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The Electrical Resistance of Rutherford-Type Superconducting Cable Splices

S. Heck, C. Scheuerlein, J. Fleiter, A. Ballarino, and L. Bottura
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Keywords: Cables, inductance, interconnection, resistance, measurement.

Abstract

The electrical resistance of Large Hadron Collider main busbar cable lap splices produced by soft soldering has been measured with two independent methods as a function of intercable contact area and for splices made of cables with various defects. For defect-free lap splices, the resistance increases from 0.3 to 10 n Ω (at 4.3 K in self-field) when reducing the cable overlap length from 120 to 3 mm, as expected assuming that the resistance is inversely proportional to the intercable contact area. The resistance of bridge splices that connect side-by-side cables can be predicted from the lap splice resistances and the overlap areas involved.

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Index Terms—Cables, inductance, interconnection, resistance measurement.

I. INTRODUCTION

RUTHERFORD-TYPE cables are widely used for building accelerator magnet coils when the inductance of a magnet wound of a single wire would be too high. An advantage of these compact and flat cables, made for instance of Nb–Ti/Cu, Nb₃Sn/Cu strands, is that lap splices with a well-defined resistance can be relatively easily produced by soft soldering. As an example, the resistance of each of the about 10 000 main busbar cable splices of the Large Hadron Collider (LHC) [1] at 1.9 K in self-field (about 0.7 Tesla at maximum current) is 0.30 nΩ [2].

The LHC busbar cables are surrounded by an additional Cu stabilizer [3]. The LHC interconnection splices consist therefore of the Rutherford cable splices and the splices of the stabilizer profiles (see Fig. 1). During the first long LHC shutdown the resistance of all of the about 20 000 LHC Cu stabilizer profile splices has been measured at ambient temperature and the results are reported elsewhere [4].

The goal of this paper is to describe how the resistance of the superconducting Rutherford cable lap splices varies with the intercable contact area and with different cable defects. In addition we compare the resistance of the standard lap splices to that of another splice geometry connecting two side-by-side cables, as it could possibly happen to connect an inner and an outer layer inside a magnet.

Splice resistances have been measured in self-field at 4.3 K with two independent methods, notably by measuring the current decay time in test loops with known inductance, and

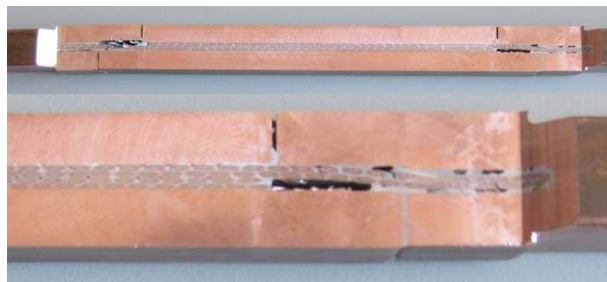


Fig. 1. Longitudinal cross section through an LHC main interconnection splice.

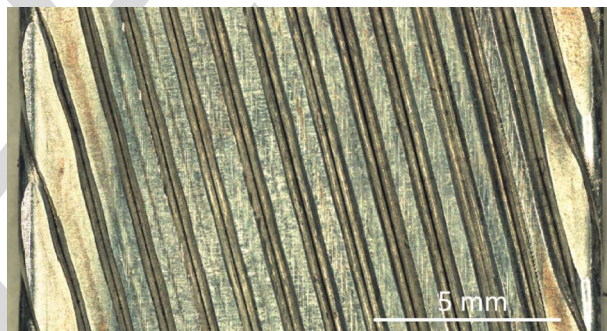


Fig. 2. Outer surface of an LHC-type 01 Rutherford cable.

by four-point resistance measurements with currents up to 27 000 A.

