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# Direct measurement of Nb<sub>3</sub>Sn filament loading strain and stress in accelerator magnet coil segments

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## Abstract

We have directly measured, for the first time, the Nb<sub>3</sub>Sn and Cu loading strains and stresses in 11 T dipole coil segments upon compressive loading using neutron diffraction. For this purpose a load frame that enables rotation of the sample load axis with respect to the neutron scattering geometry was installed in the Stress-Spec beamline at the Heinz Maier-Leibnitz FRM II neutron source. The neutron diffraction data suggests that the magnet coil wound of Rutherford type cables can be considered as a fibre reinforced composite material. In the axial load direction the load is mainly carried by the Nb<sub>3</sub>Sn filaments and the composite stiffness can be estimated by the rule of mixtures assuming iso-strain conditions in all composite constituents. Under transverse compression the fully annealed Cu provides an isotropic pressure around the Nb<sub>3</sub>Sn filaments. The transverse load stresses in the Cu and Nb<sub>3</sub>Sn are similar, indicating iso-stress behaviour of the coil constituents under transverse compression. The broadening of the Nb<sub>3</sub>Sn diffraction peaks above critical stress values indicates reversible and irreversible Nb<sub>3</sub>Sn loading stress effects.

Keywords: Nb<sub>3</sub>Sn, accelerator magnet, diffraction

(Some figures may appear in colour only in the online journal)

## 1. Introduction

The mechanical stress exerted on the coils of superconducting magnets affects their ultimate performance limits. Reversible critical current ( $I_c$ ) changes of Nb<sub>3</sub>Sn conductors are commonly ascribed to elastic lattice distortions [1–3]. When the externally applied load exceeds a critical value, crack formation in the Nb<sub>3</sub>Sn filaments causes an irreversible  $I_c$  degradation [4].

In solenoid magnets the Lorentz forces mainly cause a tensile stress in the axial conductor direction. The effect of uniaxial tensile loading on the superconductor strain state and superconducting properties has been studied extensively, and the strain state in composite wires and tapes and the load

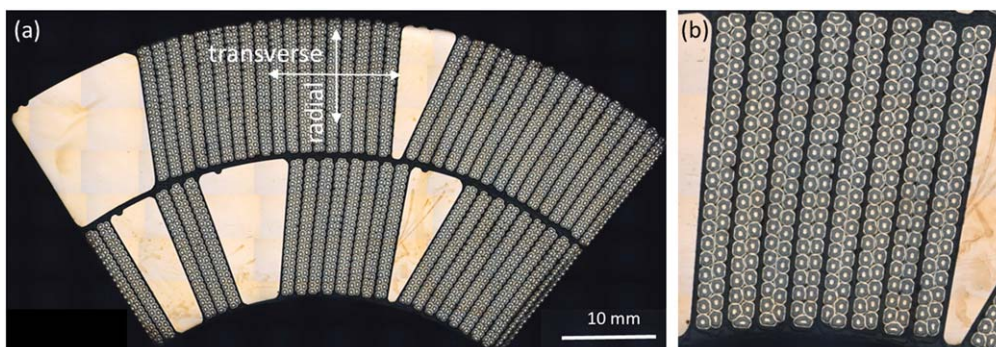
transfer among the different conductor constituents could be measured directly as a function of uniaxial tensile stress [5–9].

In order to keep coil inductance within acceptable limits, Nb<sub>3</sub>Sn accelerator magnet coils are wound using high current Rutherford type cables [10]. A cross section of the 11 T dipole coil made of Nb<sub>3</sub>Sn Rutherford cables is presented in figure 1. The void space between the electrically insulated cables is filled with an epoxy resin in order to improve the critical stress levels that the conductor can resist without an irreversible conductor degradation by filament breakage.

