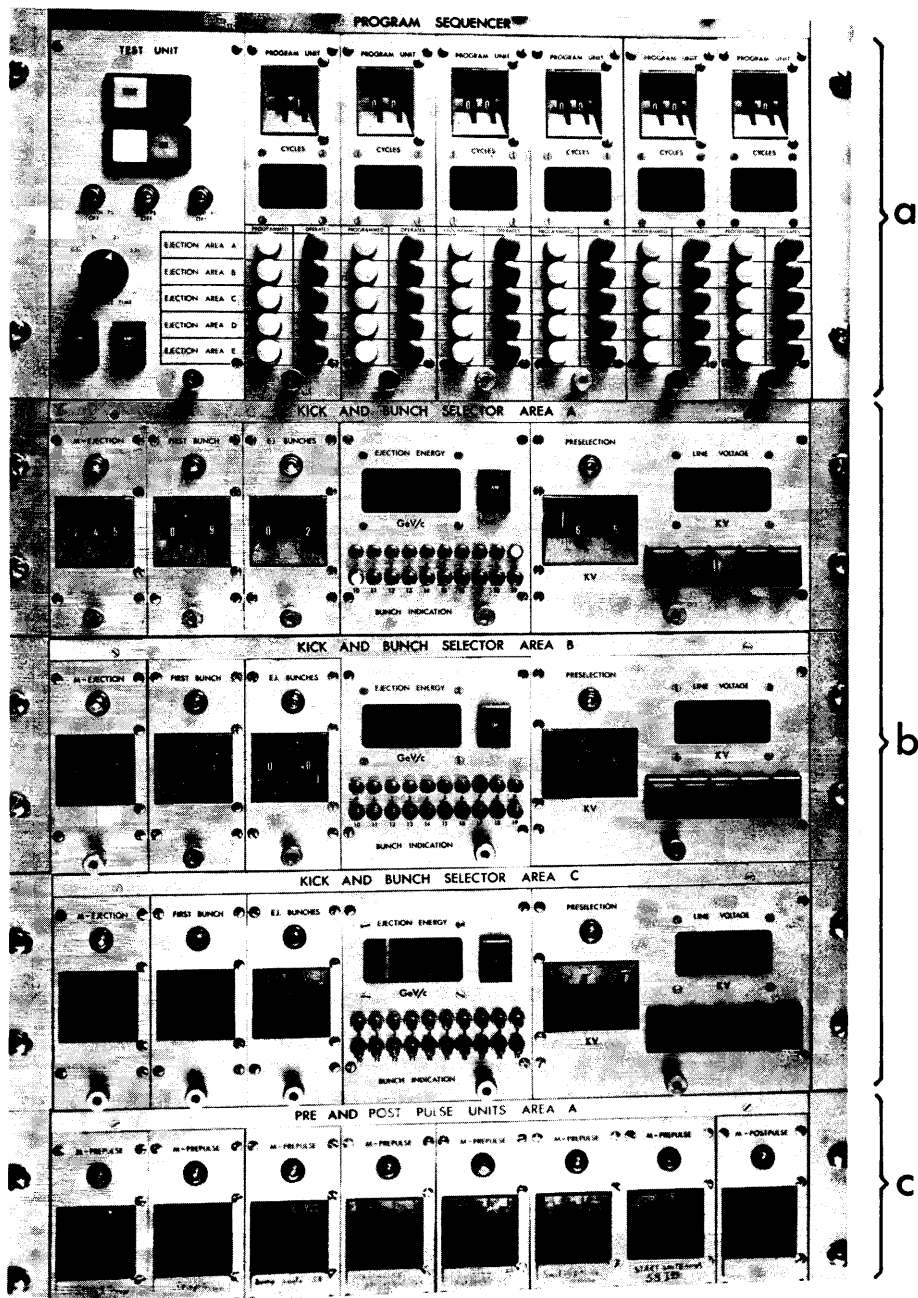


Fig. 5 Programming and Timing

a) Program sequencer

The programs are repeated for a preselected number of acceleration cycles, with Nixies displaying the counted cycles. In each program unit the ejection areas are switched on with the left-hand knob, and the right hand light flashes when the high voltage pulse generator is triggered. After completion of the preselected cycles, the next program unit is started; the last program unit restarts the first unit. For tests during stops of the PS accelerator, the test unit simulates the M-train, RF and RF/20 signals. The test cycle time can be varied between 0,5 and 3,3 sec.

b) Kick and Bunch selector

The M-ejection unit counts the M-pulse train and provides a selection of the ejection energy. The first bunch unit selects the first bunch to be ejected, and the ejected bunches unit selects the total number of bunches to be ejected. The ejection energy is calculated from the main magnetic field, and is displayed by Nixies. The line voltage is preselected, sampled immediately before ejection and displayed. Push-buttons under the line voltage display select the lines to be pulsed and the polarity of the magnetic kick.

c) Pre- and post-pulse units

For synchronization of auxiliary ejection operations or physics experiments to the ejection moments a number of units is allocated to each area. Example : a number of 23 programmed on a pre-M-pulse unit of area A, results in a trigger pulse 23 M-pulses before the ejection M-pulse of area A. The M units are for rough timing, the RF units have max. 1-2 ns jitter with respect to the first ejected bunch.