II. EXPERIMENTAL

A. Rutherford Cable Splices

Splices made out of Nb–Ti/Cu LHC main busbar cable have been assembled by soft soldering, using inductive heaters [5]. The LHC superconducting strands are already coated with a 0.1 to 1 μm thin Sn–Ag layer [6]. In order to prevent the complete transformation into Cu₆Sn₅ and Cu₃Sn intermetallics [7], before connection the cable extremities have been pre-tinned in a resistively heated furnace. Soldering was performed using 0.2 mm thick Sn96Ag4 foil and non-activated rosin liquid flux Kester 135. During the soldering process with a peak temperature of 270 °C the residual resistivity ratio of the Cu matrix of the strands increases to about 200 [8].

The 15.1 mm wide LHC busbar cables consist of 36 strands with a nominal diameter of 0.825 mm. The cable mid-thickness is 1.48 mm and the keystone angle is $0.90 \pm 0.05^\circ$. The cable transposition pitch is 100 ± 5 mm [9].

Fig. 2 shows the outer cable surface of an inner layer LHC dipole conductor. It can be seen that the initially round strands

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Fig. 3. Both intercable contact areas after fracturing of an LHC busbar cable splice with 10 mm cable overlap length.



Fig. 4. LHC busbar cable test loops for current decay constant measurements. The cable splices have been prepared with different cable overlap lengths ranging from 3 to 120 mm.

are flattened during the cabling process, and that the cable cross section that is in contact with the opposing cable is significantly smaller than the projected cable area and depends on the strand diameter and the cable compaction.

The resistance of splices with cable overlap lengths varying between 3 and 120 mm has been measured. The overlap lengths have been measured after fracturing the splices during tensile tests at 4.3 K (see Fig. 3). The accuracy of the stated cable overlap lengths is ± 1 mm.

B. Resistance Measurements

Splice resistance measurements have been performed with two different methods, notably by measuring the current decay time in test loops, and by four-point resistance measurements.

Current decay measurements have been performed at the CERN Cryolab. The measurement of the current decay time in test loops with a well defined geometry [10] allows to determine very low splice resistances, which are difficult to determine otherwise. Some of the test loops made of the spliced Rutherford cables produced for this study are shown in Fig. 4.

The resistance R is determined from the loop inductance L and the current decay time constant τ ($R = L/\tau$). The inductance of 260 nH that has been calculated for a busbar cable loop with ideal dimension [11] is somewhat lower than the average loop inductance of 306 nH determined by comparing splice resistance results obtained by four-point measurements



Fig. 5. Cable splices with 3, 9, 24, and 120 mm intercable contact lengths instrumented with voltage taps.

TABLE I
CURRENT DECAY CONSTANT τ OF 13 kA LHC BUSBAR CABLE SPLICES WITH DIFFERENT INTERCABLE CONTACT LENGTHS AT 4.3 K

splice length (mm)	τ (s)	*R (n Ω)
120	970 \pm 42	0.31
24	158 \pm 3.8	1.93
9.7	64.4 \pm 10	4.75
3.6	29.7 \pm 2.4	10.3

* The splice resistance R is calculated from τ , assuming a loop inductance of 306 nH.

and the decay constants for the loops made with the same 91 splices. The experimentally determined value of 306 nH is used 92 in the following.

Four-point resistance measurements in self-field at 4.3 K 94 have been performed in the FRESCA test station [12]. Several 95 splices are connected in series. The distance between the differ- 96 ent splices is about 120 mm. The voltage taps are placed in a 97 distance of 50 mm from each splice extremity. Photographs of 98 the splices with 3, 9, 24, and 120 mm overlap lengths that were 99 used for the four-point measurements are shown in Fig. 5. 100

III. RESULTS

A. Splice Resistance as a Function of Cable Overlap Length

Since the resistance in the superconductor along the con- 103 tinuous Nb-Ti filaments is zero, it can be assumed that the 104 cable splice resistance is inversely proportional to the intercable 105 contact area. In order to confirm this assumption resistance 106 measurements have been performed with LHC busbar lap 107 splices for which the overlap length has been varied between 108 3 mm and the nominal splice length of 120 mm. 109