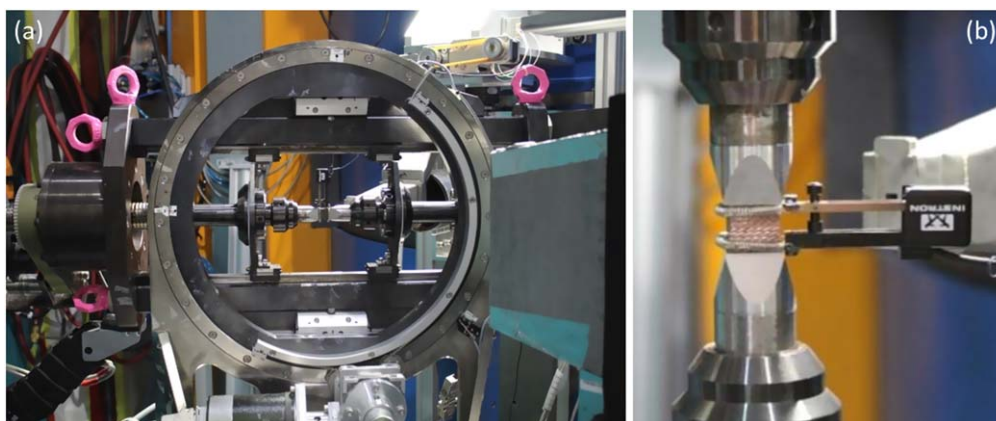
In accelerator magnets [11] like the Nb<sub>3</sub>Sn magnets presently build for the LHC High Luminosity upgrade (HL-LHC) [12], or those developed for the Future Circular Collider study, the dominant load case is transverse compressive loading. It is well known that transverse compressive stress can cause a strong degradation of the Nb<sub>3</sub>Sn superconducting properties [13]. When the macroscopic transverse compressive stress exerted at room temperature on a 11 T dipole Rutherford cable



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**Figure 1.** (a) Metallographic cross section of 11 T dipole coil with six conductor blocks with definition of transverse and radial directions. (b) Detailed view of a conductor block.



**Figure 2.** (a) Load frame mounted in Eulerian cradle in the Stress-Spec beamline in horizontal measurement position. (b) Nb<sub>3</sub>Sn Rutherford cable stack mounted for a compression test with the extensometer attached.

exceeds about 150 MPa the conductor is permanently degraded, presumably due to cracking of the brittle Nb<sub>3</sub>Sn filaments [14].

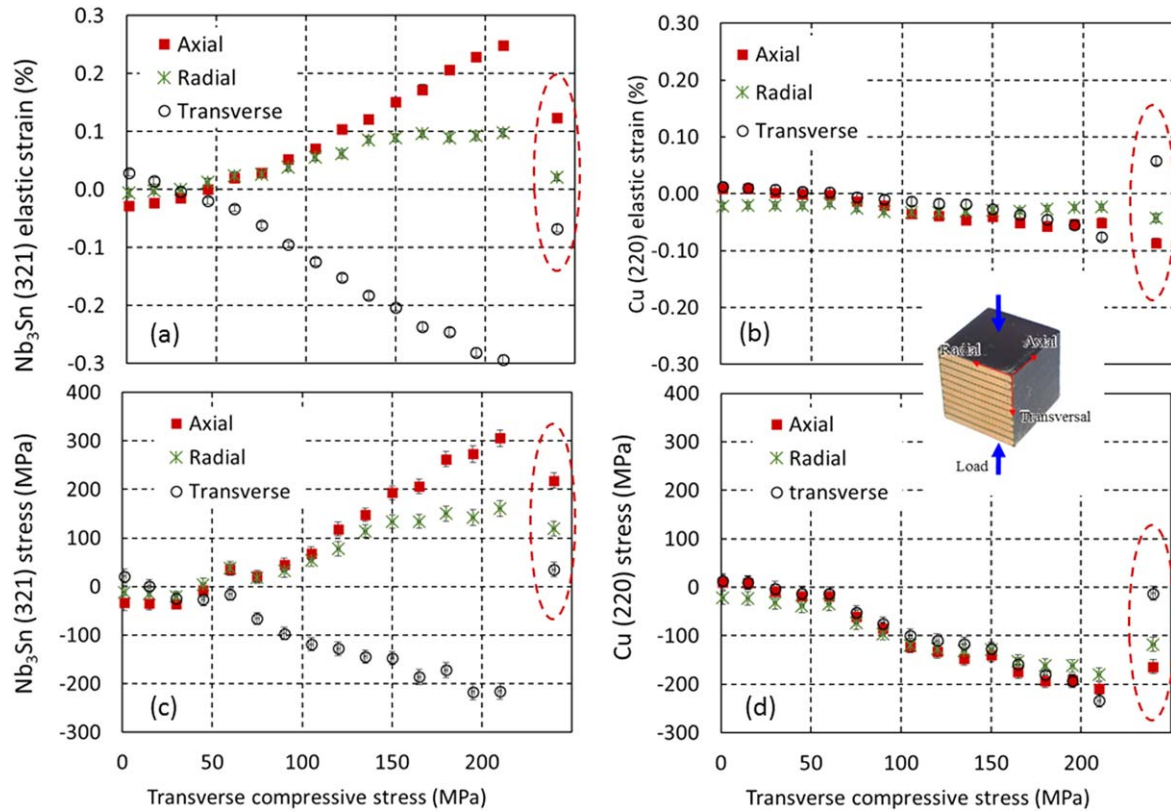
A detailed understanding of the stress–strain behaviour of the conductor blocks and their constituent materials under superconducting accelerator magnet assembly and operating conditions is required to better understand the degradation mechanisms, and to further optimise the conductor and magnet design. So far, the Nb<sub>3</sub>Sn strain and stress state evolution in magnet coils during application of an external load is not well known, and the stress–strain behaviour of conductor blocks has often been modelled using estimated average isotropic material properties [15].