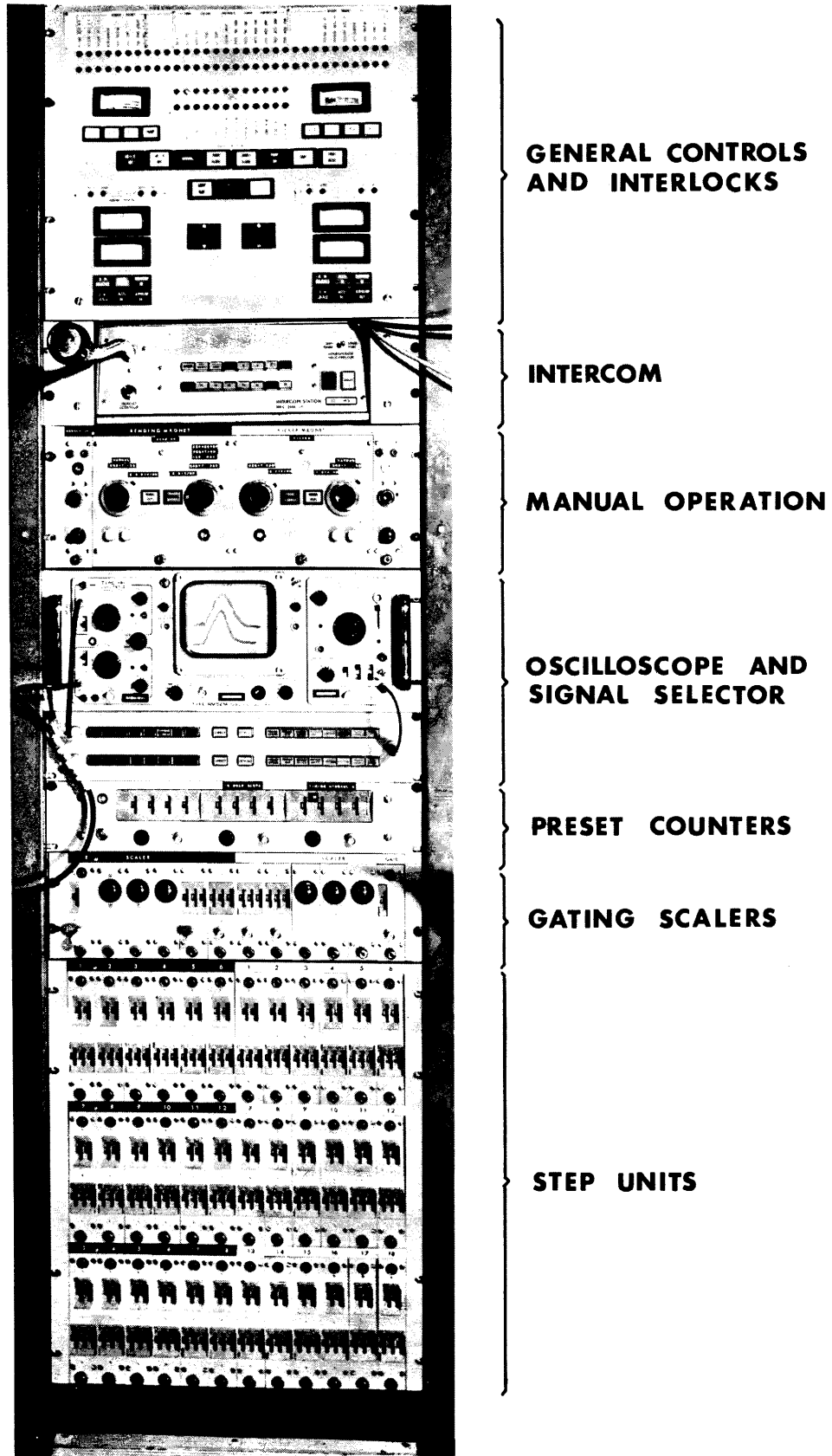


Fig. 6 Hydraulic servoactuator controls and programmer

The program is an electrical analog signal first composed in steps by the step units, then smoothed by a filter and modulated on the carrier wave of the servosystem. Each step unit is a preset counter combined with preset voltage generator. At the chosen M-pulse the analog signal assumes the voltage preselected on the unit, until the next unit takes over in the same way. The cycle may be advanced or delayed as a whole by the gating scalars which let the M-train through at chosen moments.