The current decay constants determined with loops with lap 110 splices (see Fig. 4) are summarized in Table I. The results 111 shown are average values for three loops that have been pro- 112 duced for each nominal overlap length. 113

After the current decay constant measurements the loops 114 were cut (see Fig. 5) so that the four-point splice resistance 115 measurements could be performed. The voltages measured 116 across the different splices at 4.3 K as a function of the test 117 current up to 15 kA are presented in Fig. 6. Each data point has 118 been averaged over a measurement time of 300 sec. The current 119

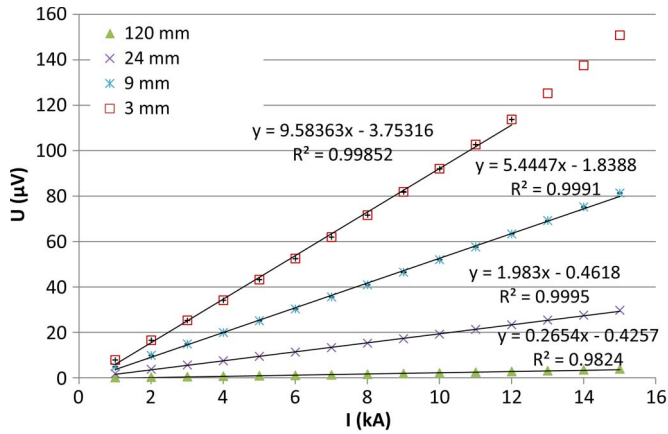


Fig. 6. Electrical potential U as a function of current I at 4.3 K without external field for splices with 3, 9, 24, and 120 mm intercable contact lengths.

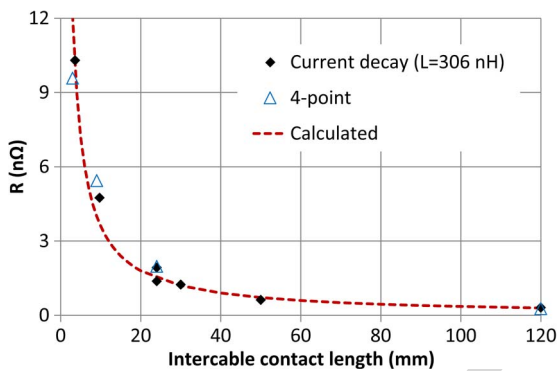


Fig. 7. Comparison of the measured and calculated LHC busbar cable splice resistances as a function of intercable overlap length.

120 ramp was about 300 A/s. Voltages below $2 \mu\text{V}$ have not been
121 taken into account for the resistance calculations.

122 The 4.3 K resistances vary between $0.27 \text{ n}\Omega$ (1200 mm
123 overlap) and $9.6 \text{ n}\Omega$ (3 mm overlap). For the 3 mm splice the
124 data points above 12 kA have not been considered because they
125 appear to deviate from the linear voltage–current relationship,
126 possibly because the critical current in some or all strands is
127 approached (the quench current of the 3 mm splice was about
128 17 kA).

129 In Fig. 7 the resistances measured for splices with different
130 overlap length are compared with resistances that were calcu-
131 lated assuming that the splice resistance is inversely propor-
132 tional to the contact length, and that a splice with 120 mm
133 overlap length has a resistance of $0.30 \text{ n}\Omega$, which is the average
134 LHC busbar splice resistance measured *in situ* in the LHC [2].
135 It can be seen that in the contact length range 3–120 mm the
136 splice resistance can be well predicted when the resistance of
137 one splice overlap length is known.