State-of-the-art neutron scattering facilities like the Stress-Spec strain scanner at the FRM II neutron source [16] enable direct residual and applied strain measurements in accelerator coil segments. Previously we reported on residual Nb<sub>3</sub>Sn strain remaining in 11 T Nb<sub>3</sub>Sn dipole magnet coil segments after magnet cold testing and disassembly [17]. In this article we report, for the first time, on a direct measurement of the effect of externally applied transverse and axial compressive stress on the internal strain and stress state in the different composite coil constituents.

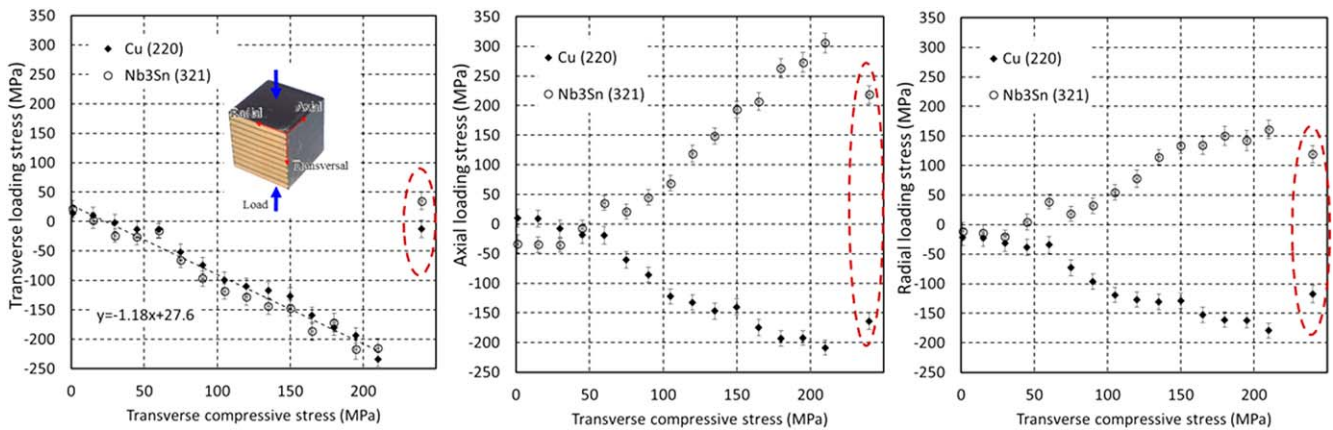
## 2. Experimental

### 2.1. The samples

The samples studied are stacks made of ten reacted Nb<sub>3</sub>Sn Rutherford cables used for the 11 T dipole coils (so-called ten-stack samples). The 11 T dipole cables with a nominal width of 14.7 mm and a mid-thickness of 1.25 mm, are stacked alternately in order to compensate for the keystone angle of 0.79° [10]. The Rutherford cables are made of 40 Restacked-Rod Process (RRP) type Nb<sub>3</sub>Sn strands from Oxford Instruments Superconducting Technology, now Bruker-OST. The Nb<sub>3</sub>Sn heat treatment was performed with a ramp rate of 50 °C h<sup>-1</sup> and comprised three isothermal plateaus of 210 °C-48 h, 400 °C-48 h and 665 °C-75 h. The cables with a 25 μm thick stainless steel core are surrounded by a 0.15 mm thick cable insulation made of a mica tape and S2/E-glass fibre. A non-impregnated and an impregnated cable stack were used for the experiments in the transverse and axial load directions, respectively. The height of the non-impregnated and impregnated ten-stack samples was 16.6 mm and 15.6 mm, respectively. For more information about the samples see [18].