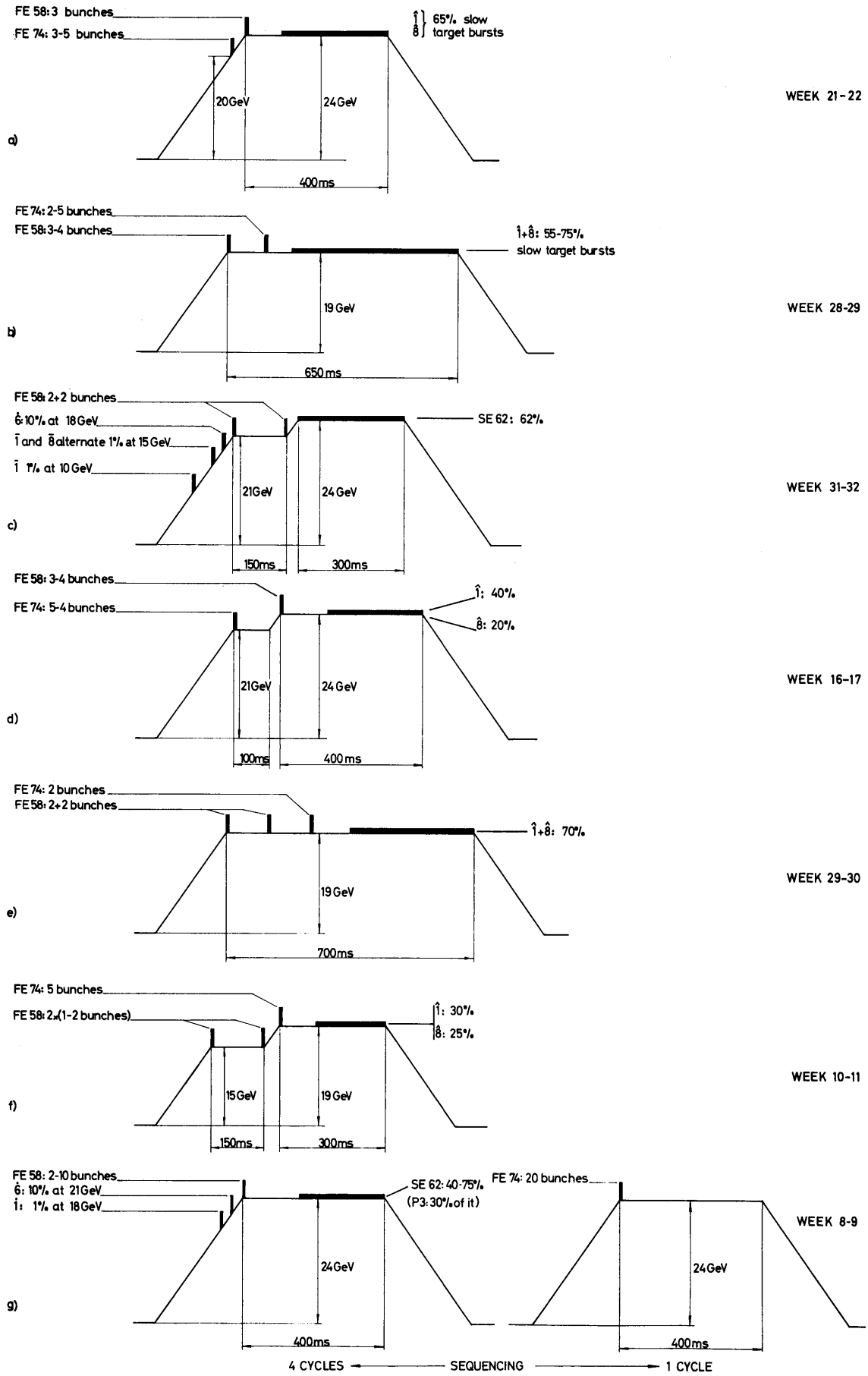


Fig. 7 Typical beam sharing schemes

FE 58 means fast ejection into channel 58, etc. SE 62 means slow ejection into channel 62. \hat{i} means a short burst on target n , \hat{h} a medium burst, $\hat{i}+\hat{h}$ a long burst.