138 B. Side-by-Side Cable Bridge Splice

139 The production of lap splices always requires some cable
140 movement and bending, which is acceptable in case of ductile
141 Nb–Ti/Cu cables, but may be a problem for brittle cables, like
142 $\text{Nb}_3\text{Sn}/\text{Cu}$. A bridge splice can connect two side-by-side cables
143 without any cable bending. In order to verify if the resistance of

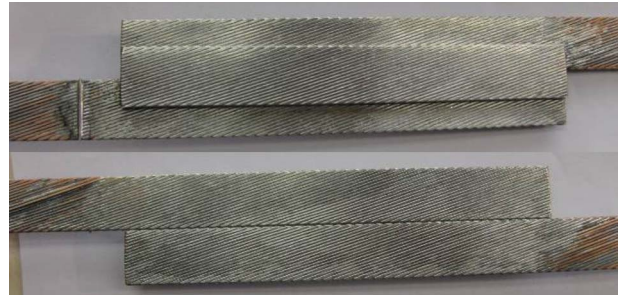


Fig. 8. Splice with two side-by-side cables connected with one opposing cable.

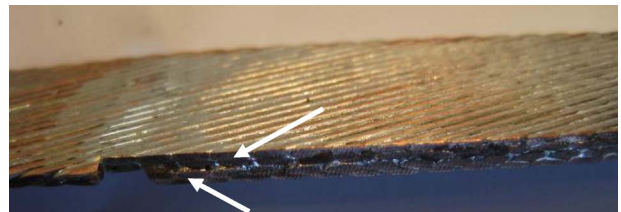


Fig. 9. Rutherford cable splice made with cables in which the strands of both opposing cables were cut on one side along the entire 120 mm overlap length.

such a bridge can be predicted with the simple assumption that
144 the resistance is inversely proportional to the intercable contact
145 area we have produced and tested the bridge splice shown in
146 Fig. 8. The resistance of this splice is $1.31 \text{ n}\Omega$.
147

The bridge splice can be considered as two lap splices that
148 are connected in series. The intercable contact area of each of
149 these is about half of that of a standard LHC lap splice. With
150 this assumption a total resistance of two times $0.6 \text{ n}\Omega = 1.2 \text{ n}\Omega$
151 can be calculated, which is in reasonable agreement with the
152 measured resistance of $1.31 \text{ n}\Omega$.
153

C. Influence of Mechanical Defects on the Resistance of 120 mm Overlap Lap Splices

In order to determine the influence of different geometrical
156 cable defects on the splice resistance, lap splices with 120 mm
157 overlap length have been prepared using LHC busbar cable on
158 which part of the strands had been cut. Fig. 9 shows a splice
159 made of two cables with all strands cut on one side along the
160 entire 120 mm intercable contact length.
161

As shown in Fig. 10 this defect increases the splice resistance
162 to $0.45 \text{ n}\Omega$, which is about 50% higher than the resistance of
163 a defect free splice. A relatively strong resistance increase to
164 $2.7 \text{ n}\Omega$ is obtained when all strands are cut along both cables on
165 both sides of the splice.
166

The 120 mm splice resistances are summarized in Table II.
167

IV. DISCUSSION AND CONCLUSION

In the following discussion it is assumed that the influence
169 of the solder resistance on the overall splice resistance can
170 be neglected. This assumption is based on the resistivity re-
171 sults obtained for the solder material [13], and on resistance
172 measurements of splices soldered with different solder alloys
173 [14]. The resistance of Nb–Ti/Cu Rutherford-type cables lap
174