**Figure 3.** (a) Nb<sub>3</sub>Sn (321) and (b) Cu (220) loading strains and (c) Nb<sub>3</sub>Sn (321) and (d) Cu (220) stresses in non-impregnated 11 T dipole cable stack as a function of externally applied axial transverse compressive stress. Circled data points show the residual strain when the external stress is released.



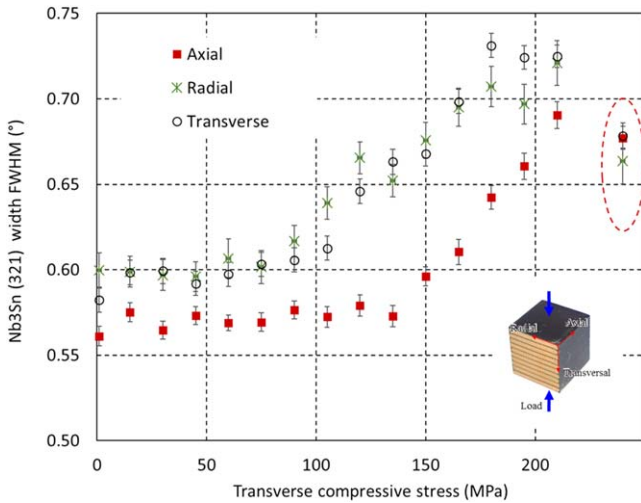
**Figure 4.** Comparison of Nb<sub>3</sub>Sn (321) and Cu (220) loading stress evolution in (a) transverse, (b) axial and (c) radial directions as a function of externally applied transverse compressive stress. Circled data points show the residual strain when the external stress is released.

**2.2. Loading strain measurements**

Loading strains were measured at ambient temperature *in situ* under a neutron beam as a function of externally applied stress. Compressive stresses were applied either in the transverse or in the axial direction using a load frame combined with an Eulerian cradle that enables rotation of the sample load axis with respect to the scattering geometry (figure 2). The maximum force that can be applied with the load frame is 50 kN, corresponding to a maximum compressive stress of 220 MPa on the samples with a cross section of 225 mm<sup>2</sup>. The

effect of friction on the stress–strain results was limited by adding lubricant (PTFE spray) on the sample to pressing tool contact surfaces. In order to limit buckling effects, the sample height does not exceed the sample width. Force measurements were performed with an HBM Type 03 50 kN load cell, and the sample strain was measured with an Instron 2620-602 extensometer with a gauge length of 13.1 mm (figure 2).

All experiments were started with a compressive preload of about –0.2 kN, corresponding with a pre-stress of about 1 MPa. Measurements were performed with applied stress



**Figure 5.** Nb<sub>3</sub>Sn (321) diffraction peak width evolution as a function of externally applied transverse compressive stress. Circled data points show the residual strain when the external stress is released.

steps of 15 MPa, and the load rate between the stress plateaus was always 50 N s<sup>-1</sup>.

A bent Si (400) monochromator provides a neutron beam with an approximate wavelength of  $\lambda = 1.672 \text{ \AA}$ . Lattice strain measurements were performed in the assumed principal stress directions, which are in the following referred to as axial, radial and transverse directions. The transverse direction corresponds to the azimuthal direction in a coil. A diffraction angle range  $70.5^\circ < 2\theta < 83.5^\circ$  was recorded, and the Nb<sub>3</sub>Sn (321) and Cu (220) reflections were fitted by Gaussian functions. In addition to the pure Cu stabiliser, the reacted RRP type conductor contains  $\alpha$ -bronze in the Nb<sub>3</sub>Sn subelement cores. Because of the Sn in solid solution the Cu lattice parameter of  $\alpha$ -bronze is larger than the pure Cu lattice parameter, and both diffraction peaks could be distinguished in the experiment. Only the pure Cu diffraction peak has been fitted and taken into account in the elastic strain calculations.