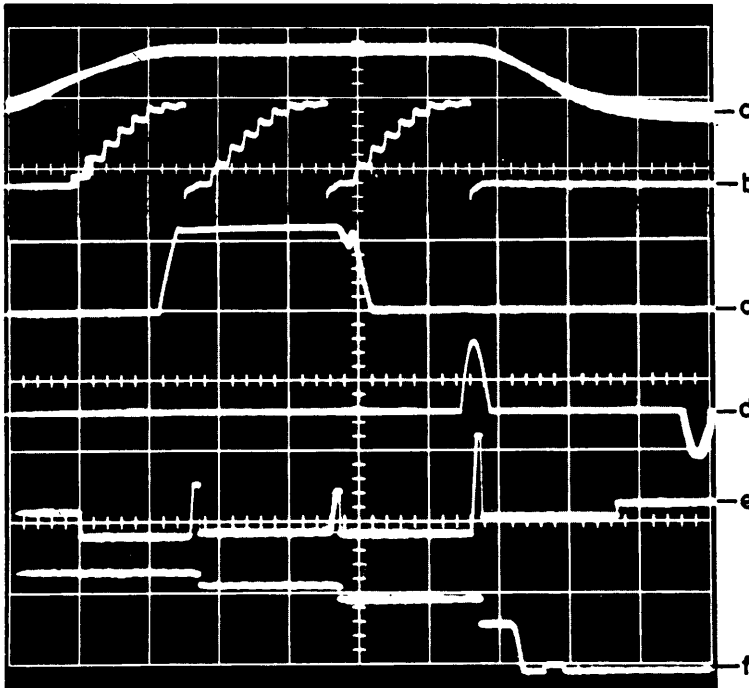


Figure 8 Triple fast ejection

Two shots are ejected into the bubble chamber channel and then one shot into the neutrino channel, all in intervals of 200 ms at 19.2 GeV/c. The oscillogrammes (100 ms/div) show

- a) kicker movement
- b) line voltage
- c) bump current during ejection into bubble chamber channel
- d) bump current during ejection into the neutrino channel
- e) RF-perturbations
- f) internal beam current trafo

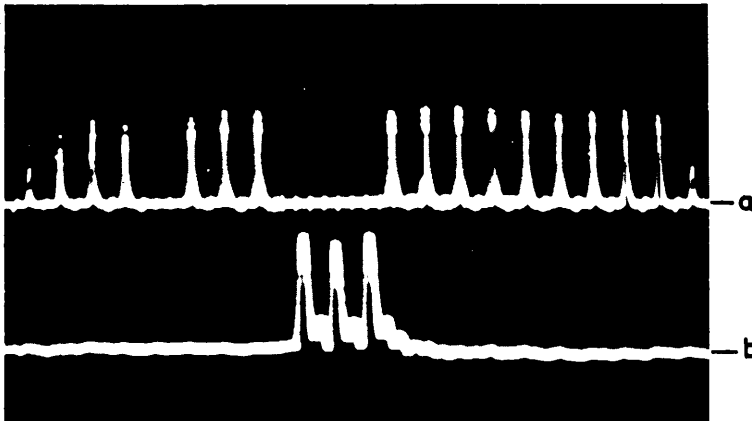


Figure 9 Second shot of triple fast ejection

The oscillogramme a) shows the bunch structure with 105 ns from bunch to bunch of the internal beam just after the second shot, 1 bunch having been ejected by the first shot and 3 bunches by the second shot. The oscillogramme b) shows the three ejected bunches of the second shot passing the bubble chamber channel.

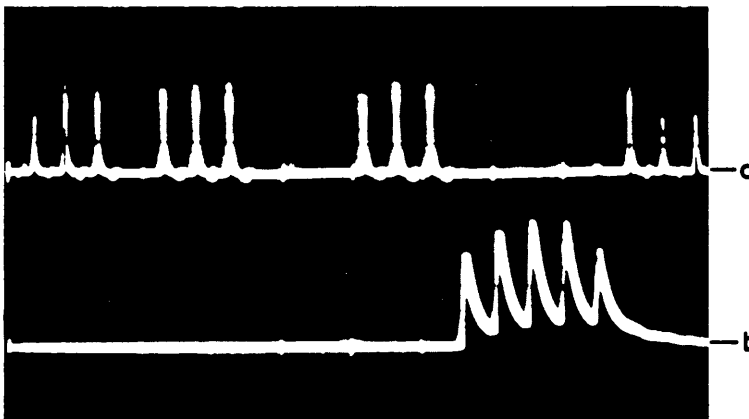


Figure 10 Third shot of triple fast ejection

The oscillogramme a) shows the bunch structure with 105 ns from bunch to bunch of the internal beam just after the third shot, 1 bunch having been ejected by the first shot, 3 bunches by the second shot and 5 bunches by the third shot. The oscillogramme b) shows the 5 ejected bunches of the third shot in the neutrino channel.