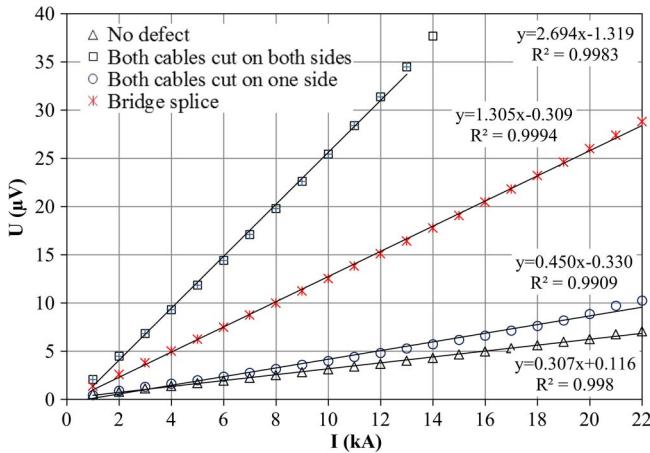


Fig. 10. Electrical potential U as a function of current I at 4.3 K without external field for splices with 120 mm intercable contact length and different defects. The results for the bridge splice of Fig. 8 is shown as well.

TABLE II
RESISTANCE OF 120 mm LONG 13 kA LHC BUSBAR CABLE SPLICES
WITH DIFFERENT DEFECTS AT 4.3 K IN SELF-FIELD

Defect	R_{loop} (n Ω)*	$R_{4\text{-point}}$ (n Ω)
None	0.26±0.03	0.31
Bridge splice	n.m.	1.31
All strands of both cables cut on one side	0.48±0.07	0.45
All strands of both cables cut on both sides	n.m.	2.69

* Assuming a loop inductance of 306 nH.

splices can then be predicted from the Cu cross sections and the Cu RRR involved. This is also the case for Rutherford cables made of Nb₃Sn/Cu wires, provided that diffusion barriers do not strongly contribute to the splice resistance [13].

Since the resistance along the superconducting filaments of the continuous cable is zero it can be assumed that in longitudinal cable direction the current is uniformly distributed over the entire splice length, and the splice resistance is inversely proportional to the intercable contact length. This is confirmed by the resistance results obtained for the Rutherford cable lap splices produced with different overlap lengths (see Fig. 7).

The influence of single cut strands on the resistance of the LHC busbar cable splices is negligible. The extreme case where all strands are cut on both sides of the Rutherford cables along the entire splice length causes a resistance of about 2.7 n Ω .

The resistance results presented here have been obtained in self-field with a huge critical current density margin of the Nb–Ti superconductor. The application of external fields influences the resistance of internal magnet splices because of the additional Cu magnetoresistance, and in case the critical current density is exceeded in some strands by a current redistribution.

The resistance of a bridge splice can be estimated from the resistance of a lap splice produced with the same cable, and the intercable contact areas. Unlike lap splices, bridge splices allow to interconnect cables without any cable bending, which is important when brittle superconductors need to be connected.

With a bridge splice a layer jump inside a Nb₃Sn magnet maybe possible. Further studies are needed to understand the performance of the different splice layouts in high applied fields.

Because of the strong field dependence of the critical current density of Nb–Ti and Nb₃Sn superconductors, there is always a huge margin in terms of critical current density for splices that are outside the high field region of a magnet. The critical current density of high temperature superconductors like Bi-2212 is only relatively weakly related to the applied field, and if such conductors are exploited at their full potential the I_c margin in self-field will be relatively small, so that the splice production and non-destructive splice tests will require particular attention.

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AQ2 = Please provide publication update in Ref. [9].

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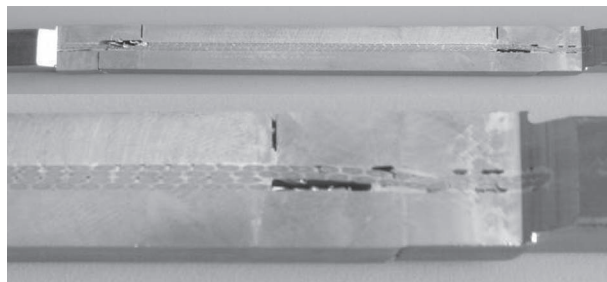