Previous stress dependent synchrotron x-ray diffraction measurements where a large d-spacing range could be recorded [6] have shown that the Nb<sub>3</sub>Sn (321) reflection represents the overall Nb<sub>3</sub>Sn strain behaviour well. In face-centred cubic materials like Cu the effect of intergranular stresses on peak position is comparatively strong on (200) reflexes [19], therefore, these peaks have been avoided. Prior to peak fitting the diffractograms were corrected for the detector efficiency using incoherent scattering from a vanadium scan. The diffraction angles are an average inside the analysed gauge volume of nominally  $5 \times 5 \times 5 \text{ mm}^3$ , which is defined by a  $5 \times 5 \text{ mm}^2$  slit that shapes the beam and by a radial collimator in front of the detector. The acquisition time for the recording of the Nb<sub>3</sub>Sn (321), and Cu (220) diffraction peaks in the three directions is about 45 min per measurement point. The main Nb (100) peak is not present in this configuration (beam parallel to wire drawing axis) because of the strong Nb texture [20].

The Nb<sub>3</sub>Sn and Cu loading strains  $\varepsilon_{hkl}$  in the transverse, axial, and radial directions have been determined from the

Nb<sub>3</sub>Sn (321) and Cu (220) scattering angles  $\theta_{hkl}$  according to equation (1). The assumed stress free scattering angles are  $2\theta_{0\text{-Nb}_3\text{Sn}(321)} = 72.783^\circ$  and  $2\theta_{0\text{-Cu}(220)} = 81.937^\circ$ .

$$\varepsilon_{hkl} = \frac{d_{hkl} - d_{0,hkl}}{d_{0,hkl}} = \frac{\sin(\theta_{0,hkl})}{\sin(\theta_{hkl})} - 1. \quad (1)$$

### 2.3. Loading stress calculations

Loading stresses have been calculated according to equation (2), assuming that the transverse, axial and radial directions are the principal stress directions in the sample, and that there are no shear stresses. Nb<sub>3</sub>Sn (321) and Cu (220) elastic constants ( $E_{hkl}$ ) and Poisson ratios ( $\nu_{hkl}$ ) have been calculated from single crystal elastic constants [21, 22] using the Kröner coupling model [23] for the interaction between crystallites ( $E_{\text{Nb}_3\text{Sn}(321)} = 131 \text{ GPa}$ ,  $\nu_{\text{Nb}_3\text{Sn}(321)} = 0.363$ ,  $E_{\text{Cu}(220)} = 138.9 \text{ GPa}$ ,  $\nu_{\text{Cu}(220)} = 0.333$ ).

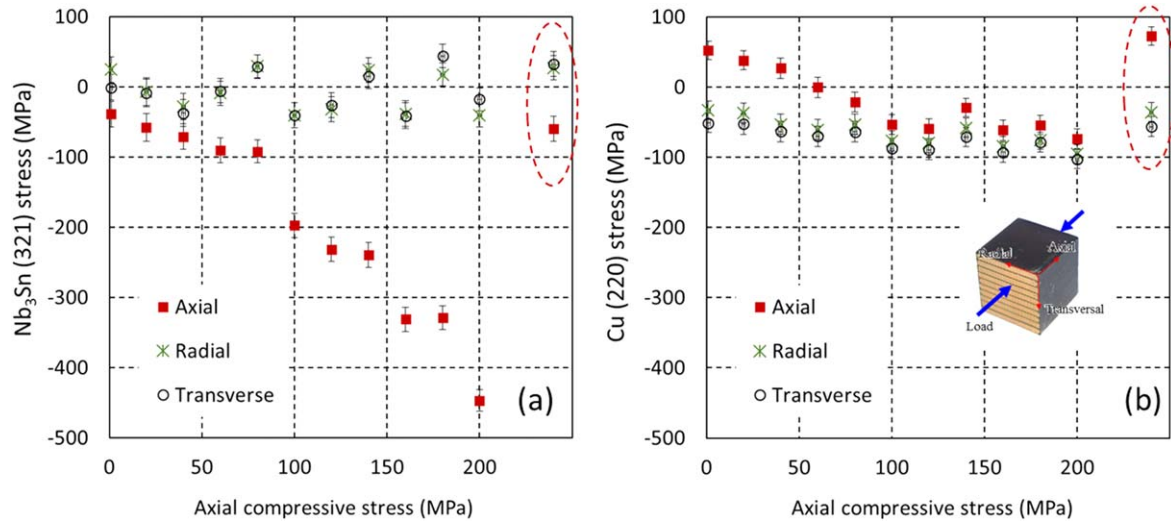
$$\sigma_{ii} = \frac{E_{hkl}}{1 + \nu_{hkl}} \left( \varepsilon_{ii} + \frac{\nu_{hkl}}{1 - 2\nu_{hkl}} (\varepsilon_{11} + \varepsilon_{22} + \varepsilon_{33}) \right). \quad (2)$$