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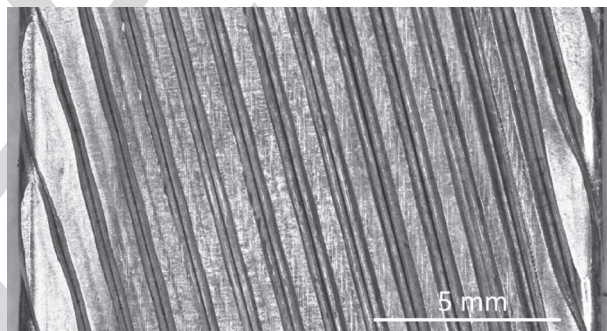


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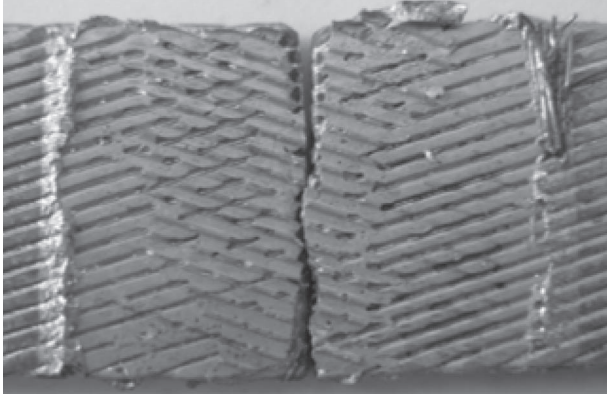


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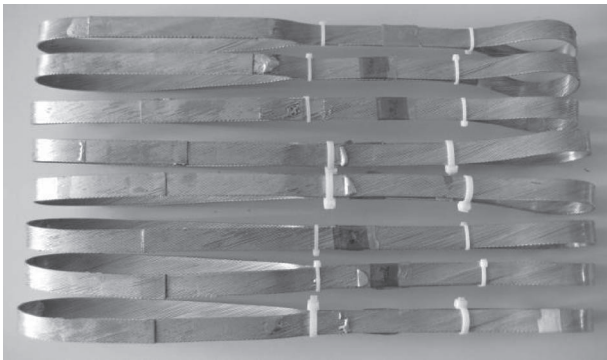


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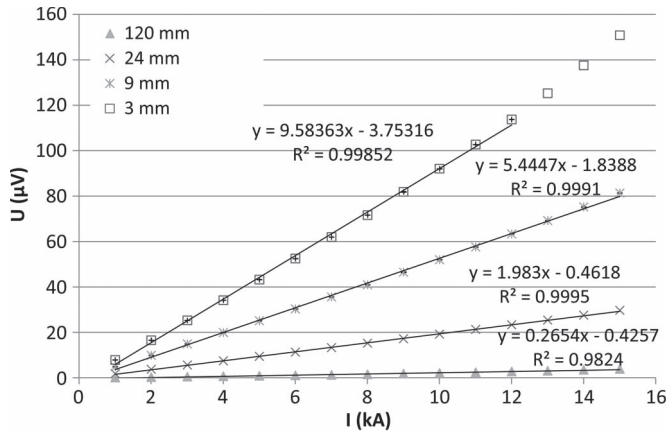


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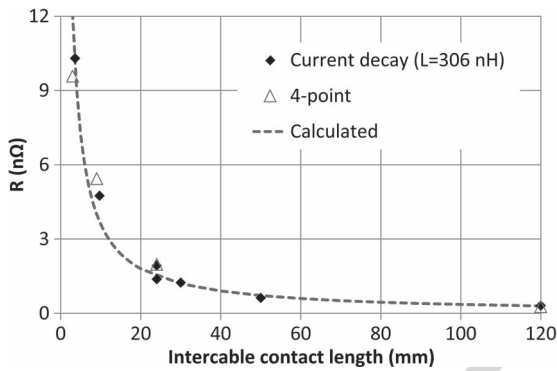


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129 In Fig. 7 the resistances measured for splices with different
130 overlap length are compared with resistances that were calcu-
131 lated assuming that the splice resistance is inversely propor-
132 tional to the contact length, and that a splice with 120 mm
133 overlap length has a resistance of $0.30 \text{ n}\Omega$, which is the average
134 LHC busbar splice resistance measured *in situ* in the LHC [2].
135 It can be seen that in the contact length range 3–120 mm the
136 splice resistance can be well predicted when the resistance of
137 one splice overlap length is known.

138 B. Side-by-Side Cable Bridge Splice

139 The production of lap splices always requires some cable
140 movement and bending, which is acceptable in case of ductile
141 Nb–Ti/Cu cables, but may be a problem for brittle cables, like
142 $\text{Nb}_3\text{Sn}/\text{Cu}$. A bridge splice can connect two side-by-side cables
143 without any cable bending. In order to verify if the resistance of

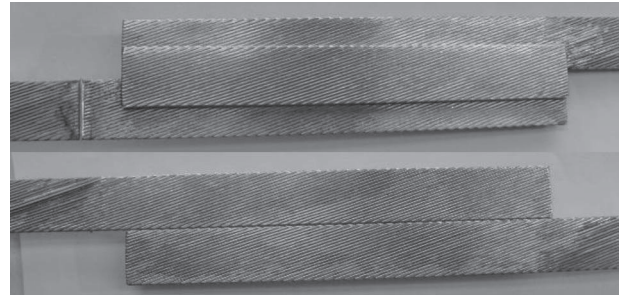


Fig. 8. Splice with two side-by-side cables connected with one opposing cable.

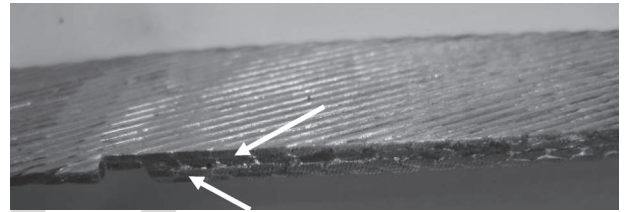


Fig. 9. Rutherford cable splice made with cables in which the strands of both opposing cables were cut on one side along the entire 120 mm overlap length.

such a bridge can be predicted with the simple assumption that
144 the resistance is inversely proportional to the intercable contact
145 area we have produced and tested the bridge splice shown in
146 Fig. 8. The resistance of this splice is $1.31 \text{ n}\Omega$.
147

The bridge splice can be considered as two lap splices that
148 are connected in series. The intercable contact area of each of
149 these is about half of that of a standard LHC lap splice. With
150 this assumption a total resistance of two times $0.6 \text{ n}\Omega = 1.2 \text{ n}\Omega$
151 can be calculated, which is in reasonable agreement with the
152 measured resistance of $1.31 \text{ n}\Omega$.
153

C. Influence of Mechanical Defects on the Resistance of 120 mm Overlap Lap Splices

In order to determine the influence of different geometrical
156 cable defects on the splice resistance, lap splices with 120 mm
157 overlap length have been prepared using LHC busbar cable on
158 which part of the strands had been cut. Fig. 9 shows a splice
159 made of two cables with all strands cut on one side along the
160 entire 120 mm intercable contact length.
161

As shown in Fig. 10 this defect increases the splice resistance
162 to $0.45 \text{ n}\Omega$, which is about 50% higher than the resistance of
163 a defect free splice. A relatively strong resistance increase to
164 $2.7 \text{ n}\Omega$ is obtained when all strands are cut along both cables on
165 both sides of the splice.
166

The 120 mm splice resistances are summarized in Table II.
167

IV. DISCUSSION AND CONCLUSION

In the following discussion it is assumed that the influence
169 of the solder resistance on the overall splice resistance can
170 be neglected. This assumption is based on the resistivity re-
171 sults obtained for the solder material [13], and on resistance
172 measurements of splices soldered with different solder alloys
173 [14]. The resistance of Nb–Ti/Cu Rutherford-type cables lap 174