## 3. Results

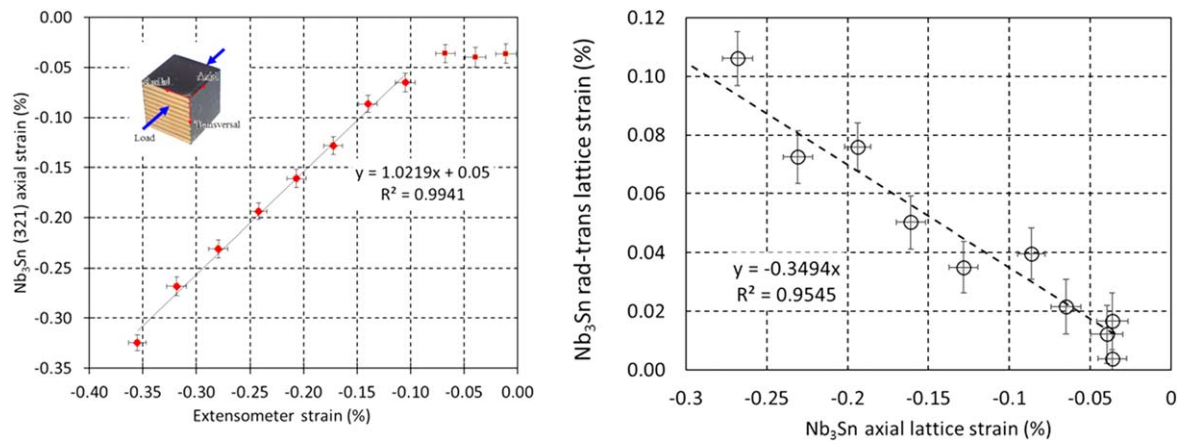
### 3.1. Transverse compression

The evolution of the Nb<sub>3</sub>Sn and Cu loading strains and stresses in a non-impregnated 11 T dipole cable stack in the three principal directions are presented in figure 3. Before application of external stress, Nb<sub>3</sub>Sn is under slight axial compression and Cu under slight axial tension. This is the result of the thermal expansion mismatch of the different conductor constituents during cooling from the Nb<sub>3</sub>Sn processing temperature of 650 °C. Upon application of external transverse pressure, a similar compressive Cu loading stress evolution is observed in the three principal directions (figure 3(d)). The transverse Cu pressure in the axial and radial directions imposes an axial and radial tensile stress on the Nb<sub>3</sub>Sn filaments (figure 3(c)).

In figure 4 the Nb<sub>3</sub>Sn and Cu loading stresses in the non-impregnated 11 T dipole cable stack are compared. In the transverse direction (i.e. the loading direction), the Nb<sub>3</sub>Sn and Cu stress evolutions are nearly identical, and the transverse stresses increase linearly with increasing external pressure. This indicates that the composite exhibits iso-stress behaviour when it is loaded perpendicularly to the filament (wire) direction. The Nb<sub>3</sub>Sn and Cu loading stress increase is about 20% higher than the external pressure increase. This difference can be partly explained by the presence of about 25% porosity in the sample that does carry load. When the external load is released the transverse Nb<sub>3</sub>Sn and Cu stresses are almost completely relaxed as well. In the radial direction Nb<sub>3</sub>Sn and Cu stresses have similar magnitude, Nb<sub>3</sub>Sn being in tension and Cu in compression. In the axial direction the higher Nb<sub>3</sub>Sn tensile stress with respect to the Cu compressive stress can be explained by a comparatively smaller



**Figure 6.** (a) Nb<sub>3</sub>Sn and (b) Cu loading stresses in an impregnated cable stack as a function of axial compressive stress. Circled data points show the residual strain when the external stress is released.