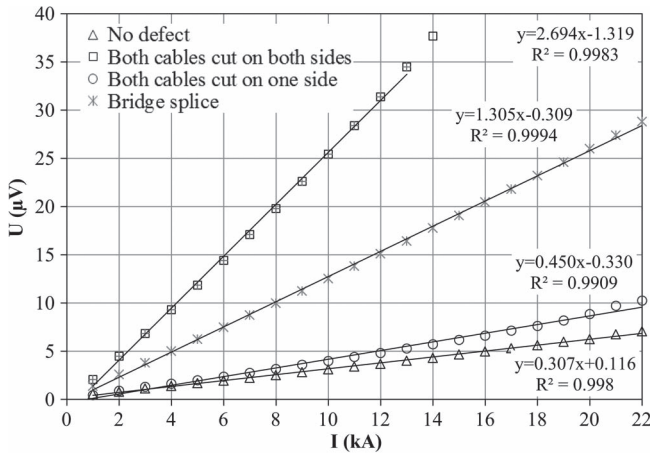


Fig. 10. Electrical potential U as a function of current I at 4.3 K without external field for splices with 120 mm intercable contact length and different defects. The results for the bridge splice of Fig. 8 is shown as well.

TABLE II
RESISTANCE OF 120 mm LONG 13 kA LHC BUSBAR CABLE SPLICES
WITH DIFFERENT DEFECTS AT 4.3 K IN SELF-FIELD

Defect	R_{loop} (n Ω)*	$R_{4\text{-point}}$ (n Ω)
None	0.26±0.03	0.31
Bridge splice	n.m.	1.31
All strands of both cables cut on one side	0.48±0.07	0.45
All strands of both cables cut on both sides	n.m.	2.69

* Assuming a loop inductance of 306 nH.

175 splices can then be predicted from the Cu cross sections and the 176 Cu RRR involved. This is also the case for Rutherford cables 177 made of Nb₃Sn/Cu wires, provided that diffusion barriers do 178 not strongly contribute to the splice resistance [13].

179 Since the resistance along the superconducting filaments of 180 the continuous cable is zero it can be assumed that in longitu- 181 dinal cable direction the current is uniformly distributed over 182 the entire splice length, and the splice resistance is inversely 183 proportional to the intercable contact length. This is confirmed 184 by the resistance results obtained for the Rutherford cable lap 185 splices produced with different overlap lengths (see Fig. 7).

186 The influence of single cut strands on the resistance of the 187 LHC busbar cable splices is negligible. The extreme case where 188 all strands are cut on both sides of the Rutherford cables along 189 the entire splice length causes a resistance of about 2.7 n Ω .

190 The resistance results presented here have been obtained in 191 self-field with a huge critical current density margin of the 192 Nb–Ti superconductor. The application of external fields influ- 193 ences the resistance of internal magnet splices because of the 194 additional Cu magnetoresistance, and in case the critical current 195 density is exceeded in some strands by a current redistribution.

196 The resistance of a bridge splice can be estimated from the 197 resistance of a lap splice produced with the same cable, and 198 the intercable contact areas. Unlike lap splices, bridge splices 199 allow to interconnect cables without any cable bending, which 200 is important when brittle superconductors need to be connected.

201 With a bridge splice a layer jump inside a Nb₃Sn magnet 202 maybe possible. Further studies are needed to understand the 203 performance of the different splice layouts in high applied 204 fields.

205 Because of the strong field dependence of the critical current 206 density of Nb–Ti and Nb₃Sn superconductors, there is always a 207 huge margin in terms of critical current density for splices that 208 are outside the high field region of a magnet. The critical current 209 density of high temperature superconductors like Bi-2212 is 210 only relatively weakly related to the applied field, and if such 211 conductors are exploited at their full potential the I_c margin 212 in self-field will be relatively small, so that the splice pro- 213 duction and non-destructive splice tests will require particular 214 attention.

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