**Figure 7.** (a) Elastic axial strain derived from neutron diffraction data as a function of the macroscopic axial sample strain measured with an extensometer. (b) Average transverse and radial Nb<sub>3</sub>Sn (321) strain as a function of axial strain.

Nb<sub>3</sub>Sn cross section with respect to the Cu cross section. When the external transverse pressure is released the axial and radial stresses are only partly released.

The Nb<sub>3</sub>Sn loading stresses shown above are average values inside the gauge volume. The maximum Nb<sub>3</sub>Sn stresses are likely higher, as indicated by the Nb<sub>3</sub>Sn diffraction peak broadening when the external load is increased (figure 5). Nb<sub>3</sub>Sn diffraction peak broadening indicates that the strain inhomogeneity increases, which occurs first in the transverse and radial directions. When the external transverse pressure on the non-impregnated cable stack exceeds 130 MPa, Nb<sub>3</sub>Sn (321) peak broadening is also observed in the axial direction.

### 3.2. Axial compression

Figure 6 presents the Nb<sub>3</sub>Sn and Cu loading stress evolution in an impregnated 11 T dipole cable stack under axial compressive loading. At 150 MPa externally applied axial pressure the axial Nb<sub>3</sub>Sn (321) and Cu (220) loading stresses are about 300 MPa

and 100 MPa, respectively. This stress evolution is compatible with the assumption of iso-strain conditions when the conductor is loaded in the wire and Nb<sub>3</sub>Sn filament direction.

The assumption of iso-strain conditions is further confirmed by the comparison of the macroscopic sample strain measured with an extensometer, and the Nb<sub>3</sub>Sn filament strain determined from the Nb<sub>3</sub>Sn diffraction angles (figure 7(a)). Under axial loading the radial and transverse lattice parameter changes can be explained almost entirely by the Poisson effect (figure 7(b)).

## 4. Discussion and conclusion

Thanks to the combined stress–strain and Nb<sub>3</sub>Sn filament and Cu matrix lattice parameter measurements, a detailed understanding of the stress–strain behaviour of the conductor blocks in superconducting accelerator magnets has been obtained. The neutron diffraction results suggest that the

magnet coil wound of Rutherford type cables can be considered as a fibre reinforced composite material, which exhibits strongly anisotropic mechanical properties.

In the axial load direction, the coil block stress–strain behaviour can be predicted assuming iso-strain conditions in all composite constituents. This is consistent with the directly measured axial stiffness of an 11 T dipole cable stack of 94 GPa [18], and the stiffness calculated according to the rule of mixtures from the constituent  $E$ -moduli,  $E_{\text{wire}} = 126$  GPa [24] and  $E_{\text{epoxy}} = 4$  GPa.

In axial load direction the load is mainly carried by the  $\text{Nb}_3\text{Sn}$  filaments because the annealed Cu cannot carry high loads (at 150 MPa externally applied axial pressure the axial  $\text{Nb}_3\text{Sn}$  (321) loading stress is about 300 MPa).

Under transverse pressure the annealed Cu in the coil, which has a proof stress of  $R_{p0.2} = 50$  MPa [25], exhibits an isotropic compressive stress around the filaments. The transverse load stresses in the Cu and  $\text{Nb}_3\text{Sn}$  are similar, indicating iso-stress behaviour of the coil constituents under transverse compression.

The results presented here are a new opportunity to validate finite element models and to simulate the mechanical and electromechanical behaviour of  $\text{Nb}_3\text{Sn}$  accelerator magnet coils in more realistic conditions than has been possible so far. Under transverse compression the epoxy impregnation can reduce the  $\text{Nb}_3\text{Sn}$  loading stresses. However, assuming iso-stress behaviour, the elastic properties of the impregnation material should not strongly influence the  $\text{Nb}_3\text{Sn}$  coil stiffness.

The load case of transverse compression of unconstrained cable stacks is not fully representative for the mechanical loading in magnets, where the coils are constrained in the axial and radial directions. However, the three main results of this study, iso-strain conditions in axial load direction, iso-stress conditions in transverse compression and the isotropic compressive stress distribution in the annealed Cu, are valid for magnets too.

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